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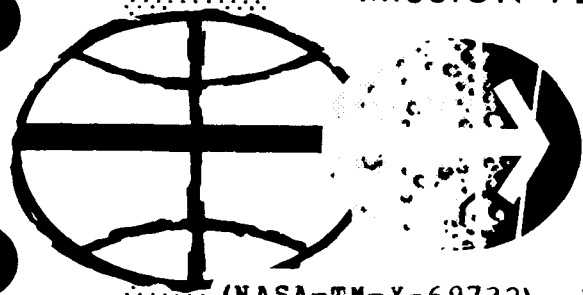
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VIEWS FROM THE SPACECRAFT  
DURING APOLLO 10 (MISSION F)  
MAY 18, 1969 LAUNCH DATE

Flight Analysis Branch

MISSION PLANNING AND ANALYSIS DIVISION



MANNED SPACECRAFT CENTER  
HOUSTON, TEXAS

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PROJECT APOLLO

VIEWS FROM THE SPACECRAFT DURING APOLLO 10  
(MISSION F) MAY 18, 1969 LAUNCH DATE

By Alfred N. Lunde  
Flight Analysis Branch

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April 22, 1969

MISSION PLANNING AND ANALYSIS DIVISION  
NATIONAL AERONAUTICS AND SPACE ADMINISTRATION  
MANNED SPACECRAFT CENTER  
HOUSTON, TEXAS

Approved: Charlie C. Allen  
Charlie C. Allen, Chief  
Flight Analysis Branch

Approved: John P. Mayer  
John P. Mayer, Chief  
for Mission Planning and Analysis Division

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# VIEWS FROM THE SPACECRAFT DURING APOLLO 10 (MISSION F)

MAY 18, 1969 LAUNCH DATE

By Alfred N. Lunde

## SUMMARY

The purpose of this document is to visually depict various aspects of the Apollo 10 (Mission F) lunar flight. Views of the earth and the moon as seen from the spacecraft are shown during the translunar and transearth coast phases as well as the view from the spacecraft during critical maneuvers. The data should prove invaluable in assuring the crew that maneuver attitudes are correct. All data presented in this report are for the first opportunity, 72° launch azimuth, May 18, 1969 launch date.

## INTRODUCTION

The geometry of a lunar mission can be very difficult to visualize. The primary objective of this report is to provide views from the spacecraft during Apollo 10 (Mission F) because a knowledge of how the spacecraft should be oriented with respect to familiar objects visible from the spacecraft window would be invaluable for performance of the various maneuvers.

A detailed visual representation of Apollo 10 (Mission F) for the May 17, 1969 launch date is presented in reference 1. Because of the 1-day slip in the launch date, most of the data in reference 1 are no longer applicable to the Apollo 10 flight. A discussion of the trajectory geometry and the general information are presented in reference 1.

In the figures for the lunar orbit phase section, the location of the planets Venus, Mars, Jupiter, and Saturn has been shown.

## SYMBOLS

c.g.	center of gravity
CDH	constant delta height
CM	command module
CSI	concentric sequencing initiation
CSM	command and service modules
DOI	descent orbit insertion
EI	entry interface
g.e.t.	ground elapsed time
$h_E$	altitude above earth's surface
$h_M$	altitude above moon's surface
LOI	lunar orbit insertion
LM	lunar module
PTC	passive thermal control
$R_E$	radius from center of earth
$R_M$	radius from center of moon
SEQ	star identification number
SM	service module
TEC	transearth coast
TEI	transearth injection
TLC	translunar coast
TLI	translunar injection
TPI	terminal phase initiation
$V_i$	inertial velocity

## DISCUSSION OF THE DATA

The geometry associated with the Apollo 10 lunar mission is presented in figures 1 through 5. A detailed description of figures 1 through 4 can be found in reference 1. The nominal F mission rendezvous is presented in figure 5.

### Translunar Injection Burn

The beginning, middle, and end of the TLI burn are shown in figure 6. The maneuver is executed in a heads down position. The horizon is in darkness until toward the end of the burn. The TLI burn places the spacecraft on its lunar trajectory so that at the end of the burn the velocity is 35 591 fps.

### Earth and Moon Views During TLC

The earth is shown in figure 7 with a constant field of view. Because the earth gets quite small as the spacecraft progresses on its lunar trajectory, the earth with a variable field of view is presented in figure 8. The purpose of the enlarged views of the earth is to show details such as continents and terminator. Because these views are almost identical to the views shown on pages 60 through 77 in reference 1, only a few TLC variable field views are shown in this report. The reader who desires to find out what portion of the earth is visible to the crew every hour during TLC should consult the above mentioned pages in reference 1.

Views of the moon are presented in figures 9 and 10. Because of the earth-moon-sun geometry at this particular time, the moon will be almost totally dark as viewed from the spacecraft on the approach trajectory.

### Lunar Orbit Insertion Maneuver

The beginning, middle, and end of the LOI burn are depicted in figure 11. There is a rather large yaw attitude component during this burn designed to place the spacecraft in an orbit similar to that of the lunar landing mission. The crew are in a heads down position during this burn, and the burn is performed in a retrograde attitude to brake the trajectory speed so that a lunar orbit may be achieved.

### Lunar Orbit Phase

Various LM events after separation from the CSM and prior to docking again with the CSM are shown in figure 12. The view from the commander's front LM window and from the docking window are shown with the correct burn attitude for DOI burn, phasing burn, LM descent stage jettison burn, insertion burn, CSI burn, CDH burn, and the TPI burn. The reader should consult figure 5 for a better understanding of those views.

### Transearth Injection Maneuver

As with TLI and LOI, the beginning, middle, and end of the TEI burn are shown in the correct burn attitude. This maneuver is a posigrade burn designed to free the spacecraft from the lunar gravitational attraction. The spacecraft attains a velocity of 8958 fps at the end of the burn to return the spacecraft to earth in approximately 54.5 hours.

### Post-TEI Views

The four post-TEI views depict the view from the spacecraft as the earth comes into view over the lunar horizon. The Southeast Asia portion of the earth is visible at this time.

### Transearth Coast

As with the translunar coast, the views of the earth and the moon are shown at various times during the coast period (figs. 15, 16, 17, and 18). During this coast period, approximately half of the earth and moon are in sunlight as seen from the spacecraft. The spacecraft leaves the lunar gravitational sphere of influence at approximately 148 hours g.e.t., at which time the velocity will gradually increase until it reaches 36 309 fps at entry.

### Entry

The entry phase is shown in figure 19. The SM is jettisoned approximately 15 minutes prior to entry interface, and the CM is in a heatshield forward attitude. The angle between the spacecraft X-axis and the earth horizon is held at  $+31.7^\circ$ , which can be monitored on the  $31.7^\circ$  scribe on the window. The moon is visible during part of the entry phase. The entry REFSMMAT's were obtained from reference 2.

(Most of the vectors needed to generate the data shown in this report were obtained from reference 3.)

### CONCLUSIONS

An understanding of spacecraft attitudes with respect to the sun, earth, moon, and stars is particularly useful to verify maneuver attitudes normally described by IMU gimbal angles. This information is especially useful for Apollo 10 (Mission F) because IMU gimbal angles are referenced to several specific inertial orientations (REFSMMAT) instead of to preferred platform alinements.

This report has presented numerous figures which depict the view from the Apollo 10 (Mission F) windows: star field, earth and moon terminators, and horizon orientations are included. This information should prove invaluable in assuring the crew that maneuver attitudes are correct.

TABLE 1. - STAR IDENTIFICATION CATALOGUE

SEQ NO.	IDENTIFICATION	RIGHT ASCENSION HRS	MIN	SEC	DECLINATION DEGREES	DECLINATION DEG	MIN	SEC	MAG	IDENTIFICATION		
1	33330	00275000	00	00	9.9	-6.20861110	-6.0	12.0	31.0	4.66	30	PSC
2	23	00324444	00	1.0	56.6	-7.53033300	-17.0	31.0	51.0	4.66	2	CEP
3	59	00590555	00	32.6	32.6	-5.70333300	-5.0	54.0	12.0	4.68	3	PSC
4	127	ALPHERATZ	SIRRAH	4.0	4.0	28.69722100	28.0	53.0	50.0	4.74	0	PSC
5	147	CAPM		7.0	17.9	58.95666000	58.0	24.0	2.92	2.15	21	AND
6	158			7.0	38.4	45.94055500	45.0	24.0	24.0	3.94	0	PSC
7	238	ALGENIB		11.0	25.8	14.98916600	14.0	59.0	21.0	2.87	0	PEB
8	272			12.0	51.8	-19.12666600	-19.0	7.0	36.0	4.68	7	CEP
9	334			15.0	15.4	38.48749900	38.0	29.0	15.0	4.44	29	J AND
10	362			16.0	29.5	38.59138800	38.0	35.0	29.0	4.51	25	J AND
11	388			17.0	38.6	-9.01777700	-9.0	1.0	4.0	3.75	8	1 CEP
12	401			18.0	15.5	-65.08055500	-65.0	4.0	50.0	4.74	0	X TUC
13	503	ALGENIB		23.0	56.3	-77.45138800	-77.0	27.0	5.0	2.90	0	0 HVI
14	516			24.0	29.1	-43.87388800	-43.0	52.0	26.0	3.90	0	0 PHE
15	519	ANKAA		24.0	33.4	-42.49611000	-42.0	29.0	46.0	2.44	0	0 PHE
16	625			29.0	57.7	-63.15833300	-63.0	9.0	30.0	4.52	0	0 TUC
17	645			30.0	59.6	62.73888900	62.0	49.0	20.0	4.24	15	K CAS
18	729			35.0	1.4	33.52694400	33.0	31.0	37.0	4.44	29	P AND
19	727			35.0	1.4	53.70444400	53.0	42.0	16.0	3.72	17	Z CAS
20	759			36.0	42.0	29.12194400	29.0	7.0	19.0	4.52	30	E AND
21	774			37.0	27.0	30.66972200	30.0	40.0	11.0	2.47	31	0 AND
22	792	SCHEDIR	SCHEDAR	39.0	30.5	56.34583300	56.0	20.0	45.0	2.47	18	A CAS
23	823			39.0	40.5	-46.27694400	-46.0	14.0	37.0	4.65	0	0 PHE
24	866			41.0	47.2	-57.65499900	-57.0	39.0	18.0	4.53	0	0 PHE
25	885	DIPMDA	DENEH	42.0	50.0	-18.11803300	-18.0	10.0	42.0	2.44	16	0 CEP
26	882			42.0	45.9	48.09305500	48.0	5.0	35.0	4.70	22	0 CAS
27	940			45.0	28.7	24.02769400	24.0	4.0	37.0	4.30	34	Z AND
28	943			46.0	51.8	7.33950000	7.0	23.0	42.0	4.55	63	0 PSC
29	962	ACHIRO		46.0	58.0	57.63055500	57.0	37.0	50.0	3.44	24	M CAS
30	985			47.0	52.5	40.88861000	40.0	53.0	19.0	4.42	35	M AND
31	1117			54.0	34.8	60.52777400	60.0	31.0	40.0	2.30	27	6 CAS
32	1122			54.0	48.2	38.31000000	38.0	18.0	36.0	3.94	37	M AND
33	1136			55.0	20.0	23.22916600	23.0	13.0	45.0	4.62	38	M AND
34	1172			56.0	53.2	-29.54638800	-29.0	32.0	47.0	4.39	0	0 A SCL
35	1258			1.0	7.4	7.70222200	7.0	42.0	8.0	4.45	71	E PSC
36	1288			1.0	3.0	86.07055500	86.0	54.0	14.0	4.50	43	0 CEP
37	1335			4.0	31.5	-46.90583300	-46.0	5.0	21.0	3.35	0	0 PHE
38	1384			6.0	49.7	-10.36722200	-10.0	22.0	2.0	3.60	31	M CEP
39	1387			6.0	55.0	-55.43249900	-55.0	25.0	57.0	4.13	0	0 Z PHE
40	1394			7.0	27.6	47.05555500	47.0	3.0	20.0	4.48	42	V AND
41	1400	MIRACH		7.0	45.9	35.43555500	35.0	26.0	8.0	2.37	43	0 AND
42	1424			8.0	57.5	54.96916600	54.0	57.0	51.0	4.52	33	J CAS
43	1441			9.0	43.6	29.90916600	29.0	54.0	15.0	4.70	83	J PSC
44	1474			11.0	50.5	24.39861100	24.0	23.0	55.0	4.64	88	V PSC
45	1591			17.0	32.2	27.08055500	27.0	4.0	50.0	4.67	90	J PSC
46	1695			18.0	16.3	-8.36361110	-8.0	21.0	49.0	3.82	45	J CEP
47	1715	KSORA	HUCMA	23.0	30.5	60.05916600	60.0	3.0	50.0	2.88	37	8 CAS
48	1787			26.0	50.8	-43.49722200	-43.0	29.0	15.0	3.48	0	0 PHE
49	1839			29.0	36.4	15.16883300	15.0	9.0	57.0	3.72	9	0 PSC
50	1847			29.0	47.7	-49.25916600	-49.0	13.0	15.0	3.46	0	0 D PHE
51	1948			34.0	44.0	41.23111100	41.0	13.0	52.0	4.18	50	U AND
52	1966			35.0	49.9	48.45166600	48.0	27.0	6.0	3.77	51	0 A AND
53	1979	ACHERMAR		38.0	24.7	-57.41416600	-57.0	24.0	51.0	4.60	0	0 A ERI
54	2055			39.0	36.4	5.31111110	5.0	18.0	40.0	4.68	106	M PSC
55	2102			41.0	27.3	50.51305500	50.0	30.0	47.0	4.20	0	0 V PER

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

54	2123	1-70736109	1-0	42-0	26-5	-16+12111000	-14+0	71-0	16+0	3+65	52 T	CET
56	2139	1-72569442	1-0	43-0	32-5	8+98222220	8-0	58-0	56+0	4+50	110 O	PSC
58	2249	1-82886110	1-0	49-0	43-9	-10-50722210	-10-0	30-0	46+0	3+92	55 Z	CET
59	2272	1-85133332	1-0	51-0	4+8	29+74299900	29+0	44-0	33+0	3+58	2 A	TRI
60	2291	1-86008333	1-0	51-0	36-3	19+12277700	19+0	74-0	22+0	4+75	5 6	ARI
61	2289	1-86424999	1-0	51-0	51-3	63+49861100	63+0	29-0	55+0	3+44	45 E	CAS
62	2303	1-87072220	1-0	52-0	14-6	-46+47361000	-46+0	26+0	25+0	4+41	0 Y	PHE
63	2309	1-87836109	1-0	52-0	42-1	20+63777000	20+0	38-0	16+0	2+72	6 B	ARI
64	2331	1-90074998	1-0	54-0	2+7	-67+81916600	-67+0	49-0	9+0	4+72	0 M	HYI
65	2339	1-90944443	1-0	54-0	35+8	-51+78277000	-51+0	46-0	58+0	3+73	0 K	ERI
66	2369	1-92966665	1-0	55-0	46+8	-47+55555500	-47+0	33+0	20+0	4+74	0	PHE
67	2405	1-96111110	1-0	57-0	40-0	-61+73972100	-61+0	44-0	23+0	3+02	0 A	HYI
68	2419	1-97258331	1-0	58-0	21+3	-21+24666600	-21+0	14-0	48+0	4+18	59 U	CET
69	2424	1-98408331	1-0	59-0	2+7	70+73861000	70+0	44-0	19+0	4+61	48	CAS
70	2443	ALRUCCABA	1-0	59-0	24-3	89+10222100	89+0	64-0	84-0	2+12	0 A	URI
71	2452	KAITAIN	2-0	0	14-0	2+59555550	2+0	35-0	44-0	4+33	113 A	PSC
72	2445	ALRISHA	2-0	0	24-3	72+25333300	72+0	15-0	12+0	4+06	50	CAS
73	2477	ALAMAK	2-0	1-0	44-5	42+16277700	42+0	9-0	46+0	4+24	0 6	AND
74	2504	ALAMAK	2-0	2-0	55-3	-29+48416700	-29+0	27-0	51+0	4+74	0 N	FOR
75	2538	MAHAL	2-0	5-0	11-7	23+29777700	23+0	17-0	52+0	2+23	13 A	ARI
76	2572	MAHAL	2-0	7-0	27-2	34+82250000	34+0	49-0	21+0	3+04	4 B	TAI
77	2654	MIRA	2-0	11-8	8+5	8+68333300	8+0	41-0	11+0	4+07	45 C	CET
78	2742	MIRA	2-0	15-0	13-6	33+68338000	33+0	41-0	11+0	4+07	9 6	TRI
79	2756	MIRA	2-0	15-0	15-5	-51+67361100	-51+0	40-0	25+0	3+78	0 V	ERI
80	2796	MIRA	2-0	17-0	34-5	-3+13555550	-3+0	8-0	8-0	2+00V	48 0	CET
81	2872	MIRA	2-0	21-0	7-2	-68+81833200	-68+0	49-0	6+0	4+26	0 8	HYI
82	2954	MIRA	2-0	25-0	42-1	-47+84027700	-47+0	51-0	37+0	4+44	0 K	HYI
83	2952	MIRA	2-0	26-0	9-2	67+24666600	67+0	14-0	48+0	4+59	0 I	CAS
84	2960	MIRA	2-0	26-0	17-7	8+30416660	8+0	18-0	15+0	4+34	73 C	CET
85	3192	MIRA	2-0	37-0	41-1	-17861111	-17861111	10-0	43+0	4+04	82 D	CET
86	3217	MIRA	2-0	38-0	27-9	-43+04111000	-43+0	24-0	28+0	4+53	0 E	HYI
87	3240	MIRA	2-0	39-0	2+7	-68+41638000	-68+0	24-0	59+0	4+26	0 K	HYI
88	3237	MIRA	2-0	39-0	17-1	-40+00444400	-40+0	14-0	14+0	4+06	0 I	ERI
89	3273	MIRA	2-0	41-0	23-5	27+55444400	27+0	33-0	34+0	4+58	35	ARI
90	3276	KAFFALJIDHMA	2-0	41-0	29-1	3+08916670	3+0	54-0	21+0	3+58	86 8	CET
91	3277	KAFFALJIDHMA	2-0	41-0	47-8	49+08166600	49+0	49-0	54-0	4+22	13 J	PER
92	3300	MIRA	2-0	42-0	27-3	-14+00611100	-14+0	10	23+0	4+39	89 P	CET
93	3309	MIRA	2-0	43-0	2+8	89+67500000	89+0	58-0	33+0	4+36	87 M	CET
94	3318	MIRA	2-0	43-0	28-1	-18+71972200	-18+0	43+0	11+0	4+61	1 Y	ERI
95	3354	MIRA	2-0	45-0	49-1	29+10277800	29+0	64-0	10+0	4+62	39	ARI
96	3387	MIRA	2-0	47-0	37-5	-32+52221000	-32+0	33-0	8+0	4+50	0 8	FOR
97	3391	MIRA	2-0	47-0	55-1	27+17500000	27+0	7-0	3-0	3+88	41	ARI
98	3390	MIRAM	2-0	48-0	7+7	55+75166600	55+0	45-0	64-0	3+93	15 M	PER
99	3401	MIRAM	2-0	48-0	22-0	38+17583300	38+0	10+0	33+0	4+27	16	PER
100	3419	MIRAM	2-0	49-0	21-1	34+91694400	34+0	55-0	1+0	4+67	17	PER
101	3463	MIRAM	2-0	50-0	40-6	-75+20999900	-75+0	12-0	36+0	4+70	0 N	HYI
102	3462	MIRAM	2-0	51-0	45-8	52+62055500	52+0	37-0	14+0	4+06	18 Y	PER
103	3539	AZHA	2-0	54-0	42-9	-9+03638800	-9+0	24-0	11+0	4+05	3 M	ERI
104	3567	AZHA	2-0	56-0	30-9	39+52388800	39+0	31-0	26+0	4+62	22 P	PER
105	3584	ACAMAR	2-0	56-0	56-0	-40+44416600	-40+0	26+0	39+0	3+42	0 J	ERI
106	3582	ACAMAR	2-0	57-0	12-3	21+20138900	21+0	12-0	5+0	4+44	48 E	ARI
107	3595	ACAMAR	2-0	57-0	50-1	8+76888800	8+0	46-0	8-0	4+69	91 L	CET
108	3643	MEKAR	3-0	0	26-8	3+95361110	3+0	57-0	13+0	2+82	92 A	CET
109	3649	MEKAR	3-0	0	50-9	-23+76055500	-23+0	45-0	38+0	4+16	11 Y	ERI
110	3644	ALGOL	3-0	2-0	14-9	53+37083300	53+0	22+0	15+0	3+08	23 6	PER
111	3682	ALGOL	3-0	2-0	55-6	38+70583300	38+0	42+0	21+0	3+00V	25	PER
112	3733	ALGOL	3-0	5-0	53-0	40+82221000	40+0	49-0	20+0	2+30	24 9	PER
113	3740	ALGOL	3-0	6-0	31-8	49+46111100	49+0	28+0	52+0	4+17	0 I	PER

CYMR  
OKDA

TABLE 1. - STAR IDENTIFICATION CATALOGUE - Continued

114	3755	MISAM	3.11874990	3.00	7.00	7.5	44.72611000	44.0	43.10	34.00	4.00	27	K	PER
115	3805	BOTEIN	3.16030880	3.00	9.00	3.4	19.59555500	19.00	35.00	44.00	4.53	57	D	ARI
116	3831		3.17430880	3.00	10.00	3.0	-49.12416600	-29.00	7.00	27.00	3.95	0	A	FOR
117	3879		3.17930550	3.00	17.00	57.5	-21.08041600	-21.00	53.00	33.00	3.95	16	T	ARI
118	3981		3.30361110	3.00	18.00	13.00	28.92277800	28.00	55.10	22.10	4.72	0		
119	4000	MIRFAK	3.30880100	3.00	18.00	31.9	-43.20277800	-43.00	12.00	10.00	4.30	82		ARI
120	4041	MIRFAK	3.36355550	3.00	21.00	48.8	49.73033300	49.00	44.00	18.00	1.90	33	A	PER
121	4070		3.38211100	3.00	25.00	55.6	8.90694400	8.00	54.00	25.00	3.80	1	B	TAU
122	4107		3.42130800	3.00	25.00	16.1	9.61194450	9.00	36.00	43.00	3.75	2	C	TAU
123	4113		3.443697210	3.00	26.00	13.1	59.82027700	59.00	49.00	13.00	4.67	2		CAM
124	4133		3.444758320	3.00	26.00	51.3	49.38916600	49.00	49.00	21.00	4.67	34		PER
125	4158		3.446827770	3.00	28.00	5.8	47.87611100	47.00	52.00	34.00	4.55	35	S	PER
126	4184		3.48221770	3.00	28.00	56.2	12.81805550	12.00	49.00	5.00	4.28	5		TAU
127	4244		3.52133330	3.00	31.00	16.8	-9.57555550	-9.00	34.00	32.00	3.81	18	E	ARI
128	4258		3.53733330	3.00	32.00	14.4	-21.74916600	-21.00	44.00	57.00	4.24	4	T	ERI
129	4287		3.56655550	3.00	32.00	59.6	48.07777700	48.00	44.00	40.00	4.26	37	V	PER
130	4313		3.58479900	3.00	35.00	5.1	*29.166666	*0	17.00	30.00	4.90	10		TAU
131	4329		3.59727700	3.00	35.00	50.2	-40.38861000	-40.00	23.00	19.00	4.58	0		ERI
132	4427		3.597372220	3.00	40.00	25.4	47.67222100	47.00	40.00	38.00	3.10	39	D	PER
133	4455		3.62225000	3.00	41.00	33.1	-37.42305500	-37.00	25.00	23.00	4.64	0		ERI
134	4450	RANA	3.62823300	3.00	41.00	34.2	-9.88083300	-9.00	52.00	51.00	3.72	23	D	ERI
135	4461	ATIKS	3.70197210	3.00	42.00	7.1	32.17888800	32.00	10.00	44.00	3.94	38	0	TAU
136	4477	ELECTRA	3.71322220	3.00	42.00	48.6	24.00472200	24.00	28.00	17.00	3.81	17		TAU
137	4474		3.71347220	3.00	42.00	48.6	42.46972100	42.00	28.00	11.00	3.93	41	N	PER
138	4486	TARGETA	3.71866660	3.00	43.00	7.2	24.35888900	24.00	21.00	32.00	4.37	19		TAU
139	4500	MAIA	3.72899900	3.00	43.00	46.4	24.25972100	24.00	15.00	35.00	4.02	20		TAU
140	4517		3.72922220	3.00	43.00	49.2	-64.91694300	-64.00	55.00	55.00	3.60	0	B	RET
141	4512	MEROPE	3.73741660	3.00	44.00	18.7	23.88083300	23.00	50.00	47.00	4.25	23		TAU
142	4525		3.74141660	3.00	44.00	29.1	-12.21027760	-12.00	12.00	37.00	4.64	26	B	ERI
143	4547		3.75564460	3.00	45.00	20.5	-23.35194300	-23.00	21.00	7.00	4.33	27	T	ERI
144	4541	ALCYONE	3.75666660	3.00	45.00	24.0	23.99833300	23.00	59.00	54.00	2.96	25	H	TAU
145	4553		3.77158330	3.00	46.00	17.7	65.41999900	65.00	25.00	12.00	4.71	0		CAM
146	4557		3.77719440	3.00	46.00	37.9	71.22669400	71.00	13.00	37.00	4.67	0	B	CAM
147	4586	ATLAS	3.78461110	3.00	47.00	9.6	23.94777800	23.00	54.00	52.00	3.80	27		TAU
148	4633		3.79602770	3.00	47.00	48.7	-74.34666600	-74.00	20.00	48.00	3.17	0	B	HTI
149	4624		3.80238800	3.00	48.00	8.6	-36.38527700	-36.00	18.00	19.00	4.24	0		ERI
150	4608	HENKHIB	3.86544440	3.00	51.00	58.6	31.78111100	31.00	48.00	52.00	2.91	44	Z	PER
151	4759		3.92497220	3.00	55.00	29.9	-39.91055800	-39.00	54.00	38.00	2.96	45	E	PER
152	4778	ZAURAK	3.93991660	3.00	56.00	23.7	-13.40694400	-13.00	36.00	25.00	3.19	34	B	ERI
153	4779		3.94480550	3.00	56.00	41.3	35.69194400	35.00	41.00	31.00	4.05	46	C	PER
154	4808		3.96977770	3.00	58.00	11.2	-61.49861100	-61.00	29.00	55.00	4.41	0	B	RET
155	4801		3.97388100	3.00	58.00	25.9	-24.11444400	-24.00	8.00	52.00	4.69	36	V	ERI
156	4805		3.97897210	3.00	58.00	44.3	12.39277770	12.00	23.00	34.00	3.90	35	L	TAU
157	4855		4.00641660	3.00	58.00	23.1	-62.25666600	-62.00	15.00	24.00	4.46	0	B	RET
158	4862		4.02152770	3.00	58.00	17.5	5.89361110	5.00	53.00	37.00	3.94	38	N	TAU
159	4897		4.04364440	3.00	2.00	37.3	21.88777700	21.00	59.00	14.00	4.50	37	L	PER
160	4924		4.06413880	3.00	3.00	58.1	50.25805300	50.00	15.00	29.00	4.33	47	L	PER
161	4967		4.10188100	3.00	6.00	6.7	47.62083300	47.00	37.00	15.00	4.03	48	U	PER
162	5056	BEID	4.16924990	3.00	10.00	9.3	-6.92749990	-6.00	55.00	39.00	4.14	38	0	ERI
163	5099		4.20533330	3.00	12.00	19.2	48.33222200	48.00	19.00	28.00	4.28	51	N	PER
164	5121		4.21400000	3.00	12.00	30.4	-42.37999900	-42.00	22.00	40.00	3.83	0	A	HR
165	5134		4.22719430	3.00	13.00	7.9	0.80611100	0.00	48.00	22.00	4.32	49	A	TAU
166	5138		4.22766660	3.00	13.00	39.6	-7.70611100	-7.00	42.00	22.00	4.32	49	0	ARI
167	5164		4.23283320	3.00	13.00	58.2	-62.56111000	-62.00	33.00	42.00	3.36	40	0	ARI
168	5179		4.25177770	3.00	15.00	6.4	-51.57416600	-51.00	34.00	27.00	4.36	0	B	DOE
169	5174		4.26055550	3.00	15.00	34.2	50.21138900	50.00	12.00	47.00	4.60	0	B	PER
170	5194		4.26458320	3.00	15.00	54.5	-9.38583300	-9.00	23.00	9.00	4.42	0	E	RET
171	5201		4.27613880	3.00	16.00	34.1	-33.88277700	-33.00	52.00	58.00	3.59	41	U	ERI



TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

172	5226	4+29663880	4+0	17+0	47+9	15+54444450	15+0	32+0	40+0	3+94	54 6	TAU
173	5304	4+34855550	4+0	20+0	54+8	17+46194400	17+0	27+0	43+0	3+93	61 0	TAU
174	5349	4+37866660	4+0	22+0	43+2	-34+09722100	-34+0	5+0	50+0	4+06	43 0	ERI
175	5350	4+38799990	4+0	23+0	16+8	22+21527700	22+0	12+0	55+0	4+06	45 K	TAU
176	5354	4+39102780	4+0	23+0	27+7	17+84944400	17+0	50+0	56+0	4+24	68 2	TAU
177	5370	4+40350000	4+0	24+0	12+6	22+73583300	22+0	44+0	9+0	4+40	49 0	TAU
178	5375	4+40580550	4+0	24+0	20+9	15+54027700	15+0	32+0	25+0	4+60	71 0	TAU
179	5430	4+44283320	4+0	26+0	34+2	19+10416600	19+0	6+0	15+0	3+63	74 E	TAU
180	5433	4+44286100	4+0	26+0	34+2	15+80583320	15+0	53+0	9+0	4+04	77 J	TAU
181	5436	4+44433320	4+0	26+0	39+6	15+79472210	15+0	47+0	41+0	3+62	78 J	TAU
182	5558	4+53100000	4+0	31+0	51+6	14+72222200	14+0	46+0	20+0	4+75	86 M	TAU
183	5572	4+53561100	4+0	32+0	8+2	-29+83838900	-29+0	50+0	11+0	4+59	50 U	ERI
184	5600	4+55397210	4+0	33+0	14+3	-55+11694400	-55+0	7+0	1+0	3+47	0 A	DOA
185	5599	4+56213880	4+0	33+0	43+7	10+09555500	10+0	5+0	26+0	4+38	88	TAU
186	5605	4+56516660	4+0	33+0	54+6	16+44027800	16+0	26+0	25+0	1+04	87 A	TAU
187	5614	4+56980550	4+0	34+0	11+3	-30+63305500	-30+0	37+0	59+0	3+88	52 U	ERI
188	5609	4+57097220	4+0	34+0	15+5	41+19472200	41+0	11+0	41+0	4+46	58	PER
189	5617	4+57613890	4+0	34+0	34+1	-3+42277770	-3+0	25+0	22+0	4+12	48 M	ERI
190	5645	4+60330550	4+0	36+0	11+9	12+42222100	12+0	26+0	32+0	4+30	90	TAU
191	5657	4+60961100	4+0	36+0	34+6	-14+37111110	-14+0	22+0	16+0	3+98	53	ERI
192	5695	4+64849990	4+0	38+0	54+6	-19+73750000	-19+0	44+0	15+0	4+54	54	ERI
193	5708	4+65719940	4+0	39+0	25+9	-41+92972200	-41+0	55+0	47+0	4+52	0 A	CAE
194	5716	4+66902770	4+0	40+0	8+5	22+89138000	22+0	53+0	29+0	4+33	94 Y	TAU
195	5796	4+72916660	4+0	43+0	45+0	-3+31750000	-3+0	19+0	3+0	4+18	57 M	ERI
196	5875	4+7987220	4+0	47+0	56+3	6+90166670	6+0	54+0	6+0	3+31	1 P	ORI
197	5892	4+81169440	4+0	48+0	42+1	8+84166660	8+0	50+0	40+0	4+35	2 P	ORI
198	5911	4+8223320	4+0	49+0	20+4	5+54666660	5+0	32+0	38+0	3+78	3 P	ORI
199	5924	4+84261100	4+0	50+0	33+4	6+22858200	6+0	17+0	9+0	4+38	9 A	CAM
200	5954	4+85280880	4+0	51+0	10+4	-5+51000000	-5+0	30+0	36+0	4+45	61 0	ERI
201	5978	4+8737770	4+0	52+0	25+6	2+38472220	2+0	23+0	5+0	3+90	8 P	ORI
202	5987	4+8827770	4+0	52+0	58+0	10+09666650	10+0	5+0	48+0	4+24	7 P	ORI
203	6025	4+90669440	4+0	54+0	24+1	13+46055540	13+0	27+0	38+0	4+28	9 0	ORI
204	6017	4+90788880	4+0	54+0	28+4	53+69833000	53+0	41+0	54+0	4+44	7 0	CAM
205	6029	4+9186100	4+0	54+0	42+7	33+11249900	33+0	6+0	45+0	2+90	3 1	AUR
206	6048	4+94552770	4+0	54+0	43+9	1+66166665	1+0	39+0	42+0	4+73	10 P	ORI
207	6123	4+99088880	4+0	59+0	27+2	43+72333300	43+0	44+0	24+0	3+00V	7 E	AUR
208	6137	5+00047210	5+0	6+0	1+7	41+02666600	41+0	1+0	36+0	3+90	8 2	AUR
209	6136	5+0094440	5+0	6+0	17+8	60+39361100	60+0	23+0	37+0	4+22	10 8	CAM
210	6158	5+01669440	5+0	1+0	1	21+54166600	21+0	32+0	30+0	4+70	102 1	TAU
211	6191	5+0427770	5+0	2+0	34+0	15+35494450	15+0	21+0	25+0	4+65	11	ORI
212	6212	5+05244430	5+0	3+0	8+8	-35+52999900	-35+0	31+0	48+0	4+62	0 6	CAE
213	6231	5+06630550	5+0	3+0	58+7	-22+41944400	-22+0	25+0	1+0	3+47	2 E	LEP
214	6226	5+06761110	5+0	4+0	3+4	41+18888800	41+0	11+0	20+0	3+48	10 M	AUR
215	6274	5+10213880	5+0	6+0	7+7	-5+13027770	-5+0	49+0	2+92	4+78	67 8	ERI
216	6304	5+12449990	5+0	7+0	28+2	-8+79749990	-8+0	51+0	4+34	4+34	49 L	ERI
217	6374	5+1727210	5+0	10+0	39+8	-11+80722200	-11+0	54+0	35+0	4+54	3 1	LEP
218	6382	5+18930550	5+0	11+0	21+5	-16+24983300	-16+0	14+0	45+0	3+50	5 M	LEP
219	6381	5+19099990	5+0	11+0	27+6	-2+82083300	2+0	49+0	15+0	4+64	17 M	ORI
220	6387	5+19355540	5+0	11+0	36+8	-12+98166660	-12+0	58+0	54+0	4+46	4 K	LEP
221	6410	5+21424900	5+0	12+0	51+3	-8+24083300	-8+0	14+0	27+0	1+34	19 8	ORI
222	6427	5+23500000	5+0	14+0	8+0	45+96444400	45+0	57+0	52+0	2+1	13 A	AUR
223	6480	5+26508320	5+0	15+0	54+3	-6+88083300	-6+0	52+0	51+0	3+88	20 Y	ORI
224	6531	5+29936110	5+0	17+0	57+7	-13+21166660	-13+0	42+0	44+9	4+59	6 L	LEP
225	6559	5+31588880	5+0	18+0	57+2	-21+27361100	-21+0	16+0	25+0	4+73	0 0	LEP
226	6579	5+33291660	5+0	19+0	58+5	-7+41555555	-7+0	24+0	54+0	4+65	22 0	ORI
227	6646	5+3709990	5+0	22+0	15+6	-7+83888880	-7+0	50+0	20+0	4+21	29	ORI
228	6655	5+37861100	5+0	22+0	43+0	-2+42777770	-2+0	25+0	40+0	3+44	28 M	ORI
229	6660	5+38213880	5+0	22+0	55+7	1+81583333	1+0	48+0	57+0	4+73	25	ORI

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

230	6668	BELLATRIX	5.38752780	5.0	23.0	15.1	6.31944440	4.0	19.0	10.0	1.70	24 G	ORI
231	6681	ELNATH	5.40130550	5.0	24.0	4.7	28.57972200	28.0	34.0	47.0	1.76	112 B	TAU
232	6713		5.41669440	5.0	25.0	.1	3.08666660	3.0	4.0	.0	4.66	30 Y	ORI
233	6762	NIHAL	5.44574990	5.0	26.0	4.47	-20.78611000	-20.0	47.0	10.0	2.96	9 B	LEP
234	6813		5.48183330	5.0	28.0	54.6	5.92277770	5.0	55.0	22.0	4.32	32	ORI
235	6846		5.49947220	5.0	29.0	58.1	-35.49527700	-35.0	29.0	43.0	3.92	0 E	OL
236	6841		5.50264460	5.0	30.0	9.4	18.54972200	18.0	34.0	11.0	4.70	119	Y U
237	6847	MINTAKA	5.50361100	5.0	30.0	13.0	-3.23411100	0.0	19.0	25.0	2.44	34 D	ORI
238	6850		5.50394430	5.0	30.0	14.2	-7.32583330	-7.0	19.0	33.0	4.64	36 U	ORI
239	6875	ARNEB	5.51975000	5.0	31.0	11.1	-17.84611000	-17.0	50.0	46.0	2.69	11 A	LEP
240	6907		5.54830550	5.0	32.0	53.9	9.44750000	9.0	28.0	3.0	4.53	37 V	ORI
241	6915	HEKA	5.55347220	5.0	33.0	12.5	9.91222220	9.0	54.0	44.0	3.66	39 L	ORI
242	6944		5.55530550	5.0	33.0	19.1	-62.51250000	-62.0	30.0	45.0	4.00V	0 B	DOR
243	6926		5.55555540	5.0	33.0	20.0	-6.02388890	-6.0	1.0	26.0	4.67	0	ORI
244	6934		5.56097220	5.0	33.0	34.5	-4.85999990	-4.0	51.0	36.0	4.65	42	ORI
245	6937	MATYSA	5.56199990	5.0	33.0	43.2	-5.93138890	-5.0	55.0	53.0	2.87	44 I	ORI
246	6960	ALNILAM	5.57394440	5.0	34.0	24.2	-1.22277777	-1.0	13.0	22.0	1.75	46 E	ORI
247	6972		5.58302780	5.0	34.0	58.9	9.27305560	9.0	16.0	23.0	4.39	40 V	ORI
248	6985		5.59252780	5.0	35.0	33.1	21.12277700	21.0	7.0	22.0	3.00	123 Z	TAU
249	7031		5.61647220	5.0	36.0	59.3	-2.61888880	-2.0	37.0	8.0	3.78	48 S	ORI
250	7092		5.62227770	5.0	37.0	20.2	4.10305550	4.0	6.0	11.0	4.54	47 W	ORI
251	7078	PHAKT	5.63964460	5.0	38.0	23.8	-34.09164400	-34.0	5.0	30.0	2.75	0 A	COL
252	7089	ALNITAK	5.64981110	5.0	38.0	59.5	-1.95972221	-1.0	57.0	35.0	2.05	50 Z	ORI
253	7197		5.71672220	5.0	40.0	.2	-22.45861100	-22.0	27.0	31.0	3.80	13 G	LEP
254	7246		5.74516660	5.0	40.0	42.6	-65.74861000	-65.0	44.0	55.0	4.52	0 D	DOR
255	7247		5.75613880	5.0	45.0	22.1	-14.83388870	-14.0	50.0	2.0	3.67	14 Z	LEP
256	7287	SAIPH	5.7824990	5.0	46.0	5.7	-9.68083320	-9.0	40.0	51.0	2.20	53 K	ORI
257	7287		5.77425000	5.0	46.0	29.3	-51.07861100	-51.0	4.0	43.0	3.94	0 B	PIC
258	7277		5.77913890	5.0	46.0	49.9	39.17111100	39.0	10.0	16.0	4.64	29 Y	AUR
259	7334		5.81772220	5.0	46.0	3.8	39.14027700	39.0	8.0	25.0	4.18	32 M	AUR
260	7353		5.81983330	5.0	49.0	11.4	-56.17472200	-56.0	10.0	29.0	4.38	0 G	PIC
261	7364		5.82875000	5.0	49.0	43.5	-35.76055500	-36.0	46.0	50.0	3.22	0 B	COL
262	7362		5.83024990	5.0	49.0	48.9	-20.88083300	-20.0	52.0	51.0	3.90	15 D	LEP
263	7389		5.85211110	5.0	51.0	7.6	27.60555500	27.0	36.0	20.0	4.54	136	TAU
264	7419		5.87180550	5.0	52.0	18.5	20.27138800	20.0	16.0	17.0	4.62	54 X	ORI
266	7477	BETELGEUSE	5.89719440	5.0	53.0	16.4	7.40194440	7.0	24.0	7.0	100V	58 A	ORI
267	7492		5.91350000	5.0	53.0	49.9	-43.10027700	-43.0	6.0	1.0	4.53	0	PIC
268	7536		5.93824990	5.0	56.0	48.6	-14.17277760	-14.0	10.0	22.0	3.77	16 M	LEP
269	7521		5.94408330	5.0	56.0	17.7	-35.28611100	-35.0	17.0	10.0	4.36	0 G	COL
270	7543	MEMKALINAN	5.94933320	5.0	56.0	38.7	54.28416600	54.0	17.0	3.0	3.88	33 D	AUR
271	7557		5.95555550	5.0	57.0	20.0	44.94583300	44.0	54.0	45.0	2.07	34 B	AUR
272	7554		5.95561100	5.0	57.0	20.2	37.21194400	37.0	12.0	43.0	2.71	37 J	AUR
273	7591		5.96788880	5.0	58.0	4.4	45.93555500	45.0	56.0	8.0	4.59	35 P	AUR
274	7587		5.97172220	5.0	58.0	18.2	-42.81638700	-42.0	48.0	59.0	4.03	0 M	COL
275	7635		6.00761110	6.0	1.0	27.4	-3.07416660	-3.0	4.0	27.0	4.68	0 I	ORI
276	7675		6.03066670	6.0	1.0	50.4	20.14083300	20.0	8.0	56.0	4.19	61 M	ORI
277	7676		6.03319440	6.0	1.0	59.5	23.26694400	23.0	16.0	1.0	4.30	62 X	ORI
278	7742		6.07616660	6.0	4.0	34.2	-14.93083300	-14.0	55.0	51.0	4.67	18 J	LEP
279	7772		6.0928890	6.0	5.0	34.4	14.77416660	14.0	40.0	27.0	4.40	67 M	ORI
280	7889	TEJAT PRIOR	6.16583330	6.0	9.0	57.0	18.21833320	18.0	13.0	6.0	4.35	70 C	ORI
281	7889		6.21274990	6.0	12.0	45.9	22.51861100	22.0	31.0	7.0	3.00V	7 M	LEM
282	7981		6.21913890	6.0	13.0	8.9	29.51277700	29.0	30.0	46.0	4.45	44 K	AUR
283	7986		6.21913890	6.0	13.0	8.9	-6.26277770	-6.0	15.0	46.0	4.09	5 G	MON
284	8020		6.24988880	6.0	14.0	59.4	69.33527700	69.0	20.0	7.0	4.73	22	CAM
285	8042		6.25508320	6.0	15.0	18.3	-35.12805500	-35.0	7.0	41.0	4.51	0 K	COL
286	8068		6.27561110	6.0	16.0	32.2	59.02611000	59.0	1.0	34.0	4.42	2	LYN
287	8170	FURUD	6.31613880	6.0	18.0	58.1	-30.04666600	-30.0	2.0	48.0	3.10	1 Z	CMA

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

288	8214		6.34722220	6.0	20.0	50.6	-33.41777700	25.0	4.0	3.98	3 0	COL
289	8208	TEJAT POSTERIOR	6.34738880	6.0	20.0	50.6	22.53333300	32.0	0	3.19	13 M	GEM
290	8223	MIRZAH	6.35263880	6.0	21.0	9.5	-17.93722100	56.0	14.0	1.99	2 0	CHA
291	8210		6.36522220	6.0	21.0	54.8	4.61194400	36.0	43.0	4.48	6 E	HON
292	8302	CANOPUS	6.36625000	6.0	23.0	10.5	-52.67411100	40.0	34.0	0.86	0 A	CAR
293	8410		6.44783330	6.0	26.0	53.2	-32.55694400	33.0	25.0	4.40	0 L	CHA
294	8394		6.44808320	6.0	26.0	53.1	20.23583300	20.0	9.0	4.06	18 N	GEM
295	8413		6.45197220	6.0	27.0	7.1	-7.00716660	7.0	33.0	4.64	11 0	HON
296	8476		6.50661100	6.0	30.0	23.8	-23.39194400	23.0	31.0	4.35	4 C	CHA
297	8506		6.51686110	6.0	31.0	17	7.35999990	7.0	21.0	4.50	13	HON
298	8577		6.5590540	6.0	33.0	35.3	-42.93583300	23.0	5.0	4.54	5 C	CHA
299	8604		6.5700560	6.0	34.0	12.2	-52.94638900	52.0	47.0	4.44	0	CAR
300	8624		6.5859440	6.0	35.0	9.4	-19.22500000	19.0	30.0	4.14	7 N	CHA
301	8633	ALHENA	6.59483330	6.0	35.0	41.4	16.43055500	16.0	25.0	1.93	24 6	GEM
302	8640		6.60583330	6.0	36.0	21.0	-18.20583300	16.0	21.0	4.65	8 N	CHA
303	8475		6.61149990	6.0	36.0	41.4	-43.16444400	43.0	9.0	3.18	0 N	PUP
304	8750		6.65083330	6.0	37.0	3.0	9.92772220	9.0	55.0	4.68	15	HON
305	8786	HEBSUTA	6.65633320	6.0	41.0	40.8	25.16749900	25.0	10.0	3.18	27 E	GEM
306	8793		6.70225000	6.0	42.0	19	13.26472210	13.0	15.0	4.65	30	GEM
307	8823		6.72208320	6.0	43.0	19.6	12.9372220	12.0	54.0	3.44	31 C	GEM
308	8833	SIRIUS	6.7247770	6.0	43.0	36.4	-16.66666600	16.0	40.0	0	9 A	CHA
309	8892		6.74724890	6.0	46.0	2.1	2.45194400	2.0	27.0	4.70	18	HON
310	8991		6.75722210	6.0	47.0	50.0	-31.90361000	61.0	56.0	3.30	0 A	PIC
311	8976		6.80888880	6.0	48.0	32.0	-32.46694400	32.0	26.0	3.78	13 6	CHA
312	8949		6.81777780	6.0	49.0	4.0	-50.57222200	50.0	34.0	2.83	0 Y	PUP
313	8972		6.81825000	6.0	49.0	5.7	-53.58083200	53.0	51.0	4.38	0	CAR
314	8949		6.84138880	6.0	50.0	28.0	34.00527800	34.0	0	3.64	34 J	GEM
315	9034		6.86724990	6.0	52.0	2.1	-20.17972200	20.0	10.0	4.66	18	CHA
316	9051		6.87605540	6.0	52.0	33.8	-11.99361120	11.0	59.0	4.25	14 J	CHA
317	9049		6.87783320	6.0	52.0	40.2	13.22361100	13.0	25.0	4.70	38	GEM
318	9059		6.8797210	6.0	52.0	40.7	-24.13916600	24.0	8.0	4.12	16 0	CHA
319	9094		6.90175000	6.0	54.0	6.3	-20.09055500	20.0	5.0	4.62	18 0	CHA
320	9082		6.90419440	6.0	54.0	15.1	58.47083300	58.0	28.0	4.54	18	LYN
321	9107		6.90958330	6.0	56.0	34.5	-17.00750000	17.0	0	4.39	20 1	CHA
322	9073		6.91652770	6.0	56.0	59.5	77.02583300	79.0	1.0	4.75	21	CAM
323	9108	ADHARA	6.95416670	6.0	57.0	18.0	-28.92333300	28.0	55.0	1.63	21 6	CHA
324	9274		7.00541660	7.0	1.0	19.5	-27.88361100	27.0	53.0	3.48	22 8	CHA
325	9307		7.02605550	7.0	1.0	33.8	-23.78111000	23.0	46.0	3.12	24 8	CHA
326	9313	HEKUDA	7.03388880	7.0	2.0	2.0	20.62333300	20.0	37.0	3.90	43 2	GEM
327	9320	MULIPHEIN	7.03624990	7.0	2.0	10.5	-15.58027770	16.0	34.0	4.07	23 6	CHA
328	9493	BEZEN	7.11613880	7.0	6.0	58.1	-26.33666600	26.0	20.0	1.98	25 0	CHA
329	9484		7.14855550	7.0	8.0	54.8	30.30416600	30.0	18.0	4.48	46 Y	GEM
330	9514		7.15086110	7.0	9.0	3.1	-70.44222100	70.0	32.0	3.87	0 6	VOL
331	9589		7.16794440	7.0	10.0	4.6	-4.33333333	0	46.0	4.09	22 0	HON
332	9589		7.19269440	7.0	11.0	33.7	-46.69999900	46.0	22.0	4.47	0	PUP
333	9608		7.20783330	7.0	12.0	28.2	-44.58194400	44.0	34.0	4.50	0	PUP
334	9608		7.21375000	7.0	13.0	49.5	-26.29111000	26.0	17.0	4.64	27	CHA
335	9625		7.22316660	7.0	13.0	23.4	-24.71083300	24.0	39.0	3.63	20 8	CHA
336	9706		7.28511110	7.0	15.0	54.4	-37.03361100	37.0	1.0	2.74	0 P	PUP
337	9701		7.28805550	7.0	16.0	5.0	16.60499900	16.0	36.0	3.65	54 L	GEM
338	9747		7.2880890	7.0	16.0	51.2	-67.89332200	67.0	53.0	4.02	0 0	VOL
339	9733		7.28934100	7.0	17.0	3.7	-36.66916600	36.0	9.0	4.48	0 U	PUP
340	9726		7.28781110	7.0	17.0	15.4	-24.88944400	24.0	22.0	4.40	30 Y	CHA
341	9755	MASAT	7.30058330	7.0	18.0	2.1	-22.04833300	22.0	2.0	3.51	58 0	GEM
342	9886	ALUDRA	7.37850000	7.0	22.0	42.6	-29.23388900	29.0	19.0	2.43	31 M	CHA
343	9897		7.39258330	7.0	23.0	33.3	-27.86916600	27.0	52.0	3.89	40 1	GEM
344	9909		7.40130550	7.0	24.0	4.7	49.28305500	49.0	16.0	4.45	21	LYN
345	9947	GOMEISA	7.42088880	7.0	25.0	15.2	8.36111110	8.0	40.0	3.09	3	B

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

346	9974	7.43763080	7.0	28.0	15.5	8.99777770	8.0	59.0	52.0	4.60	4	6	CHI
347	9977	7.44772210	7.0	28.0	51.8	31.85555500	31.0	51.0	20.0	4.19	62	R	GEM
348	10040	7.46866660	7.0	28.0	7.2	-43.22972100	-43.0	13.0	47.0	3.27	0	3	PUP
349	10120	7.53947210	7.0	32.0	22.1	31.96638800	31.0	57.0	59.0	1.58	66	A	GEM
350	10134	7.54255550	7.0	32.0	37.2	-22.21944400	-22.0	17.0	10.0	4.52	108	A	PUP
351	10167	7.56280550	7.0	33.0	46.1	26.97500000	26.0	58.0	30.0	4.22	69	U	GEM
352	10178	7.56624990	7.0	33.0	58.6	-28.29111100	-28.0	28.0	28.0	4.55	0	0	PUP
353	10246	7.60119440	7.0	38.0	4.3	-34.88888800	-34.0	53.0	20.0	4.62	0	0	PUP
354	10286	7.61405550	7.0	38.0	50.6	-25.28444400	-25.0	17.0	4.0	4.84	0	0	PUP
355	10281	7.62311100	7.0	37.0	23.2	-26.72111100	-26.0	43.0	16.0	4.50	0	K	PUP
356	10277	7.62499990	7.0	38.0	28.2	5.31583330	5.0	18.0	57.0	4.8	10	A	CHI
357	10345	7.6595320	7.0	37.0	34.6	-9.46833330	-9.0	28.0	6.0	4.07	26	A	MON
358	10373	7.68544440	7.0	41.0	7.6	28.96972100	28.0	59.0	11.0	4.26	75	S	GEM
359	10444	7.70438890	7.0	42.0	15.8	-22.52249700	-22.0	31.0	21.0	3.89	0	3	VOL
360	10403	7.70561110	7.0	42.0	20.2	24.48333300	24.0	27.0	.0	3.88	77	K	GEM
361	10417	7.70669450	7.0	42.0	24.1	-28.87027700	-28.0	52.0	13.0	4.10	3	3	PUP
362	10438	7.71961110	7.0	43.0	10.6	28.11222200	28.0	6.0	44.0	1.21	78	B	GEM
363	10482	7.73344440	7.0	44.0	.4	-37.88277700	-37.0	58.0	58.0	3.72	0	0	PUP
364	10532	7.77718660	7.0	48.0	37.8	-25.89916700	-26.0	50.0	57.0	4.59	0	0	PUP
365	10553	7.78824990	7.0	47.0	17.7	-46.98861000	-46.0	59.0	19.0	4.64	0	0	PUP
366	10562	7.79702770	7.0	47.0	49.3	-24.77083300	-24.0	46.0	15.0	3.47	7	C	PUP
367	10576	7.80286100	7.0	48.0	10.3	-46.28444400	-46.0	17.0	4.0	4.25	0	0	PUP
368	10655	7.85022210	7.0	51.0	.8	-40.48472200	-40.0	27.0	5.0	3.76	0	A	PUP
369	10661	7.85675000	7.0	51.0	24.3	-38.77138800	-38.0	46.0	17.0	4.53	0	0	PUP
370	10689	7.87122210	7.0	52.0	14.4	-48.01111100	-48.0	.0	40.0	4.32	0	0	PUP
371	10756	7.92255550	7.0	55.0	21.2	-22.78555500	-22.0	47.0	8.0	4.35	11	7	PUP
372	10770	7.93147220	7.0	55.0	53.3	-22.88777700	-22.0	53.0	16.0	3.60	0	X	CAR
373	10802	7.95388880	7.0	57.0	14.0	-49.14916600	-49.0	8.0	57.0	4.004	0	0	PUP
374	10825	7.97163890	7.0	58.0	17.9	-18.30222200	-18.0	18.0	8.0	4.64	232	0	PUP
375	10891	8.00741670	8.0	.0	28.7	2.43194440	3.0	25.0	55.0	4.52	0	0	CHI
376	10947	8.03922210	8.0	2.0	21.2	-39.90341000	-39.0	54.0	13.0	2.27	0	3	PUP
377	11034	8.1008870	8.0	6.0	3.2	-24.20250000	-24.0	12.0	12.0	2.88	15	R	PUP
378	11051	8.11391050	8.0	6.0	50.1	-2.88053550	-2.0	52.0	50.0	4.41	29	Z	MON
379	11071	8.12438870	8.0	7.0	27.8	-19.14138800	-19.0	8.0	29.0	4.34	16	E	VOL
380	11078	8.13041650	8.0	7.0	49.5	-48.51416500	-48.0	30.0	51.0	4.46	0	0	VOL
381	11105	8.1408880	8.0	8.0	27.2	-47.23277800	-47.0	13.0	58.0	1.90	0	6	VEL
382	11134	8.16049990	8.0	9.0	37.8	-12.82194440	-12.0	49.0	19.0	4.68	19	0	PUP
383	11149	8.16844440	8.0	10.0	6.4	-39.51333300	-39.0	30.0	48.0	4.43	0	0	PUP
384	11215	8.21341660	8.0	12.0	48.3	-40.24027700	-40.0	19.0	25.0	4.43	0	0	PUP
385	11254	8.24363880	8.0	14.0	37.1	9.29472220	9.0	17.0	41.0	3.76	17	B	CNC
386	11343	8.28741660	8.0	17.0	14.7	-36.55000000	-36.0	33.0	.0	4.43	0	0	PUP
387	11419	8.32433320	8.0	19.0	27.6	-76.80972100	-76.0	48.0	35.0	4.08	0	A	CHA
388	11401	8.34077770	8.0	20.0	26.8	43.30194400	43.0	18.0	7.0	4.43	31	18	LYN
389	11481	8.36211100	8.0	21.0	43.6	-77.37222200	-77.0	22.0	20.0	4.26	0	J	CHA
390	11463	8.36327770	8.0	21.0	47.8	-59.39638800	-59.0	23.0	47.0	1.74	0	E	CAR
391	11499	8.39852770	8.0	23.0	54.7	-3.79111100	-3.0	47.0	28.0	3.95	30	7	MON
392	11567	8.4272210	8.0	23.0	21.8	-66.01972100	-66.0	1.0	11.0	3.65	0	0	VOL
393	11573	8.45619430	8.0	27.0	22.3	60.83694400	60.0	50.0	13.0	3.47	1	0	UHA
394	11823	8.59474990	8.0	35.0	48.3	5.82494440	5.0	49.0	37.0	4.18	4	0	HVA
395	11852	8.60686100	8.0	36.0	24.7	-42.86611100	-42.0	51.0	58.0	4.18	0	0	VEL
396	11886	8.61547210	8.0	38.0	55.7	3.46527780	3.0	27.0	55.0	4.54	5	8	HTA
397	11923	8.64552770	8.0	38.0	43.9	-35.18305500	-35.0	10.0	59.0	4.04	0	0	PTX
398	11933	8.65483320	8.0	39.0	17.4	-52.9722200	-52.0	40.0	50.0	3.68	0	0	VEL
399	11951	8.6572210	8.0	39.0	27.8	-46.52361100	-46.0	31.0	25.0	4.06	53	0	VEL
400	11964	8.6648330	8.0	39.0	50.7	-59.4583300	-59.0	38.0	9.0	4.42	0	0	CAR
401	11982	8.6872210	8.0	41.0	15.8	21.5955500	21.0	35.0	44.0	4.73	43	0	CNC
402	11987	8.68994440	8.0	41.0	23.8	3.52527770	3.0	31.0	31.0	4.34	7	H	HVA
403	12006	8.69924980	8.0	41.0	57.3	-7.10666660	-7.0	40.0	24.0	4.70	31	0	MON

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

404	12018	8-70308320	8.0	42.0	11.1	-33.05944400	-33.0	3.0	34.0	3.70	0.4	PYA
405	12022	8-71163800	8.0	42.0	41.9	18.28416600	18.0	17.0	3.0	4.17	47.0	CNC
406	12050	8-71913870	8.0	43.0	8.9	-42.52166600	-42.0	31.0	18.0	4.12	0	VEL
407	12069	8-72894330	8.0	43.0	44.2	-54.57972100	-54.0	34.0	47.0	2.01	0.0	VEL
408	12083	8-74305540	8.0	44.0	35.0	28.88916700	28.0	53.0	21.0	4.20	48.1	CNC
409	12097	8-74536100	8.0	44.0	43.3	-13.41888870	-13.0	25.0	8.0	4.44	12	HYA
410	12109	8-74733320	8.0	44.0	50.4	-45.91277700	-45.0	54.0	46.0	4.09	0	VEL
411	12102	8-74872210	8.0	44.0	55.4	6.54833330	6.0	32.0	54.0	3.48	11.8	HYA
412	12138	8-76341660	8.0	45.0	48.3	-56.64055500	-56.0	38.0	24.0	4.63	0	CAR
413	12198	8-77633330	8.0	46.0	34.8	5.98472220	5.0	58.0	65.0	4.42	13.8	HYA
414	12216	8-81744440	8.0	46.0	2.8	-27.57916600	-27.0	34.0	45.0	4.19	0.6	PYA
415	12327	8-89241660	8.0	53.0	32.7	6.07972220	6.0	4.0	47.0	3.30	16.2	HYA
416	12359	8-90427770	8.0	54.0	15.4	-60.51027800	-60.0	30.0	37.0	3.98	0	CAR
417	12406	ACUBENS SERTAN 8-94291650	8.0	56.0	34.5	11.99416670	11.0	59.0	39.0	4.27	65.4	CNC
418	12407	8-94699990	8.0	56.0	49.2	48.18027700	48.0	10.0	49.0	3.12	9.1	UMA
419	12434	8-97291650	8.0	58.0	22.5	41.92249900	41.0	55.0	21.0	4.09	10	UMA
420	12451	8-97949420	8.0	58.0	46.9	-41.11666600	-41.0	7.0	0	4.42	91	VEL
421	12503	9-0204990	9.0	1.0	14.7	47.28411100	47.0	17.0	46.0	3.68	12.8	UMA
422	12532	9-03163890	9.0	1.0	53.9	-66.25611100	-66.0	15.0	22.0	4.18	0.4	VEL
423	12545	9-04908320	9.0	2.0	56.7	-46.95777700	-46.0	57.0	28.0	3.69	0	VEL
424	12565	9-07180550	9.0	4.0	18.5	38.59333300	38.0	35.0	36.0	4.71	0	LYN
425	12595	9-08452760	9.0	5.0	4.3	-72.46194300	-72.0	27.0	43.0	4.50	0	CAR
426	12604	9-1068880	9.0	6.0	24.8	51.74232100	51.0	44.0	50.0	4.54	15	UMA
427	12823	SUMAIL ALSUMAIL 9-1117770	9.0	6.0	42.4	-43.29055500	-43.0	17.0	24.0	2.22	0.4	VEL
428	12896	9-13422220	9.0	8.0	3.2	63.65749900	63.0	39.0	27.0	9.74	14.7	UMA
429	12896	9-16741660	9.0	10.0	2.7	-58.82305500	-58.0	49.0	23.0	3.56	0	CAR
430	12707	9-1749990	9.0	10.0	29.1	-62.17305500	-62.0	10.0	23.0	4.18	0	CAR
431	12743	9-20908320	9.0	12.0	32.7	2.4627770	2.0	27.0	46.0	3.84	22.2	HYA
432	12744	MIAPLACIUS 9-21374990	9.0	12.0	49.5	-69.57305500	-69.0	34.0	23.0	1.80	0.8	CAR
433	12787	9-23916650	9.0	14.0	21.0	-37.26866600	-37.0	16.0	0	4.70	0	VEL
434	12813	9-25358320	9.0	15.0	12.9	-57.39449300	-57.0	23.0	40.0	4.18	0	CAR
435	12831	9-26922220	9.0	16.0	9.2	-59.12805500	-59.0	7.0	41.0	2.25	0.1	CAR
436	12830	9-27786100	9.0	16.0	40.3	36.95194400	36.0	57.0	7.0	3.82	38	LYN
437	12880	9-31547220	9.0	18.0	55.7	34.54166700	34.0	32.0	30.0	3.30	40.4	LYN
438	12938	9-35047210	9.0	21.0	1.7	-54.86083300	-54.0	51.0	39.0	2.63	0.8	VEL
439	12772	9-37699990	9.0	22.0	37.2	26.33388900	26.0	20.0	2.0	4.61	1.8	LEO
440	13044	ALPHARD COR-HYDRAE 9-43111100	9.0	25.0	52.0	-8.50611110	-8.0	30.0	22.0	2.16	30.4	HYA
441	13091	9-46330550	9.0	27.0	47.9	-35.79777700	-35.0	47.0	52.0	4.64	0.8	ANT
442	13109	9-47963320	9.0	28.0	47.4	63.21611000	63.0	12.0	58.0	3.75	23	UMA
443	13140	9-48866660	9.0	29.0	19.2	-40.31277700	-40.0	18.0	46.0	3.64	0.7	VEL
444	13143	9-49544430	9.0	29.0	43.6	23.12333300	23.0	7.0	24.0	4.48	4.4	LEO
445	13160	9-50261090	9.0	30.0	9.4	-56.87944400	-56.0	52.0	46.0	3.00	0	VEL
446	13153	9-50330550	9.0	30.0	11.9	-1.02972221	-1.0	1.0	47.0	4.50	32.7	HYA
447	13157	9-5087760	9.0	30.0	31.4	51.83777700	51.0	50.0	16.0	3.26	25.2	CAR
448	13192	9-52274990	9.0	31.0	21.9	-62.63311100	-62.0	38.0	1.0	4.00	0	CAR
449	13171	9-52366670	9.0	31.0	25.2	69.98585400	69.0	59.0	8.0	4.57	24	UMA
450	13203	9-53474990	9.0	32.0	5.1	36.55388900	36.0	33.0	14.0	4.62	10	LMI
451	13174	9-53741660	9.0	32.0	14.7	81.48332000	81.0	29.0	0	4.58	1	DRA
452	13212	9-54041110	9.0	32.0	24.2	52.20805500	52.0	12.0	29.0	4.65	24	UMA
453	13246	9-55713880	9.0	33.0	25.7	-59.07305500	-59.0	4.0	23.0	4.20	0	CAR
454	13293	9-57288870	9.0	35.0	34.4	-49.19777700	-49.0	11.0	52.0	4.49	0	VEL
455	13341	9-63447210	9.0	38.0	4.1	-98.305555	-98.0	58.0	59.0	4.10	35.1	HYA
456	13355	9-63966660	9.0	38.0	22.8	-61.16916600	-61.0	10.0	9.0	4.47	0	CAR
457	13366	9-6547210	9.0	39.0	17.0	10.0522220	10.0	3.0	8.0	3.74	14.0	LEO
458	13373	9-66141660	9.0	39.0	41.1	-23.43166600	-23.0	25.0	54.0	4.74	0	HYA
459	13443	RAS-ELASED AUSTR. 9-7313870	9.0	43.0	52.1	23.93611100	23.0	56.0	10.0	3.12	17.8	LEO
460	13462	9-73888310	9.0	44.0	17.1	-62.34583300	-62.0	20.0	45.0	4.00	0	CAR
461	13504	9-77047220	9.0	46.0	13.7	-64.90916600	-64.0	54.0	33.0	3.08	0	CAR

HYA ALFARU

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

462 13540	9.60861110	9.0	48.0	31.0	59.20444400	50.0	12.0	16.0	3.89	29 U	UMA
463 13559	9.82894440	9.0	49.0	44.2	54.22888800	54.0	13.0	44.0	4.54	30 V	UMA
464 13570	9.82898890	9.0	50.0	47.6	-14.60166660	-14.0	40.0	54.0	4.29	39 U	MYA
465 13587	9.83872210	9.0	50.0	19.4	-46.30355500	-46.0	22.0	59.0	4.56	0	VEL
466 13590	9.84627740	9.0	50.0	40.6	26.17249900	24.0	10.0	21.0	4.10	24 M	LEO
467 13711	9.92719430	9.0	55.0	37.9	-54.40055500	-54.0	24.0	2.0	3.70	0 V	VEL
468 13861	10.05697210	10.0	3.0	25.1	-12.89444430	-12.0	53.0	40.0	4.72	40 U	MYA
469 13896	10.08949980	10.0	5.0	22.2	35.41611100	36.0	24.0	58.0	4.97	21	LMJ
470 13899	10.09044420	10.0	5.0	25.6	16.93388800	16.0	56.0	2.0	3.58	30 M	LEO
471 13911	10.10080530	10.0	6.0	2.9	10.16972210	10.0	10.0	11.0	4.58	31	LEO
472 13916	10.10244430	10.0	6.0	8.8	-20.00000000	0.0	12.0	0.0	4.50	15 A	SEX
473 13926	KALB10.10849980	10.0	6.0	30.6	12.13888880	12.0	8.0	20.0	1.34	32 A	LEO
474 13982	10.14799980	10.0	8.0	52.8	-12.18053550	-12.0	10.0	50.0	3.83	41 L	MYA
475 14074	10.21516650	10.0	12.0	54.6	-69.86388800	-69.0	51.0	50.0	3.56	0 W	CAR
476 14076	10.22105530	10.0	13.0	15.8	-41.94833300	-41.0	54.0	54.0	4.09	0	VEL
477 14107	ADHAFAERA	10.0	14.0	44.8	23.59222200	23.0	35.0	32.0	3.65	36 Z	LEO
478 14113	TANIA BOR.	10.0	14.0	59.6	43.08972200	43.0	5.0	23.0	3.52	33 L	UMA
479 14133	10.28519430	10.0	15.0	54.7	-61.15694400	-61.0	9.0	25.0	3.44	187	CAR
480 14177	ALGIEBA	10.0	18.0	2.7	20.01916600	20.0	1.0	9.0	2.61	41 6	LEO
481 14185	10.30491650	10.0	17.0	17.7	-54.85333300	-54.0	51.0	12.0	4.58	0	VEL
482 14220	10.32677770	10.0	19.0	34.4	-55.86638800	-56.0	51.0	59.0	4.65	0	VEL
483 14232	TANIA AUSTR.	10.0	20.0	15.0	41.67411100	41.0	40.0	34.0	3.21	34 M	UMA
484 14323	10.39511100	10.0	23.0	42.4	-73.85333300	-73.0	51.0	12.0	4.08	0	CAR
485 14326	10.40661110	10.0	24.0	23.8	-16.65694400	-16.0	39.0	25.0	4.06	42 M	MYA
486 14352	10.42580540	10.0	25.0	44.3	-30.88916600	-30.0	53.0	21.0	4.10	0 A	ANT
487 14358	10.43108310	10.0	25.0	51.9	36.88722200	36.0	53.0	14.0	4.41	31 B	LMI
488 14388	10.44316650	10.0	26.0	35.4	-58.56027700	-59.0	33.0	37.0	4.08	0	CAR
489 14489	10.51291640	10.0	30.0	44.8	-61.50500000	-61.0	30.0	10.0	3.58	0	CAR
490 14487	10.51616640	10.0	30.0	58.2	9.48722220	9.0	29.0	14.0	3.85	47 R	LEO
491 14570	10.57063880	10.0	34.0	14.3	-57.37411100	-57.0	22.0	34.0	4.54	0 2	CAR
492 14604	10.58452740	10.0	35.0	40.3	-78.42411000	-78.0	25.0	34.0	4.10	0 8	CMA
493 14614	10.59711100	10.0	35.0	49.6	-48.04361100	-48.0	2.0	37.0	4.06	0	VEL
494 14647	10.62358320	10.0	37.0	24.9	-59.00055500	-59.0	0	2.0	4.73	0	CAR
495 14662	10.63183320	10.0	37.0	54.6	-35.42083300	-35.0	25.0	15.0	4.25	0	VEL
496 14755	10.69505540	10.0	41.0	42.2	-64.21083200	-64.0	12.0	39.0	3.03	0 J	CAR
497 14762	10.70333330	10.0	42.0	12.0	-60.38277700	-60.0	22.0	58.0	4.49	0	CAR
498 14842	10.75430540	10.0	45.0	15.5	-49.23472200	-49.0	14.0	5.0	2.84	0 M	VEL
499 14843	10.75799970	10.0	45.0	28.8	-80.35555600	-80.0	21.0	20.0	4.62	0 D	CMA
500 14898	10.79827770	10.0	47.0	53.8	-16.01000000	-16.0	0	36.0	3.32	0 N	MYA
501 14961	10.85599990	10.0	51.0	21.6	34.40388800	34.0	24.0	14.0	3.92	46 0	LMI
502 14980	10.86774980	10.0	52.0	34.9	-58.66722200	-58.0	40.0	2.0	3.88	0	CAR
503 15014	10.89536100	10.0	53.0	43.3	24.93666600	24.0	56.0	12.0	4.51	54	LEO
504 15047	10.91819400	10.0	55.0	54.5	-34.94944400	-34.0	56.0	58.0	4.70	0 I	ANT
505 15106	ALKE8	10.0	58.0	44.4	-18.11194400	-18.0	6.0	43.0	4.20	7 A	CRT
506 15118	10.97572210	10.0	58.0	32.6	-42.03777700	-42.0	2.0	16.0	4.56	239	VEL
507 15145	MERAK	10.0	59.0	44.5	56.57027700	56.0	34.0	13.0	2.44	48 B	UMA
508 15162	11.00772220	11.0	0	27.8	20.36777700	20.0	22.0	4.0	4.42	60	LEO
509 15185	DUBHE	11.0	1.0	35.0	61.94027700	61.0	56.0	25.0	1.95	50 A	UMA
510 15235	11.05352770	11.0	3.0	12.7	7.52555550	7.0	31.0	32.0	4.66	63 A	LEO
511 15329	11.11813870	11.0	7.0	54.3	-58.78527700	-58.0	47.0	7.0	4.02	260	CAR
512 15340	11.12838880	11.0	7.0	42.2	44.68861100	44.0	41.0	19.0	3.15	0 V	UMA
513 15385	11.14555540	11.0	9.0	56.0	-22.63444400	-22.0	38.0	4.0	4.52	11 B	CRT
514 15415	ZOSMA	11.0	11.0	54.5	-60.12494400	-60.0	7.0	37.0	4.73	0	CAR
515 15436	ZOSMA	11.0	12.0	15.0	20.71555500	20.0	42.0	56.0	2.58	68 0	LEO
516 15441	COXA	11.0	12.0	24.3	15.62111100	15.0	37.0	16.0	3.41	70 J	LEO
517 15511	11.24802500	11.0	14.0	52.9	-3.45999990	-3.0	27.0	36.0	4.58	74 V	LEO
518 15537	ALULA-AUSTR.	11.0	16.0	19.2	31.72638900	31.0	43.0	35.0	3.88	53 C	UMA
519 15547	ALULA-BOR.	11.0	16.0	35.5	33.28555500	33.0	17.0	8.0	3.71	54 M	UMA

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

520	15567	11.29313870	11.0	17.0	35.3	-14.58888890	-14.0	35.0	20.0	3.84	12 0	CRT
521	15600	11.32219430	11.0	19.0	19.9	6.22138890	6.0	17.0	17.0	4.13	77 5	LEO
522	15601	11.32338880	11.0	19.0	24.2	-54.29916600	-54.0	17.0	57.0	4.26	0 9	CEN
523	15652	11.36836100	11.0	22.0	6.1	10.72222220	10.0	43.0	20.0	4.03	78 1	LEO
524	15669	11.38550000	11.0	23.0	7.8	-17.49166600	-17.0	29.0	30.0	4.14	15 6	CRT
525	15799	11.48911090	11.0	29.0	20.8	69.52444300	69.0	31.0	28.0	4.06	1 1	ORA
526	15845	11.52127770	11.0	31.0	16.4	-21.66388900	-21.0	39.0	50.0	3.72	0 1	MYA
527	15899	11.56930540	11.0	34.0	9.5	-62.82611000	-62.0	49.0	34.0	3.34	0 1	CEN
528	15927	11.58594830	11.0	35.0	9.4	-4.30555555	0	37.0	50.0	4.47	92 0	LEO
529	16131	11.73238870	11.0	43.0	58.6	-66.53872100	-66.0	32.0	57.0	3.80	0 1	MUS
530	16135	11.73433320	11.0	44.0	3.6	6.72555550	6.0	43.0	32.0	4.20	3 0	VIR
531	16137	11.73600540	11.0	44.0	12.5	47.97333300	47.0	50.0	28.0	3.85	63 1	ORA
532	16147	11.74683320	11.0	44.0	48.6	-60.98388800	-60.0	59.0	2.0	4.22	65	CEN
533	16173	11.76969440	11.0	46.0	10.9	20.41333300	20.0	24.0	48.0	4.54	93	LEO
534	16176	11.77574990	11.0	49.0	32.7	-66.62027700	-66.0	37.0	13.0	4.71	0 0	MUS
535	16189	11.78791660	11.0	47.0	18.5	14.76777760	14.0	46.0	4.0	2.23	94 8	LEO
536	16201	11.79949980	11.0	47.0	58.2	-63.59388800	-63.0	35.0	38.0	4.52	0	CEN
537	16215	11.81452770	11.0	48.0	52.3	1.96194443	1.0	57.0	43.0	3.80	5 8	VIR
538	16236	11.82311090	11.0	49.0	23.2	-44.97861000	-44.0	58.0	43.0	4.71	0	CEN
539	16258	11.82524980	11.0	51.0	8.1	-33.71333300	-33.0	42.0	46.0	4.40	0	MYA
540	16268	11.86661090	11.0	51.0	58.8	53.88916600	53.0	48.0	21.0	2.54	64 6	ORA
541	16425	11.98463870	11.0	59.0	4.7	6.80944440	6.0	49.0	34.0	4.57	8 9	VIR
542	16463	12.0202770	12.0	1.0	13.9	-63.11805500	-63.0	7.0	5.0	4.98	0 0	CRU
543	16512	12.05711100	12.0	3.0	25.6	8.92722210	8.0	55.0	38.0	4.24	9 0	VIR
544	16551	12.08402770	12.0	5.0	2.5	-64.41861000	-64.0	25.0	7.0	4.30	0 0	CRU
545	16584	12.10891650	12.0	6.0	32.1	-50.52777800	-50.0	31.0	40.0	2.88	0 0	CEN
546	16586	12.11005540	12.0	6.0	38.2	-24.53388900	-24.0	33.0	2.0	4.18	1 1	CRV
547	16618	12.13869440	12.0	8.0	19.3	-22.42527800	-22.0	25.0	31.0	3.21	2 2	CRV
548	16651	12.16355550	12.0	9.0	48.8	-52.17388900	-52.0	10.0	26.0	4.20	0 0	CEN
549	16724	12.22124980	12.0	13.0	18.5	-58.55444400	-58.0	33.0	16.0	3.08	0 0	CRU
550	16736	12.22836110	12.0	13.0	42.1	57.22494400	57.0	13.0	37.0	3.44	69 0	ORA
551	16740	12.23338870	12.0	19.0	2	-17.34777700	-17.0	20.0	52.0	2.78	4 8	CRV
552	16764	12.26105540	12.0	15.0	38.8	-67.76611000	-67.0	48.0	48.0	4.16	0 0	MUS
553	16775	12.27094440	12.0	16.0	15.4	-79.11805500	-79.0	7.0	5.0	4.38	0 0	ORA
554	16785	12.27541660	12.0	16.0	31.5	-63.00888800	-63.0	48.0	32.0	4.24	0 2	ORA
555	16813	12.30188880	12.0	18.0	6.8	-4.72500000	0	28.0	21.0	4.00	18 0	VIR
556	16849	12.32430550	12.0	19.0	27.5	-60.20805500	-60.0	12.0	29.0	3.57	0 0	CRU
557	16953	12.41061110	12.0	21.0	38.2	-62.90527700	-62.0	54.0	19.0	1.00	0 1	CRU
558	16964	12.41991650	12.0	25.0	11.7	28.46277700	28.0	27.0	48.0	4.56	15 6	COM
559	16990	12.43543880	12.0	26.0	8.3	-50.03722200	-50.0	2.0	19.0	4.14	0 3	CEN
560	17029	12.46749980	12.0	28.0	3.0	-16.32083300	-16.0	19.0	15.0	3.11	7 0	CRV
561	17052	12.48686110	12.0	29.0	12.7	-56.91749900	-56.0	58.0	3.0	1.61	0 6	CRU
562	17087	12.50438870	12.0	30.0	15.8	-16.00249900	-16.0	0	9.0	4.42	8 0	CRV
563	17084	12.50588840	12.0	30.0	21.2	-71.94000000	-71.0	56.0	24.0	3.08	0 6	MUS
564	17124	12.53330540	12.0	31.0	59.9	69.98083300	69.0	58.0	51.0	4.04	5 0	ORA
565	17147	12.5372210	12.0	34.0	5.0	41.54722200	41.0	32.0	50.0	4.32	8 0	CEN
566	17133	12.54241660	12.0	32.0	32.7	-23.20333300	-23.0	12.0	12.0	2.64	9 8	CRV
567	17179	12.58461090	12.0	35.0	4.6	-68.94305500	-68.0	56.0	35.0	2.94	0 1	MUS
568	17194	12.59430530	12.0	35.0	46.7	-48.34888900	-48.0	20.0	56.0	4.02	0 5	CEN
569	17242	12.65941100	12.0	39.0	34.6	-48.76777700	-48.0	46.0	4.0	2.38	0 6	CEN
570	17270	12.68474990	12.0	39.0	53.1	-11.25777777	-11.0	15.0	28.0	2.91	29 8	VIR
571	17282	12.67738880	12.0	40.0	38.6	-48.62111100	-48.0	37.0	10.0	4.65	0	CEN
572	17339	12.72597210	12.0	43.0	33.5	-60.78944400	-60.0	47.0	22.0	4.68	0 1	CRU
573	17348	12.73524980	12.0	44.0	6.9	-67.91694400	-67.0	55.0	1.0	3.24	0 8	MUS
574	17374	12.76102750	12.0	45.0	39.7	-59.49777700	-59.0	29.0	52.0	1.50	0 8	CRU
575	17473	12.85205540	12.0	51.0	7.4	-48.75305400	-48.0	46.0	11.0	4.35	0	CEN
576	17489	12.85816640	12.0	51.0	28.4	-39.98888800	-39.0	59.0	20.0	4.34	0	CEN
577	17518	12.87491650	12.0	52.0	20.7	-56.14944400	-56.0	8.0	58.0	1.68	77 8	ORA

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

578	17512		12.87530870	12.0	52.0	31.4	-56.90833300	-56.0	59.0	18.0	4.24	O M	CRU
579	17593	AUYA	MINELAUVA12.89730550	12.0	53.0	50.3	3.58722220	3.0	35.0	15.0	3.66	43 D	VIR
580	17597	CHARA	COR CAROLI12.90655540	12.0	54.0	23.6	38.50694400	38.0	30.0	25.0	2.90	12 A	CYN
581	17672		12.99724980	12.0	59.0	50.1	-71.33603300	-71.0	21.0	39.0	3.63	O D	MUS
582	17687	VINDEMIA TRIX	13.00722210	13.0	4.0	26.0	11.14694450	11.0	8.0	49.0	2.95	47 E	VIR
583	17773		13.08094430	13.0	4.0	51.4	-49.71916600	-49.0	43.0	9.0	4.40	O C	CEM
584	17828		13.13550330	13.0	8.0	8.1	-5.35289990	-5.0	21.0	9.0	4.44	51 J	VIR
585	17833	DIADEM	13.13603320	13.0	8.0	17.1	17.71388900	17.0	42.0	50.0	4.50	42 A	CDM
586	17874		13.17066650	13.0	10.0	14.4	28.05500000	28.0	3.0	18.0	4.32	43 B	COM
587	18000		13.17662970	13.0	15.0	58.5	40.75438800	40.0	45.0	23.0	4.66	20	CYN
588	18012		13.28355550	13.0	17.0	18.0	-22.98750000	-22.0	59.0	15.0	3.33	46 G	HTA
589	18039		13.31038800	13.0	18.0	37.4	-36.85283300	-36.0	31.0	42.0	2.91	O I	CEM
590	18087		13.33922210	13.0	20.0	21.2	-60.80555500	-60.0	48.0	20.0	4.62	O	CEM
591	18107	MIZAR	13.36041090	13.0	21.0	38.2	-64.35333200	-64.0	21.0	12.0	4.50	79 Z	CEM
592	18133	SPICA	13.37533320	13.0	22.0	31.2	55.10749900	55.0	6.0	27.0	2.40	79 Z	UMA
593	18144	ALCOR	AZIMECH13.38908330	13.0	23.0	20.7	-10.97916680	-10.0	58.0	45.0	1.21	67 A	VIR
594	18155		13.39711100	13.0	23.0	49.6	55.17000000	55.0	10.0	12.0	4.02	80	UMA
595	18239		13.46325000	13.0	27.0	47.7	-23.10111100	-23.0	6.0	4.0	3.00V	O	HTA
596	18254		13.48344430	13.0	29.0	1.4	-39.22722200	-39.0	13.0	38.0	3.96	O	CEM
597	18251	MEZE	13.54844440	13.0	32.0	54.4	-4.91777777	-4.0	25.0	4.0	3.44	79 Z	VIR
598	18256		13.55044440	13.0	32.0	1.6	49.19416600	49.0	11.0	39.0	4.63	24	CYN
599	18458		13.62761100	13.0	37.0	39.4	-53.28916600	-53.0	17.0	21.0	2.56	O E	CEM
600	18504		13.65686100	13.0	39.0	24.7	54.85833300	54.0	51.0	30.0	4.75	83	UMA
601	18593		13.72819440	13.0	43.0	41.5	-32.86749900	-32.0	52.0	3.0	4.36	I	CEM
602	18607		13.74072200	13.0	44.0	25.7	-51.25805500	-51.0	15.0	29.0	4.68	O	CEM
603	18637		13.75997220	13.0	45.0	35.9	17.63027800	17.0	37.0	49.0	4.51	4 Y	BOO
604	18643	ALKAID	BENETNASH13.76938800	13.0	46.0	9.8	49.48749900	49.0	29.0	15.0	1.91	85 M	UMA
605	18645		13.78994440	13.0	47.0	23.8	-41.51416600	-41.0	30.0	51.0	3.53	O M	CEM
606	18666		13.79016670	13.0	47.0	24.6	-34.27666600	-34.0	16.0	36.0	4.40	Z	CEM
607	18667		13.79163890	13.0	47.0	29.9	-42.29999900	-42.0	18.0	4.0	3.32	O	CEM
608	18674		13.79647210	13.0	47.0	47.3	15.97083300	15.0	58.0	15.0	4.28	S U	BOO
609	18724	MUFRIQ	13.82972210	13.0	49.0	47.9	-32.82138900	-32.0	49.0	17.0	4.72	3	CEM
610	18805		13.86361110	13.0	53.0	1.0	18.57580000	18.0	34.0	21.0	2.80	8	BOO
611	18809		13.88908330	13.0	53.0	20.7	-47.11494400	-47.0	7.0	1.0	3.06	O Z	CEM
612	18845		13.91824990	13.0	55.0	5.7	-63.51611100	-63.0	30.0	58.0	4.68	294	CEM
613	18874		13.93555550	13.0	56.0	8.0	-41.93055500	-41.0	55.0	50.0	4.05	O V	CEM
614	18883		13.94177760	13.0	56.0	30.4	-44.63361100	-44.0	38.0	1.0	4.17	O U	CEM
615	18939		13.99216650	13.0	59.0	31.8	-45.43472200	-45.0	26.0	5.0	4.39	O U	CEM
616	18945		13.99722200	13.0	59.0	51.8	1.71305555	1.0	42.0	47.0	4.34	93 Y	VIR
617	18971		14.02227770	14.0	1.0	20.2	-60.20527700	-60.0	12.0	19.0	8.86	O B	CEM
618	19019	THUBAN	14.05733320	14.0	3.0	26.4	64.54299900	64.0	32.0	33.0	3.64	11 A	DNA
619	19017		14.06500000	14.0	3.0	54.0	-41.01277700	-41.0	1.0	46.0	4.54	O X	CEM
620	19029		14.07286090	14.0	4.0	22.3	-26.51472200	-26.0	30.0	53.0	3.48	49 P	HTA
621	19033	MENKENT	14.07691660	14.0	4.0	36.9	-36.19861100	-36.0	11.0	55.0	2.24	S J	CEM
622	19168		14.18374990	14.0	11.0	1.5	-10.11166600	-10.0	64.0	42.0	4.31	98 E	VIR
623	19207		14.20383320	14.0	12.0	13.8	51.95305500	51.0	57.0	11.0	4.60	17 K	BOO
624	19242	ARCTURUS	14.23438880	14.0	14.0	3.8	19.36388800	19.0	21.0	50.0	2.24	16 A	BOO
625	19244		14.23627760	14.0	14.0	10.6	-5.83416660	-5.0	50.0	3.0	4.16	99 I	VIR
626	19273		14.25088870	14.0	15.0	3.2	46.24832200	46.0	14.0	54.0	4.26	19 L	BOO
627	19304		14.28886100	14.0	17.0	9.1	-45.89749900	-45.0	53.0	51.0	4.10	O I	LUP
628	19311		14.28886110	14.0	17.0	12.7	-13.21033340	-13.0	12.0	39.0	4.60	100 L	VIR
629	19318		14.29774980	14.0	17.0	51.9	-56.22628800	-56.0	13.0	35.0	4.41	O U	CEM
630	19337		14.30699990	14.0	18.0	25.2	-37.72527700	-37.0	43.0	31.0	4.17	O V	CEM
631	19377		14.34786100	14.0	20.0	52.3	-39.35305600	-39.0	21.0	11.0	4.55	O	CEM
632	19449		14.35741650	14.0	21.0	5.1	-83.85099900	-83.0	30.0	36.0	4.14	O D	OCT
633	19453		14.39799990	14.0	23.0	52.8	-45.06416600	-45.0	3.0	51.0	4.65	O T	LUP
634	19454		14.39843890	14.0	23.0	55.1	-45.22222100	-45.0	13.0	20.0	4.49	O T	LUP
635	19467		14.40008330	14.0	24.0	1.3	52.01194400	52.0	1.0	43.0	4.06	23 J	BOO



TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

634	19548	14.459461090	14.0	27.0	34.4	75.05130900	75.0	51.0	4.37	5	UMI
637	19570	14.50408310	14.0	30.0	14.7	-50.30305500	-50.0	11.0	4.60	0	LUP
638	19577	14.50536100	14.0	30.0	19.3	30.52416600	30.0	31.0	3.78	25	R
639	19607	14.51113060	14.0	30.0	40.1	38.46055500	38.0	27.0	3.00	28	B
640	19459	14.55258320	14.0	33.0	9.3	29.09430900	29.0	53.0	4.48	28	S
641	19656	14.55458310	14.0	33.0	16.5	-42.00500000	-42.0	1.0	4.65	0	CEM
642	19678	14.57199790	14.0	35.0	31.2	-49.27444400	-49.0	16.0	4.14	0	R
643	19728	14.62013070	14.0	37.0	12.5	-60.69222200	-60.0	41.0	3.06	0	A
644	19777	14.65791660	14.0	39.0	28.5	13.07750000	13.0	52.0	3.86	30	Z
645	19774	14.65906100	14.0	39.0	35.5	-47.23916600	-47.0	14.0	2.89	0	A
646	19772	14.66091660	14.0	39.0	39.3	-64.02416600	-64.0	49.0	3.41	0	A
647	19779	14.66297210	14.0	39.0	46.7	-37.64444400	-37.0	38.0	4.09	0	CEM
648	19816	14.68466100	14.0	41.0	12.7	-5.50722200	-5.0	30.0	3.95	107	M
649	19820	14.69100550	14.0	41.0	30.5	-35.02416600	-35.0	1.0	4.13	371	CEM
650	19834	14.72374990	14.0	43.0	25.5	-78.09433200	-78.0	54.0	3.81	0	A
651	19836	14.72430540	14.0	43.0	27.5	27.22083300	27.0	13.0	2.70	36	E
652	19858	14.72677770	14.0	43.0	36.4	17.11138900	17.0	6.0	4.69	35	0
653	19884	14.74127750	14.0	44.0	28.6	2.03916660	2.0	2.0	3.76	109	VIR
654	19954	14.80377760	14.0	48.0	13.6	-27.01583300	-27.0	48.0	4.63	58	MYA
655	19975	14.81563080	14.0	48.0	56.3	-15.09749900	-15.0	53.0	4.90	9	A
656	19977	14.82441660	14.0	49.0	20.7	-43.43166600	-43.0	25.0	4.49	0	LUP
657	19991	14.82952760	14.0	49.0	46.3	19.24527700	19.0	14.0	4.64	37	C
658	20039	14.84644430	14.0	50.0	47.2	74.29861100	74.0	17.0	2.24	7	B
659	20115	14.92252770	14.0	56.0	21.1	-4.20500000	-4.0	12.0	4.59	16	LIB
660	20128	14.93716660	14.0	56.0	13.8	-42.99444400	-42.0	59.0	2.81	0	LUP
661	20146	14.94791660	14.0	56.0	52.5	-41.94500000	-41.0	57.0	3.35	0	CEM
662	20226	NEKKAR 15.01044440	15.0	0	77.6	40.52749900	40.0	31.0	3.63	42	B
663	20237	15.01883330	15.0	1.0	7.8	2.22749990	2.0	13.0	4.62	110	VIR
664	20253	15.03361110	15.0	2.0	1.0	-25.14583300	-25.0	8.0	3.41	20	S
665	20271	15.04541670	15.0	2.0	43.5	-46.91555500	-46.0	54.0	4.02	0	P
666	20285	15.04908320	15.0	2.0	56.7	27.08305500	27.0	4.0	4.67	43	Y
667	20356	15.10791640	15.0	6.0	28.5	-45.14666600	-45.0	8.0	4.39	0	L
668	20409	15.15816660	15.0	9.0	29.4	-48.06438800	-48.0	23.0	4.14	0	K
669	20418	15.16263870	15.0	9.0	45.5	-51.96749900	-51.0	58.0	3.50	0	LUP
670	20433	15.17036110	15.0	10.0	13.3	-19.64055500	-19.0	39.0	4.66	24	I
671	20523	15.23483310	15.0	14.0	54.4	33.44444400	33.0	26.0	3.54	49	D
672	20507	15.24544430	15.0	14.0	45.4	-58.47222200	-58.0	40.0	4.16	0	CIR
673	20539	15.25199980	15.0	15.0	7.2	-9.25500000	-9.0	15.0	2.74	27	B
674	20538	15.26024980	15.0	15.0	36.9	-68.55222100	-68.0	33.0	3.06	0	G
675	20550	15.26158320	15.0	15.0	41.7	-30.02138800	-30.0	1.0	4.43	2	LUP
676	20556	15.26811090	15.0	16.0	5.2	-47.74777700	-47.0	44.0	4.34	0	M
677	20620	15.31788870	15.0	19.0	4.4	-40.52222100	-40.0	20.0	3.93	0	LUP
678	20643	15.32630530	15.0	19.0	34.7	-36.13583300	-36.0	9.0	3.59	0	Y
679	20659	15.33624980	15.0	20.0	17.7	-44.56499900	-44.0	33.0	3.74	0	LUP
680	20663	15.34288870	15.0	20.0	34.4	-59.19638900	-59.0	11.0	4.54	0	CIR
681	20682	15.34613880	15.0	20.0	46.1	71.95861000	71.0	57.0	3.14	13	G
682	20676	15.34852770	15.0	20.0	54.7	-38.73444400	-38.0	44.0	4.69	0	V
683	20714	15.38430540	15.0	23.0	3.5	-38.66111000	-38.0	36.0	4.68	0	K
684	20724	15.38611100	15.0	23.0	10.0	37.49888800	37.0	29.0	4.97	51	M
685	20737	15.4022210	15.0	24.0	8.0	59.08805500	59.0	5.0	3.47	12	I
686	20795	15.43974980	15.0	26.0	23.1	29.2527700	29.0	13.0	3.72	3	B
687	20926	15.52527770	15.0	31.0	31.0	31.47611000	31.0	28.0	4.17	4	J
688	20926	15.52666670	15.0	32.0	48.0	-41.05055500	-41.0	3.0	2.95	0	LUP
689	20942	15.55213880	15.0	33.0	7.7	10.65472200	10.0	39.0	4.24	13	O
690	20947	15.55416660	15.0	33.0	12.3	26.83138900	26.0	49.0	2.31	5	A
691	20932	15.5582210	15.0	33.0	29.6	-66.20166500	-66.0	12.0	4.11	0	E
692	20949	15.55941660	15.0	33.0	33.9	-14.67416660	-14.0	40.0	4.02	38	B
693	20979	15.58155550	15.0	34.0	53.6	-28.02055500	-28.0	14.0	3.78	39	U

TOLINN

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KIFFAA

KIFFAB

GEMMA

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

694 21001	15.59480530	15.0	35.0	41.3	-42.45388900	-42.0	27.0	14.0	4.27	0 W	LUP
695 21019	15.60833320	15.0	36.0	30.0	-29.66416600	-29.0	39.0	51.0	3.80	40 T	L1B
696 21072	15.62561090	15.0	37.0	32.2	-34.29889000	-34.0	17.0	56.0	4.63	3 Y	LUP
697 21070	15.64622210	15.0	38.0	46.4	-44.54694900	-44.0	32.0	44.0	4.69	0 J	LUP
698 21102	15.66647220	15.0	39.0	59.3	19.78194400	19.0	46.0	55.0	4.49	21 I	S R
699 21130	15.68786100	15.0	41.0	16.3	26.40527700	26.0	24.0	19.0	3.93	8 C	S R
700 21158	COR SERPENTIS UNUKIS.70.02760	15.0	42.0	32.5	6.53444400	6.0	32.0	4.0	2.75	24 A	SER ELMAHA
701 21194	15.74283320	15.0	44.0	34.2	15.85300000	15.0	31.0	48.0	3.74	28 B	SER
702 21201	15.74569430	15.0	44.0	44.5	7.46146660	7.0	27.0	42.0	4.42	20 L	SER
703 21243	15.75447200	15.0	45.0	16.1	77.90305500	77.0	54.0	11.0	4.34	16 Z	UNI
704 21255	15.78605550	15.0	47.0	9.8	18.24833300	18.0	19.0	54.0	4.28	35 K	SER
705 21269	15.79450000	15.0	47.0	47.4	-3.33244440	-3.0	19.0	28.0	3.63	32 M	SER
706 21276	15.80208330	15.0	48.0	7.5	26.17416600	26.0	10.0	27.0	4.73	10 D	CRB
707 21281	15.81213880	15.0	48.0	43.7	-33.52222100	-33.0	20.0	4.11	4.11	5 X	LUP
708 21288	15.81780540	15.0	49.0	4.1	4.58146670	4.0	34.0	54.0	3.75	37 E	SER
709 21340	15.85772200	15.0	51.0	27.8	42.54861000	42.0	32.0	55.0	4.61	1 X	MER
710 21329	15.85841660	15.0	51.0	30.3	-25.22416600	-25.0	13.0	27.0	4.64	2	SCO
711 21342	15.86380540	15.0	51.0	49.7	-16.64280550	-16.0	37.0	41.0	4.34	46 J	L1B
712 21332	15.86733310	15.0	52.0	2.4	-63.32472100	-63.0	19.0	29.0	3.04	0 B	TRA
713 21398	15.91197220	15.0	54.0	43.1	-29.11333300	-29.0	6.0	48.0	4.02	5 R	SCO
714 21408	15.91391650	15.0	54.0	50.1	15.77444430	15.0	46.0	28.0	3.84	11 S	SER
715 21440	15.93561100	15.0	56.0	8.2	26.97805500	26.0	58.0	41.0	4.22	13 E	CRB
716 21439	15.93708320	15.0	56.0	13.5	-14.18000000	-14.0	10.0	48.0	4.68	48	L1B
717 21447	15.94549980	15.0	56.0	43.8	-26.01472100	-26.0	5.0	53.0	3.00	6 P	SCO
718 21478	15.96325000	15.0	57.0	47.7	-38.29833300	-38.0	17.0	25.0	3.64	0 M	LUP
719 21489	15.97099990	15.0	58.0	15.6	-22.52311000	-22.0	31.0	54.0	2.54	7 D	SCO
720 21539	16.01052700	16.0	5.0	37.9	-49.13388900	-49.0	8.0	2.0	4.74	0 M	NOR
721 21572	16.02050000	16.0	1.0	13.8	58.65805500	58.0	39.0	29.0	4.11	13 J	DRA
722 21580	16.02844400	16.0	1.0	42.4	46.11330550	46.0	7.0	59.0	4.64	6 U	MER
723 21593	16.04066600	16.0	2.0	24.4	-11.27805560	-11.0	16.0	41.0	4.16	0 C	SCO
724 21809	ELACRAB	16.05663800	16.0	3.0	19.71111100	-19.0	42.0	40.0	2.90	8 R	SCO
725 21825	16.07147200	16.0	4.0	17.3	-38.70811100	-38.0	42.0	31.0	4.33	0 J	LUP
726 21839	16.07924900	16.0	4.0	45.3	-20.85758330	-20.0	34.0	33.0	4.13	9 M	SCO
727 21859	16.08913800	16.0	5.0	20.9	-20.77555500	-20.0	46.0	32.0	4.58	10 B	SCO
728 21736	16.12775000	16.0	7.0	39.9	45.02555500	45.0	1.0	32.0	4.26	11 V	MER
729 21773	16.16594300	16.0	9.0	57.4	-19.37111000	-19.0	22.0	16.0	4.29	14 M	SCO
730 21778	16.16902700	16.0	10.0	8.5	-27.83722200	-27.0	50.0	14.0	4.70	13	SCO
731 21819	16.20391600	16.0	12.0	14.1	-63.95981000	-63.0	35.0	55.0	4.03	0 D	TRA
732 21838	16.20847100	16.0	12.0	30.5	-3.60555550	-3.0	36.0	20.0	3.03	1 D	OPH
733 21920	16.27444400	16.0	16.0	28.0	-4.60861100	-4.0	36.0	31.0	3.34	2 E	OPH
734 21933	16.28860000	16.0	17.0	12.7	-50.07166600	-50.0	4.0	18.0	4.14	0 E	NOR
735 21987	16.31144400	16.0	18.0	41.2	46.39583300	46.0	23.0	45.0	3.91	22 T	HER
736 21982	16.31741000	16.0	19.0	3.4	-25.85105560	-25.0	30.0	38.0	2.87	20 S	SCO
737 22012	16.33958300	16.0	20.0	22.5	19.23416600	19.0	14.0	3.0	3.79	20 G	HER
738 22020	16.34552700	16.0	20.0	43.9	30.97222100	30.0	58.0	20.0	4.72	19 C	CRB
739 22052	16.36752700	16.0	22.0	3.1	-19.95694900	-19.0	57.0	25.0	4.59	4 Y	OPH
740 22101	16.39186100	16.0	23.0	30.7	61.59305500	61.0	35.0	35.0	2.89	14 M	DRA
741 22090	16.39663800	16.0	23.0	47.9	14.11250000	14.0	6.0	45.0	4.53	24 M	HER
742 22134	16.43177700	16.0	25.0	54.4	-8.29500000	-8.0	17.0	42.0	4.68	3 U	OPH
743 22157	ANTARES VESPERTIL.16.45427700	16.0	27.0	15.4	-26.35611100	-26.0	21.0	22.0	4.22	21 A	SCO 10
744 22142	16.46702700	16.0	28.0	1.3	-78.82222200	-78.0	49.0	20.0	3.90	0 G	APS
745 22193	KORNEPHOROS RUTIL.16.47855500	16.0	28.0	42.8	21.95647220	21.0	33.0	53.0	2.81	27 B	HER ICUS
746 22195	16.48483300	16.0	29.0	5.4	-34.62972200	-34.0	37.0	47.0	4.33	8	SCO
747 22200	16.48552700	16.0	29.0	7.9	-16.53805500	-16.0	32.0	17.0	4.40	0 V	OPH
748 22203	16.48577700	16.0	29.0	8.8	2.05916660	2.0	3.0	33.0	3.85	10 L	OPH
749 22221	16.50094400	16.0	30.0	3.4	-21.39305500	-21.0	23.0	35.0	4.57	9 W	OPH
750 22276	16.54995500	16.0	32.0	58.4	42.50833300	42.0	30.0	30.0	4.25	35 S	HER
751 22303	16.56166600	16.0	33.0	42.0	-28.14500000	-28.0	8.0	42.0	2.91	23 T	SCO

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

752	22311	16.56777700	16.0	34.0	4.0	-35.18527700	-35.0	11.0	7.0	4.30	0	SCO
753	22332	16.58713800	16.0	35.0	13.7	-10.49777760	-10.0	29.0	52.0	2.70	13	Z
754	22370	16.63386100	16.0	38.0	1.9	-77.44777700	-77.0	26.0	52.0	4.16	0	B
755	22644	16.64608300	16.0	39.0	57.9	31.66500000	31.0	39.0	54.0	3.00	40	Z
756	22502	16.64941600	16.0	41.0	41.7	38.98777700	38.0	59.0	16.0	3.61	44	M
757	22558	16.74902700	16.0	44.0	56.5	-68.96611000	-68.0	57.0	58.0	1.88	0	A
758	22606	16.77922200	16.0	46.0	45.2	-58.98138800	-58.0	58.0	53.0	3.68	0	M
759	22640	16.79819400	16.0	47.0	53.5	-34.23138900	-34.0	13.0	53.0	2.36	26	E
760	23643	16.79835000	16.0	47.0	53.7	-10.72277770	-10.0	43.0	42.0	4.73	20	OPH
761	22749	16.82477700	16.0	49.0	29.2	82.09750000	82.0	5.0	51.0	4.40	22	E
762	22677	16.82491600	16.0	49.0	29.7	-37.98916600	-37.0	59.0	21.0	3.09	0	M
763	22691	16.83266600	16.0	49.0	57.6	-37.95972200	-37.0	57.0	35.0	3.64	0	M
764	22751	16.86583300	16.0	52.0	6.9	-42.30333300	-42.0	18.0	12.0	3.75	0	Z
765	22775	16.87249900	16.0	52.0	21.0	10.22166650	10.0	13.0	18.0	4.29	25	I
766	22845	16.92859300	16.0	55.0	42.9	-55.92694400	-56.0	56.0	13.0	3.04	0	Z
767	22862	16.93349900	16.0	56.0	7.6	9.42805550	9.0	25.0	41.0	3.42	27	K
768	22869	16.94444400	16.0	56.0	47.2	-53.10888800	-53.0	6.0	32.0	4.15	0	E
769	22935	16.98247200	16.0	58.0	54.9	30.97666600	30.0	58.0	36.0	3.92	58	E
770	23158	17.13947100	17.0	8.0	22.1	-15.68333300	-16.0	41.0	7.0	2.43	35	M
771	23182	17.14469300	17.0	8.0	40.9	65.75750000	65.0	45.0	27.0	3.22	22	Z
772	23180	17.16069400	17.0	9.0	38.5	-43.19500000	-43.0	11.0	42.0	3.44	0	M
773	23277	17.21749900	17.0	13.0	3.0	14.42888890	14.0	25.0	44.0	3.50	44	A
774	23294	17.22652700	17.0	13.0	35.5	24.87916600	24.0	52.0	45.0	3.16	65	D
775	23302	17.23044400	17.0	13.0	49.6	34.84750000	34.0	50.0	51.0	3.36	67	P
776	23359	17.28719400	17.0	18.0	1.9	33.13666600	33.0	6.0	12.0	4.004	68	HER
777	23392	17.30538800	17.0	18.0	19.4	-67.73666500	-67.0	44.0	12.0	4.74	0	Z
778	23424	17.31427800	17.0	18.0	51.4	-12.81305550	-12.0	48.0	47.0	4.35	53	N
779	23423	17.31505500	17.0	18.0	54.2	-21.07694400	-21.0	4.0	37.0	4.46	40	C
780	23451	17.33094400	17.0	19.0	51.4	-24.96436600	-24.0	57.0	59.0	3.37	42	J
781	23515	17.37308300	17.0	22.0	23.1	-55.49946600	-56.0	29.0	57.0	2.80	0	B
782	23517	17.37402700	17.0	22.0	26.5	-56.35894400	-56.0	20.0	49.0	3.51	0	B
783	23544	17.37455500	17.0	22.0	28.4	37.17694400	37.0	10.0	37.0	4.52	0	M
784	23597	17.40333300	17.0	24.0	13.8	-24.14500000	-24.0	8.0	42.0	4.28	44	OPH
785	23617	17.41286100	17.0	24.0	46.3	-5.05722220	-5.0	3.0	26.0	4.61	27	OPH
786	23621	17.41294300	17.0	24.0	46.6	4.116916660	4.0	10.0	9.0	4.44	49	B
787	23627	17.41861000	17.0	25.0	7.0	-29.83722200	-29.0	50.0	14.0	4.37	45	OPH
788	23681	17.46555500	17.0	27.0	56.0	-60.65694400	-60.0	39.0	25.0	3.79	0	B
789	23693	17.47302700	17.0	28.0	22.9	-37.27000000	-37.0	16.0	12.0	2.80	34	U
790	23708	17.48527000	17.0	29.0	7.9	-49.85055500	-49.0	51.0	2.0	2.97	0	A
791	23726	17.48849400	17.0	29.0	19.3	26.13583300	26.0	8.0	9.0	4.48	76	L
792	23741	17.49399900	17.0	29.0	38.4	52.32638900	52.0	19.0	35.0	2.99	23	B
793	23769	17.52049900	17.0	31.0	13.8	-37.08027700	-37.0	4.0	49.0	1.71	35	L
794	23815	17.55083300	17.0	33.0	3.0	-46.48361100	-46.0	29.0	29.0	4.63	0	B
795	23837	17.55138000	17.0	33.0	18.5	12.58416670	12.0	35.0	3.0	2.14	55	A
796	23846	17.56889000	17.0	34.0	8.0	-38.61249900	-38.0	34.0	45.0	4.34	0	SCO
797	23857	17.58000000	17.0	34.0	48.0	-42.97750000	-42.0	58.0	39.0	2.04	0	J
798	23881	17.59299900	17.0	35.0	34.8	-15.37833320	-16.0	22.0	42.0	3.64	55	C
799	23889	17.59899900	17.0	35.0	56.4	-8.09916670	-8.0	5.0	57.0	4.65	57	M
800	23965	17.64124900	17.0	38.0	28.5	46.02416600	46.0	1.0	27.0	3.79	85	I
801	23978	17.65741600	17.0	39.0	26.7	-12.85833330	-12.0	51.0	30.0	4.39	54	O
802	23988	17.66772200	17.0	40.0	3.8	-39.01388900	-39.0	3.0	50.0	2.51	0	K
803	24048	17.69569400	17.0	41.0	44.5	4.588027770	4.0	34.0	49.0	2.94	60	B
804	24044	17.69888800	17.0	42.0	17.6	-64.70972200	-64.0	42.0	35.0	3.58	0	M
805	24234	17.72425000	17.0	43.0	27.3	86.60472200	86.0	36.0	17.0	4.44	23	O
806	24138	17.75144300	17.0	45.0	5.2	-27.73989900	-27.0	44.0	24.0	3.48	86	M
807	24125	17.75225000	17.0	45.0	8.1	-40.11527700	-40.0	6.0	55.0	3.14	0	I
808	24135	17.75591600	17.0	45.0	21.3	-27.81916600	-27.0	49.0	9.0	4.004	3	S6R
809	24162	17.76894400	17.0	46.0	8.2	27.71888890	27.0	43.0	8.0	3.74	62	6

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

Star ID	Star Name	17.0	47.0	28.5	-37.0	2.0	3.0	3.55	0	Star Type
810	24188	17.79125000	17.0	52.0	56.0	52.0	39.0	3.90	0	SCO
811	24364	17.80202700	17.0	55.0	56.0	52.0	39.0	3.90	0	ORA
812	24415	17.91752700	17.0	55.0	56.0	52.0	39.0	3.90	0	HER
813	24332	17.92986000	17.0	55.0	56.0	52.0	39.0	3.90	0	ETA
814	24448	17.94005500	17.0	56.0	24.2	29.0	2.0	3.82	0	ETA
815	24468	17.95163800	17.0	57.0	5.9	29.0	2.0	3.82	0	HER
816	24778	17.95269400	17.0	57.0	9.7	30.0	15.0	3.50	0	OPH
817	24502	17.97494400	17.0	58.0	29.8	16.0	28.0	4.16	0	HER
818	24503	17.97719400	17.0	58.0	37.9	16.0	47.1	4.71	0	HER
819	24509	17.98149900	17.0	58.0	53.4	3.0	22.0	4.40	0	ETA
820	24534	17.99641000	17.0	59.0	58.6	1.0	54.0	4.40	0	ETA
821	24605	18.00638800	18.0	2.0	47.0	18.0	14.0	4.44	0	OPH
822	24632	18.05930500	18.0	3.0	3.05	29.0	35.0	4.00V	0	OPH
823	24641	18.06411600	18.0	3.0	2.06	28.0	35.0	4.00V	0	OPH
824	24635	18.06508300	18.0	3.0	54.3	3.0	22.0	4.07	0	OPH
825	24645	18.06800500	18.0	5.0	12.5	5.0	46.0	3.90	0	ARA
826	24693	18.07938300	18.0	5.0	37.8	40.0	21.0	4.44	0	PAV
827	24875	18.09480500	18.0	5.0	41.3	43.0	41.0	4.73	0	OPH
828	24694	18.09774900	18.0	5.0	51.9	27.0	27.0	4.66	0	OPH
829	24711	18.10291600	18.0	4.0	10.5	45.0	23.0	3.83	0	HER
830	24740	18.12100000	18.0	7.0	15.6	28.0	28.0	4.32	0	HER
831	24767	18.14383300	18.0	6.0	37.8	5.0	45.0	4.60	0	TEL
832	24856	18.19447100	18.0	11.0	40.1	4.0	45.0	4.00V	0	TEL
833	24944	18.25427700	18.0	15.0	15.4	3.0	27.0	3.16	0	OPH
834	24941	18.26438000	18.0	15.0	51.7	27.0	25.0	4.69	0	OPH
835	25022	18.31055500	18.0	18.0	38.0	2.0	52.0	4.34	0	LYR
836	25024	18.31253500	18.0	18.0	45.2	29.0	42.0	2.84	0	OPH
837	25046	18.32494400	18.0	17.0	29.8	2.0	44.0	3.82	0	OPH
838	25045	18.33336100	18.0	20.0	1.1	30.0	49.0	4.25	0	OPH
839	25114	18.35433200	18.0	21.0	15.4	19.0	10.0	4.24	0	OPH
840	25122	18.36147200	18.0	21.0	41.3	43.0	5.0	3.69	0	OPH
841	25100	18.38413800	18.0	21.0	50.9	28.0	11.0	1.95	0	OPH
842	25116	18.37008300	18.0	22.0	45.0	9.0	3.92	1.09	0	OPH
843	25154	18.40630500	18.0	22.0	22.7	23.0	3.76	2.22	0	TEL
844	25180	18.43016600	18.0	25.0	48.4	25.0	34.0	2.94	0	OPH
845	25183	18.43558300	18.0	26.0	8.1	5.0	31.0	4.14	0	TEL
846	25220	18.45336000	18.0	27.0	12.1	35.0	23.0	4.73	0	OPH
847	25313	18.51672200	18.0	31.0	2.2	20.0	23.0	4.69	0	CRA
848	25385	18.55502700	18.0	33.0	18.1	18.0	12.0	4.06	0	OPH
849	25466	18.59586100	18.0	35.0	45.1	38.0	45.0	1.14	0	LYR
850	25822	18.64925000	18.0	38.0	57.3	27.0	41.0	4.10	0	OPH
851	25880	18.67261000	18.0	40.0	21.4	3.0	15.0	4.70V	0	OPH
852	25668	18.72033300	18.0	43.0	13.2	39.0	31.0	4.50	0	LYR
853	25661	18.72450000	18.0	43.0	28.2	1.0	43.0	3.30	0	OPH
854	25674	18.72603100	18.0	43.0	33.9	34.0	4.29	6.1	0	LYR
855	25698	18.73588000	18.0	45.0	9.2	30.0	42.0	4.24	0	HER
856	25730	18.75527700	18.0	45.0	17.0	20.0	13.0	4.57	0	OPH
857	25734	18.75788000	18.0	45.0	28.4	6.0	28.0	4.37	0	HER
858	25735	18.76022100	18.0	45.0	36.8	4.0	39.0	4.00V	0	OPH
859	25947	18.81311000	18.0	48.0	47.2	19.0	3.38	10.8	0	LYR
860	25823	18.81630500	18.0	48.0	58.7	13.0	49.0	4.42	0	OPH
861	25941	18.88491600	18.0	53.0	5.7	20.0	31.0	2.14	0	OPH
862	25954	18.88780500	18.0	53.0	16.1	58.0	58.0	4.56	0	HER
863	25959	18.88971100	18.0	53.0	16.7	16.0	12.0	4.50V	0	LYR
864	25930	18.88916600	18.0	53.0	21.0	16.0	49.0	4.00V	0	OPH
865	25976	18.90447100	18.0	54.0	16.1	5.0	58.0	4.00V	0	LYR
866	25991	18.90797200	18.0	54.0	28.7	9.0	24.0	4.50	0	OPH
867	26019	18.92736000	18.0	55.0	38.5	9.0	16.0	3.61	0	OPH

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

068	24084	SULAPNAT	18+960555500	18+0	57+0	38+0	32+64027700	32+0	38+0	25+0	3+30	14 6	LYR
069	26091		18+967222200	18+0	58+0	2+0	15+019444400	15+0	1+0	10+0	4+21	13 E	AOL
070	26141		18+966833000	18+0	59+0	48+4	-5+789722200	-5+0	47+0	23+0	4+15	12	AOL
071	26161	ASCELLA	19+006416000	19+0	-0	23+1	-29+931944000	-29+0	55+0	55+0	2+71	38 Z	S6R
072	26224		19+004308300	19+0	2+0	35+1	-21+794444000	-21+0	47+0	40+0	3+90	39 D	S6R
073	26270		19+006333300	19+0	3+0	48+0	13+810000000	13+0	48+0	38+0	3+02	17 Z	AOL
074	26263		19+067555500	19+0	4+0	3+2	-37+115277000	-37+0	6+0	55+0	4+26	0 6	CRA
075	26295		19+073166000	19+0	4+0	23+8	-4+936333880	-4+0	56+0	11+0	3+55	16 L	AOL
076	26291		19+079249000	19+0	4+0	45+3	-27+723333200	-27+0	43+0	24+0	3+42	40 Y	S6R
077	26322		19+098555500	19+0	5+0	54+8	-40+552778000	-40+0	33+0	10+0	4+66	0 0	CRA
078	26360		19+118222000	19+0	7+0	5+6	-37+960833000	-37+0	39+0	39+0	4+12	0 A	CRA
079	26380		19+127027000	19+0	7+0	37+3	-39+398333000	-39+0	23+0	54+0	4+16	0 B	CRA
080	26384		19+128027000	19+0	7+0	40+9	-21+080833000	-21+0	4+0	51+0	3+02	41 P	S6R
081	26520	NODUS II	19+128027000	19+0	12+0	33+0	67+599999000	67+0	36+0	-0	3+24	57 D	ORA
082	26507		19+209160000	19+0	12+0	33+9	39+084721000	39+0	5+0	5+0	4+76	20 M	LYR
083	26569		19+245166000	19+0	14+0	42+6	21+327499000	21+0	19+0	39+0	4+64	1	VUL
084	26585		19+252527000	19+0	15+0	9+1	38+070277000	38+0	4+0	13+0	4+46	21 J	LYR
085	26630		19+270502000	19+0	16+0	14+1	73+291111000	73+0	17+0	28+0	4+63	60 Y	ORA
086	26621		19+271555000	19+0	16+0	17+6	53+303333000	53+0	18+0	12+0	3+98	1 K	CY6
087	26694		19+327389000	19+0	19+0	38+6	-17+914722000	-17+0	54+0	52+0	3+95	44 R	S6R
088	26697		19+328694000	19+0	19+0	43+3	-16+022222000	-16+0	1+0	20+0	4+58	46 U	S6R
089	26703	ARKAB-PRIOR	19+335388000	19+0	20+0	7+4	-44+526666000	-44+0	31+0	36+0	4+24	0 B	S6R
090	26735		19+341527000	19+0	20+0	29+5	45+646943000	45+0	38+0	49+0	4+63	58 P	ORA
091	26718	ARKAB-POSTERIOR	19+344889000	19+0	20+0	41+6	-48+867499000	-48+0	52+0	3+0	4+51	0 B	S6R
092	26737	ALNAHI	19+357222000	19+0	21+0	27+8	-40+883611000	-40+0	41+0	1+0	4+11	0 A	S6R
093	26816	DENEK OKAB	19+395555000	19+0	23+0	44+0	3+043611100	3+0	2+0	37+0	3+44	30 D	AOL
094	26809		19+454138000	19+0	27+0	14+9	24+592777000	24+0	35+0	3+0	4+63	6 A	VUL
095	26947		19+480389000	19+0	28+0	49+4	51+654444000	51+0	37+0	16+0	3+94	10 I	CY6
096	26953	ALBIREO	19+488472000	19+0	29+0	18+8	27+885000000	27+0	53+0	6+0	3+24	6 0	CY6
097	27030		19+539639000	19+0	32+0	22+7	7+303333000	7+0	18+0	12+0	4+65	38 M	AOL
098	27089		19+576305000	19+0	34+0	34+7	-24+922500000	-24+0	57+0	45+0	4+66	52	S6R
099	27103		19+581833000	19+0	34+0	54+6	-1+345555554	-1+0	21+0	56+0	4+28	41 I	AOL
900	27141		19+591649000	19+0	35+0	30+1	50+139166000	50+0	8+0	21+0	4+64	13 J	CY6
901	27215	SHAM	19+642166000	19+0	38+0	31+8	17+931944000	17+0	55+0	55+0	4+37	5 A	S6E
902	27234		19+657916000	19+0	39+0	28+5	17+393411000	17+0	23+0	37+0	4+45	6 8	S6E
903	27347		19+731305000	19+0	43+0	52+7	45+044444000	45+0	2+0	40+0	2+97	18 0	CY6
904	27354	REDA	19+743250000	19+0	44+0	35+7	10+526666600	10+0	31+0	36+0	2+80	50 8	AOL
905	27391		19+763777000	19+0	45+0	49+6	18+446666000	18+0	26+0	48+0	3+78	7 0	S6E
906	27471	TYL	19+804999000	19+0	48+0	18+0	70+178888000	70+0	10+0	44+0	3+99	63 C	ORA
907	27470	ALTAIR	19+817916000	19+0	49+0	4+5	8+774444000	8+0	46+0	28+0	4+89	53 A	AOL
908	27481		19+820305000	19+0	49+0	13+1	32+824444000	32+0	49+0	28+0	4+00V	0 I	CY6
909	27517		19+844833000	19+0	50+0	41+4	99+1444443	99+0	56+0	52+0	3+00V	55 M	AOL
910	27544		19+864194000	19+0	51+0	58+3	23+987222000	23+0	59+0	1+0	4+50	13	VUL
911	27554		19+880833000	19+0	52+0	51+0	-41+961944000	-41+0	57+0	43+0	4+21	0 I	S6R
912	27587	ALSHAIN	19+893222000	19+0	53+0	35+4	6+318055500	6+0	19+0	5+0	3+90	60 8	AOL
913	27605		19+913360000	19+0	54+0	48+1	-27+264166000	-27+0	15+0	51+0	4+62	59	S6R
914	27622		19+916527000	19+0	54+0	59+5	34+987444000	34+0	59+0	22+0	4+03	21 M	CY6
915	27631		19+942916000	19+0	56+0	34+5	-73+005833000	-73+0	-0	21+0	4+10	12 6	S6E
916	27672		19+953305000	19+0	57+0	11+9	19+395833000	19+0	23+0	45+0	3+71	12 6	S6E
917	27670		19+957499000	19+0	57+0	27+7	-35+372777000	-35+0	22+0	22+0	4+39	0 J	S6R
918	27753		19+994305000	19+0	59+0	39+5	27+655833000	27+0	39+0	21+0	4+74	15	VUL
919	27763		20+008720000	20+0	-0	30+5	-27+808810000	-27+0	48+0	31+0	4+60	62	S6R
920	27854		20+044416000	20+0	2+0	39+9	67+773611000	67+0	46+0	28+0	4+66	67 R	ORA
921	27884		20+088471000	20+0	5+0	18+5	-66+273611000	-66+0	16+0	25+0	3+64	0 0	PAY
922	28010		20+158305000	20+0	9+0	29+9	-92+6666665	-92+0	55+0	36+0	3+37	46 J	AOL
923	28044		20+168360000	20+0	10+0	6+1	77+606494000	77+0	36+0	25+0	4+40	1 K	CEP
924	28099		20+208605000	20+0	12+0	31+7	46+634444000	46+0	38+0	4+0	3+95	31 0	CY6
925	28108		20+209749000	20+0	12+0	35+1	56+459999000	56+0	27+0	36+0	4+32	33	CY6

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

926 28152	20+23861000	20+0	14+0	19+0	27+70583300	27+0	42+0	21+0	4+73	23	VUL
927 28160	20+23980500	20+0	14+0	23+3	47+60611100	47+0	34+0	22+0	4+16	32	CYG
928 28189	20+26180500	20+0	15+0	42+5	-12+61777770	-12+0	37+0	4+0	4+55	5	CAP
929 28200	20+26855500	20+0	16+0	6+8	-12+65472200	-12+0	39+0	17+0	3+77	6	CAP
930 28295	20+31741600	20+0	19+0	2+7	-14+89333330	-14+0	53+0	36+0	3+25	9	CAP
931 28338	20+34950000	20+0	20+0	58+2	40+14388800	40+0	8+0	38+0	2+32	37	CYG
932 28378	20+37433300	20+0	22+0	27+6	32+07611100	32+0	4+0	35+0	4+60	39	CYG
933 28374	20+38147200	20+0	22+0	53+3	-56+84916800	-56+0	50+0	57+0	2+12	0	AVG
934 28513	20+46055000	20+0	27+0	57+8	30+25082300	30+0	15+0	3+0	4+09	41	CEP
935 28541	20+48327700	20+0	31+0	59+8	62+87611100	62+0	52+0	34+0	4+28	2	J
936 28593	20+52564400	20+0	32+4	32+4	11+18305550	11+0	10+0	59+0	3+98	2	DEL
937 28659	20+56119400	20+0	33+0	40+3	14+55249990	14+0	33+0	9+0	4+47	4	Z
938 28682	20+58519400	20+0	35+0	6+7	-47+41499900	-47+0	24+0	55+0	3+21	0	IND
939 28709	20+59844400	20+0	35+0	54+4	14+47222220	14+0	28+0	20+0	3+72	4	DEL
940 28725	20+60833000	20+0	36+0	31+8	-1+22861110	-1+0	13+0	43+0	4+51	71	AGL
941 28780	20+63352700	20+0	38+0	7	15+78749980	15+0	47+0	35+0	3+86	9	DEL
942 28846	20+67081100	20+0	40+0	14+2	45+15444400	45+0	9+0	16+0	1+33	50	CYG ARIDED
943 28860	20+69127700	20+0	41+0	28+6	-52+04749900	-52+0	2+0	51+0	4+70	0	IND
944 28873	20+69705500	20+0	41+0	49+4	14+94777770	14+0	56+0	52+0	4+53	11	DEL
945 28862	20+69708300	20+0	41+0	49+5	-66+33083200	-66+0	19+0	51+0	3+60	0	PAY
946 28929	20+73374900	20+0	44+0	1+5	-25+38055000	-25+0	23+0	53+0	4+26	14	V
947 28942	20+73616000	20+0	44+0	12+9	30+57111100	30+0	35+0	28+0	4+34	52	CAP
948 28954	20+74138800	20+0	44+0	29+0	57+45361100	57+0	27+0	13+0	4+63	6	CEP
949 28962	20+74299900	20+0	44+0	34+8	61+70250000	61+0	42+0	9+0	3+59	3	M
950 28959	20+74655500	20+0	44+0	47+6	33+83805000	33+0	50+0	17+0	2+64	53	CEP
951 28964	20+75055500	20+0	45+0	2+0	15+97222200	15+0	59+0	50+0	4+49	12	DEL
952 28978	20+76382700	20+0	45+0	46+9	-9+62499990	-9+0	37+0	30+0	3+83	2	DEL
953 28979	20+76483300	20+0	45+0	53+4	-5+15694440	-5+0	9+0	28+0	4+60	3	ABR
954 28994	20+76738800	20+0	46+0	2+4	36+36111000	36+0	21+0	40+0	4+47	54	CYG
955 29079	20+82891600	20+0	49+0	44+1	-27+05138800	-27+0	3+0	5+0	4+24	18	W
956 29150	20+86677700	20+0	52+0	4+4	44+25388800	44+0	15+0	19+0	4+68	57	CYG
957 29133	20+86813800	20+0	52+0	5+3	-58+58777800	-58+0	35+0	16+0	3+72	0	IND
958 29251	20+93111100	20+0	55+0	52+0	41+03166600	41+0	1+0	54+0	4+04	58	N
959 29331	20+98580500	20+0	59+0	8+9	-32+39583300	-32+0	23+0	45+0	4+71	0	MIC
960 29459	21+06091600	21+0	3+0	39+3	43+78750000	43+0	47+0	15+0	3+92	62	C
961 29440	21+06636100	21+0	3+0	58+9	-17+37305500	-17+0	22+0	23+0	4+19	23	J
962 29490	21+08472100	21+0	5+0	5+0	-25+14694400	-25+0	8+0	49+0	4+60	24	CAP
963 29571	21+12813800	21+0	7+0	41+3	-11+51444440	-11+0	30+0	52+0	4+52	13	M
964 29661	21+19074900	21+0	11+0	26+7	30+08250000	30+0	4+0	57+0	3+40	44	Z
965 29591	21+22916000	21+0	12+0	46+5	9+84416660	9+0	51+0	43+0	4+76	5	W
966 29723	21+22319300	21+0	13+0	23+5	37+89522700	37+0	53+0	43+0	3+82	65	V
967 29735	21+23453500	21+0	14+0	4+4	5+10222220	5+0	6+0	8+0	4+14	8	A
968 29784	21+26730500	21+0	16+0	2+3	39+24722100	39+0	14+0	50+0	4+28	67	W
969 29802	21+27461100	21+0	16+0	28+4	34+74916600	34+0	44+0	57+0	4+42	66	U
970 29819	21+28949400	21+0	17+0	22+9	-53+59749900	-53+0	35+0	51+0	4+60	0	J
971 29848	21+29572200	21+0	17+0	44+6	62+43694400	62+0	13+0	26+0	2+60	5	A
972 29903	21+33833200	21+0	20+0	18+0	-16+98472200	-16+0	59+0	5+0	4+30	32	I
973 29914	21+34111100	21+0	20+0	28+0	19+65388800	19+0	39+0	14+0	4+24	1	PEG
974 29979	21+39288800	21+0	23+0	34+4	-65+52611100	-65+0	31+0	34+0	4+30	0	PAY
975 30020	21+41194000	21+0	24+0	40+3	-22+56388800	-22+0	33+0	50+0	3+84	34	Z
976 30059	21+44549900	21+0	26+0	43+8	-21+98055500	-21+0	57+0	28+0	4+59	36	CAP
977 30118	21+47024900	21+0	28+0	12+9	70+40694400	70+0	24+0	35+0	3+32	8	W
978 30137	21+49527700	21+0	29+0	43+0	-5+72611190	-5+0	43+0	34+0	3+07	22	W
979 30207	21+54436000	21+0	32+0	39+7	45+43688800	45+0	26+0	11+0	4+22	73	W
980 30252	21+58536100	21+0	35+0	7+3	-19+62388800	-19+0	37+0	26+0	4+72	39	Z
981 30289	21+62761100	21+0	39+4	39+4	-77+54722200	-77+0	32+0	50+0	3+74	0	M
982 30320	21+63588900	21+0	38+0	9+2	-16+82138800	-16+0	49+0	17+0	3+88	40	W
983 30440	21+70724900	21+0	42+0	26+1	58+61888800	58+0	37+0	8+0	4+00V	0	M

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

Star ID	Star Name	21+0	42+0	27+9	9+7	42+0	19+0	2+54	8 E	PE6	
984	30431 ENIF	21+70774900	21+0	42+0	27+9	9+71341100	42+0	19+0	8 E	PE6	
985	30438	21+70959300	21+0	42+0	34+5	28+58288900	35+0	2+0	7 M	CE6	
986	30444	21+71419300	21+0	42+0	34+5	17+10841100	11+0	19+0	9	PE6	
987	30439	21+71444000	21+0	42+0	52+0	-33+10433800	-33+0	11+0	9 I	PE6	
988	30450	21+71743000	21+0	43+0	3+5	25+40333300	29+0	11+0	10 K	PE6	
989	30483	21+74063800	21+0	44+0	26+3	60+95880800	60+0	32+0	10 M	CEP	
990	30491 DEMEB ALGIEDI	21+75183300	21+0	45+0	6+6	-14+28844400	-14+0	17+0	49 D	CAP	
991	30512	21+75827700	21+0	45+0	29+8	49+14694400	49+0	49+0	81 P	CY6	
992	30440	21+64358300	21+0	51+0	48+9	-37+53027800	-37+0	31+0	0 G	GRU	
993	30720	21+92580500	21+0	55+0	32+9	-55+15999700	-55+0	34+0	0 D	IND	
994	30817	22+01158300	22+0	4+0	41+7	-56+93111000	-56+0	52+0	0 E	IND	
995	30844	22+02505500	22+0	1+0	30+2	-2+32499970	-2+0	19+0	31 O	ARR	
996	30877	22+04249000	22+0	2+0	46+5	64+45694300	64+0	27+0	17 C	CEP	
997	30896 SADALMELEK	22+06841600	22+0	3+0	59+1	-+49055555	+0	29+0	34 A	ARR	
998	30892	22+06883300	22+0	4+0	6+6	-39+71305500	-39+0	47+0	0 L	GRU	
999	30814	22+07580500	22+0	4+0	32+9	-14+04027770	-14+0	25+0	33 I	ARR	
1000	30932	22+08963900	22+0	5+0	22+7	25+17333300	25+0	10+0	24 I	PE6	
1001	30942 NAQIR	22+10058300	22+0	6+0	2+1	-47+13138900	-47+0	7+0	0 A	GRU	
1002	30954	22+10575000	22+0	6+0	20+7	-33+16027700	-33+0	37+0	462	14 M	PEA
1003	31014	22+14099900	22+0	8+0	25+8	33+00583300	33+0	21+0	29 P	PE6	
1004	31013	22+14055500	22+0	8+0	26+0	6+02500000	6+0	30+0	24 J	PE6	
1005	31044	22+16061100	22+0	9+0	38+2	58+02833300	58+0	42+0	21 Z	CEP	
1006	31104	22+20622200	22+0	12+0	22+9	39+54055500	39+0	26+0	1	LAC	
1007	31135	22+22905500	22+0	13+0	44+6	56+88861100	56+0	52+0	23 E	CEP	
1008	31143	22+24064600	22+0	14+0	26+4	37+57388800	37+0	24+0	4+2	1 LAC	
1009	31152 ANCHA	22+24977700	22+0	14+0	59+2	-7+95833330	-7+0	30+0	43 J	ARR	
1010	31183	22+26863900	22+0	16+0	7+1	-60+43999900	-60+0	26+0	2	TIC	
1011	31252	22+32625000	22+0	19+0	34+5	46+35972200	46+0	21+0	2	LAC	
1012	31257 SADALACHBIA	22+33808000	22+0	19+0	50+9	-1+56444444	-1+0	33+0	48 B	ARR	
1013	31310	22+33963300	22+0	22+0	10+7	52+05305500	52+0	11+0	458	3 B	LAC
1014	31326	22+38860000	22+0	23+0	5+5	49+29833300	49+0	17+0	4+6	LAC	
1015	31328	22+39147100	22+0	23+0	29+3	1+19916866	1+0	11+0	52 P	ARR	
1016	31399	22+45099900	22+0	27+0	1+8	-+20000000	+0	12+0	55 Z	ARR	
1017	31400	22+45305500	22+0	27+0	11+0	-43+67499900	-43+0	30+0	0 D	GRU	
1018	31412	22+46122100	22+0	27+0	40+4	-43+92916600	-43+0	45+0	0 D	GRU	
1019	31421	22+46444400	22+0	27+0	52+0	58+23555500	58+0	14+0	27 D	CEP	
1020	31426	22+46780500	22+0	28+0	4+1	47+52722200	47+0	31+0	5	CAC	
1021	31449	22+48286000	22+0	28+0	58+3	42+94361000	42+0	54+0	454	LAC	
1022	31459	22+49199900	22+0	29+0	31+2	-32+52811000	-32+0	31+0	4+6	PEA	
1023	31471	22+49741600	22+0	29+0	50+7	50+10194300	50+0	6+0	7 A	LAC	
1024	31534	22+55927700	22+0	33+0	33+4	-+29833322	+0	17+0	42 M	ARR	
1025	31646	22+64538900	22+0	38+0	43+4	-27+22666600	-27+0	13+0	1 E	PEA	
1026	31652	22+64958200	22+0	38+0	58+5	44+09305500	44+0	5+0	31	LAC	
1027	31664 MOHAM	22+66191600	22+0	39+0	42+9	10+64805540	10+0	38+0	42 Z	PE6	
1028	31685	22+67641600	22+0	40+0	35+1	-47+06833300	-47+0	4+0	0 B	GRU	
1029	31704 MATAR	22+68930500	22+0	41+0	21+5	30+03777700	30+0	16+0	44 M	PE6	
1030	31712	22+70994400	22+0	42+0	35+8	-81+56811000	-81+0	33+0	0 B	DET	
1031	31776	22+74736000	22+0	44+0	50+5	23+38083300	23+0	22+0	47 L	PE6	
1032	31778	22+74902700	22+0	44+0	56+5	-11+99277770	-11+0	59+0	46 C	PE6	
1033	31813	22+77413800	22+0	46+0	26+9	-51+50138800	-51+0	30+0	0 E	GRU	
1034	31836	22+79564600	22+0	47+0	44+4	-13+77777770	-13+0	40+0	71 Y	ARR	
1035	31851	22+80516600	22+0	48+0	18+6	24+41638900	24+0	59+0	46 M	PE6	
1036	31857	22+80713800	22+0	48+0	25+7	66+01610000	66+0	58+0	32 I	CEP	
1037	31895	22+84305500	22+0	50+0	35+0	-33+06166600	-33+0	42+0	22 B	PEA	
1038	31903	22+84472000	22+0	50+0	47+3	-7+76638880	-7+0	45+0	73 L	ARR	
1039	31943 SKAT	22+87988800	22+0	52+0	47+6	-14+00749900	-14+0	27+0	74 D	ARR	
1040	31974	22+90022100	22+0	54+0	4+8	-32+72722100	-32+0	43+0	433	PEA	
1041	32000 FOMALHAUT	22+92866600	22+0	55+0	43+2	-29+80833300	-29+0	30+0	23 A	PEA	

TABLE I. - STAR IDENTIFICATION CATALOGUE - Concluded

1042	32061	22-98034100	22.0	58.0	49.3	-52.94222200	-52.0	56.0	32.0	4.18	0 2	GRU
1043	32095	23-00508300	23.0	.0	18.3	42.13749900	42.0	8.0	15.0	3.60V	1 0	AND
1044	32135	23-03455500	23.0	2.0	4.4	27.89249900	27.0	53.0	33.0	2.61	53 8	PEG
1045	32134	23-03488900	23.0	2.0	5.6	3.63138880	3.0	37.0	53.0	4.5W	4 8	PSC
1046	32149	23-05024900	23.0	3.0	.9	15.01666670	15.0	1.0	.0	2.57	54 A	PEG
1047	32184	23-08188800	23.0	4.0	5.8	-43.70999900	-43.0	42.0	36.0	4.35	3 0	GRU
1048	32176	23-08733300	23.0	5.0	14.4	9.21999990	9.0	13.0	12.0	4.69	55	PEG
1049	32237	23-11297100	23.0	6.0	4.7	75.19833200	75.0	11.0	54.0	4.54	33 P	CEP
1050	32246	23-12636100	23.0	7.0	34.9	-21.36277700	-21.0	21.0	46.0	3.80	88	ABR
1051	32270	23-13972100	23.0	8.0	23.0	-45.43666600	-45.0	25.0	12.0	4.10	0 1	GRU
1052	32316	23-18233300	23.0	10.0	56.4	49.21472100	49.0	12.0	53.0	4.62	7	AND
1053	32346	23-20847100	23.0	12.0	30.5	-6.23805550	-6.0	19.0	17.0	4.40	90 V	ABR
1054	32374	23-23430500	23.0	14.0	3.5	-9.27841110	-9.0	16.0	43.0	4.46	91 Y	ABR
1055	32415	23-25583200	23.0	15.0	21.0	3.07883330	3.0	5.0	27.0	3.85	4 6	PSC
1056	32413	23-25661000	23.0	15.0	23.8	-58.42805500	-58.0	25.0	41.0	4.10	0 6	TUC
1057	32429	23-26808300	23.0	16.0	5.1	-9.37388890	-9.0	28.0	26.0	4.56	93 V	ABR
1058	32450	23-28227800	23.0	16.0	56.2	-32.72305500	-32.0	43.0	23.0	4.51	0 6	SCL
1059	32503	23-31502700	23.0	18.0	54.1	23.54841100	23.0	34.0	55.0	4.65	42 Y	PEG
1060	32540	23-35222100	23.0	21.0	84.0	-20.29194400	-20.0	17.0	31.0	4.20	98	ABR
1061	32585	23-39380500	23.0	23.0	37.7	23.21111000	23.0	12.0	40.0	4.57	68 U	PEG
1062	32594	23-40347200	23.0	24.0	12.5	-20.83416600	-20.0	50.0	3.0	4.52	99	ABR
1063	32647	23-43649900	23.0	26.0	11.4	6.18638890	6.0	11.0	11.0	4.95	10 J	PSC
1064	32647	23-45634000	23.0	27.0	22.9	12.56722210	12.0	34.0	2.0	4.67	70	PEG
1065	32744	23-51830500	23.0	31.0	54.9	-38.01222100	-38.0	.0	44.0	4.44	0 8	SCL
1066	32832	23-59738900	23.0	35.0	50.6	46.26833300	46.0	16.0	6.0	4.00	16 L	AND
1067	32850	23-60688800	23.0	36.0	24.8	43.07416600	43.0	4.0	27.0	4.28	17 I	AND
1068	32875	23-62155500	23.0	37.0	53.6	77.43694300	77.0	26.0	13.0	3.42	35 8	CEP
1069	32879	23-63580500	23.0	38.0	8.9	5.43638890	5.0	24.0	11.0	4.28	17 1	PSC
1070	32884	23-64461000	23.0	38.0	40.4	44.14000000	44.0	6.0	24.0	4.33	19 K	AND
1071	32917	23-67097100	23.0	40.0	15.5	1.58749999	1.0	35.0	15.0	4.61	18 L	PSC
1072	32931	23-68177700	23.0	40.0	54.4	-14.73861110	-14.0	46.0	19.0	4.62	105 8	ABR
1073	33050	23-78508300	23.0	47.0	6.3	-28.32368900	-28.0	19.0	26.0	4.64	0 0	SCL
1074	33160	23-87708300	23.0	52.0	37.5	57.30472100	57.0	18.0	17.0	4.00V	7 R	CAS
1075	33230	23-93283200	23.0	55.0	58.2	24.94694400	24.0	54.0	49.0	4.75	84 V	PEG
1076	33282	23-95852700	23.0	57.0	30.7	6.66944440	6.0	40.0	10.0	4.03	28 W	PSC
1077	33280	23-96849900	23.0	58.0	6.6	-65.77194400	-65.0	46.0	19.0	4.71	0 E	TUC
1078	33321	23-99702700	23.0	59.0	49.3	-77.25888900	-77.0	15.0	32.0	4.73	0 J	OCT



TRANSLUNAR INJECTION  
BURN

TRANSLUNAR COAST

EARTH VIEWS

MOON VIEWS

LUNAR ORBIT  
INSERTION BURN

LUNAR ORBIT PHASE

TRANSEARTH INJECTION  
BURN

TRANSEARTH COAST

POST TEI

MOON VIEWS

EARTH VIEWS

ENTRY PHASE

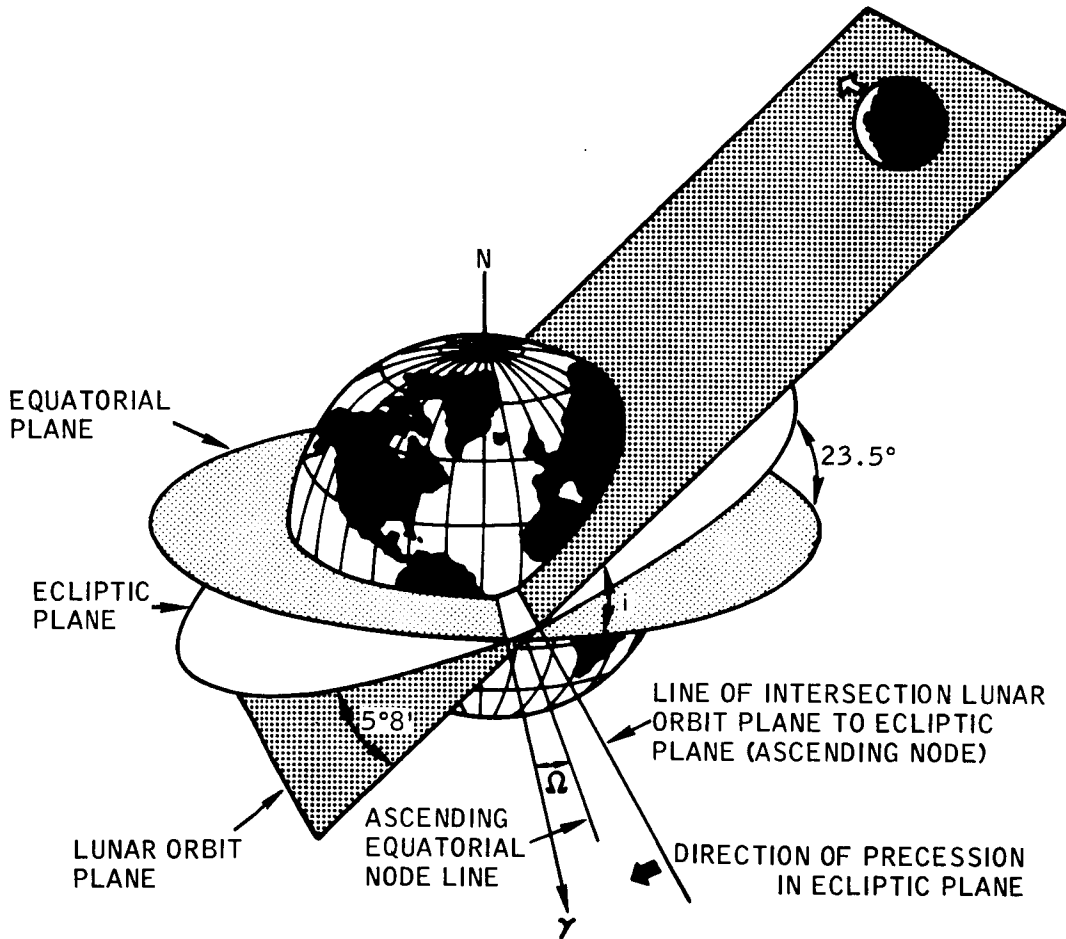


Figure 1. - Illustration of lunar orbit plane in year 1969 - inclination angle ( $i$ )  $\approx 28^\circ$ , right ascension of ascending equatorial node ( $\Omega$ )  $\approx 5^\circ$ .

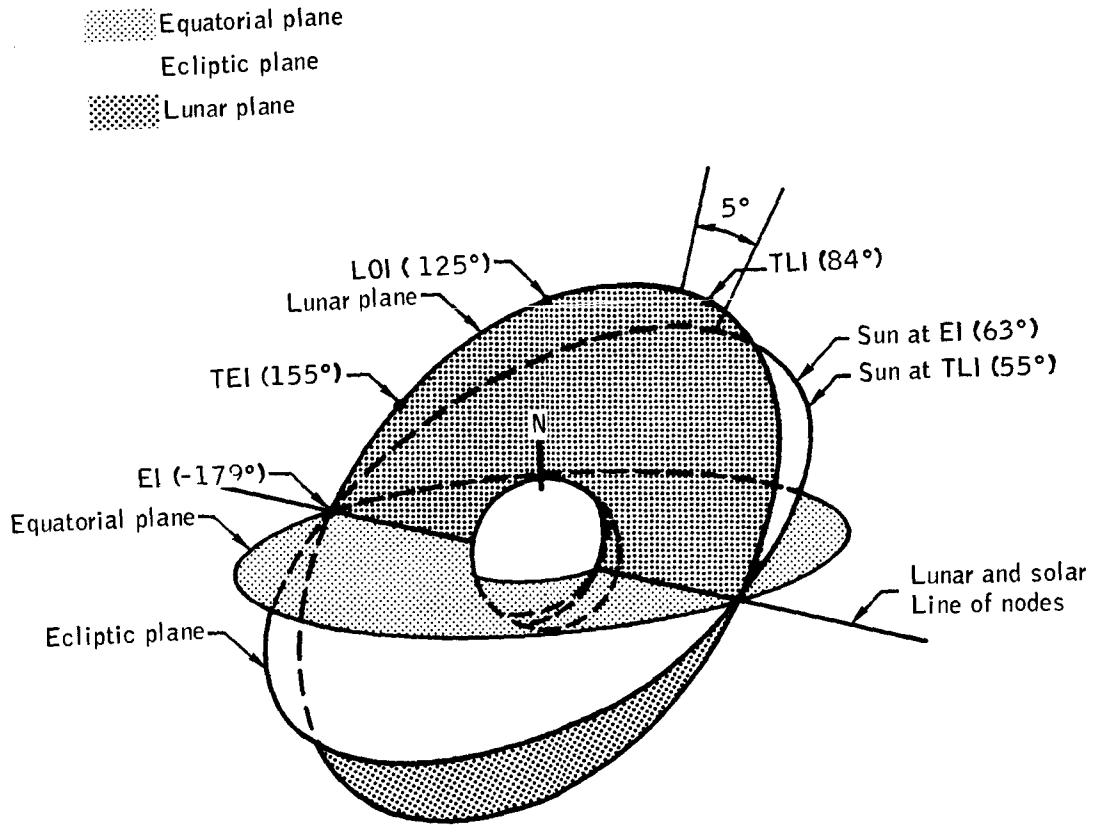


Figure 2.- Sun and moon location at major phases during Apollo 10 (Mission F).

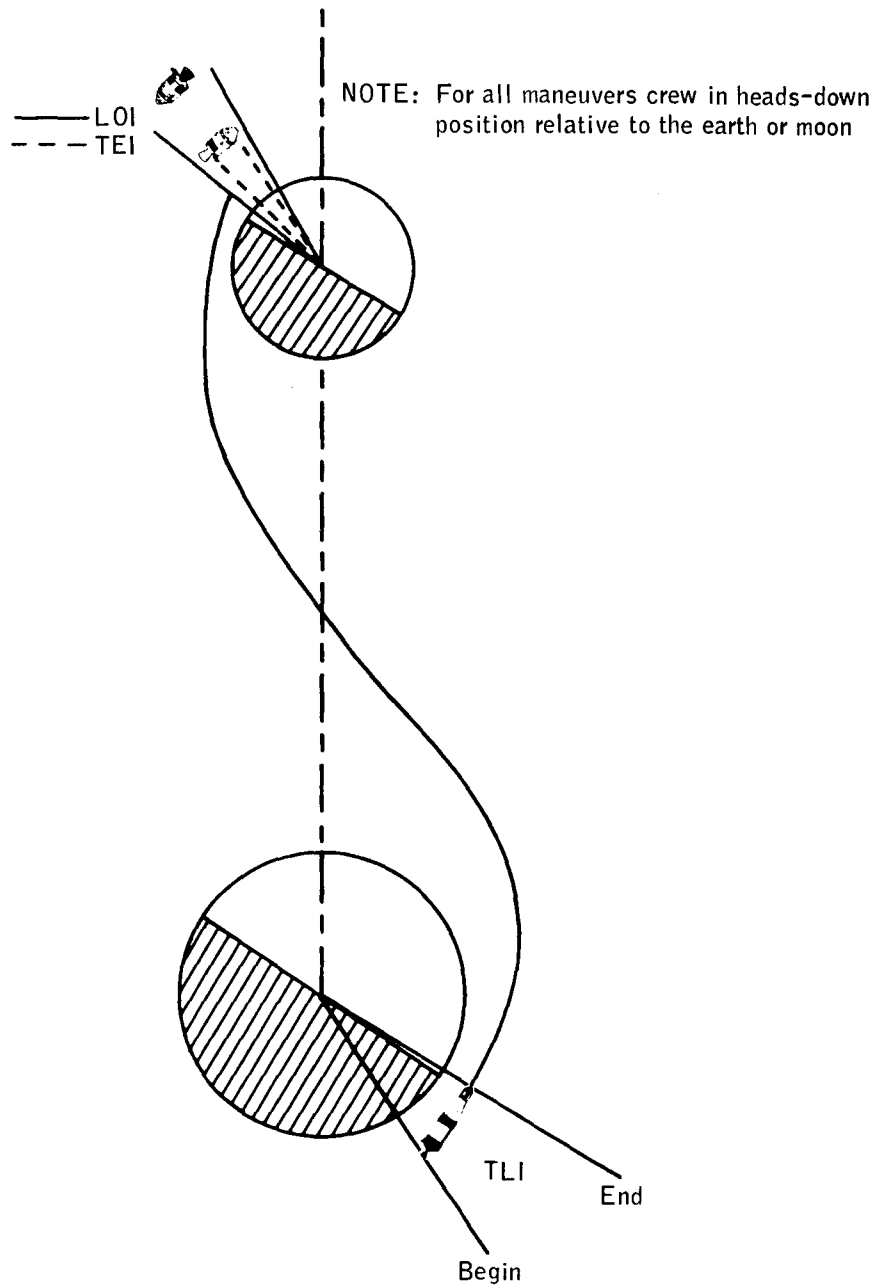


Figure 3. - A schematic of the maneuver attitudes and lighting conditions for the nominal Apollo 10 (Mission F).

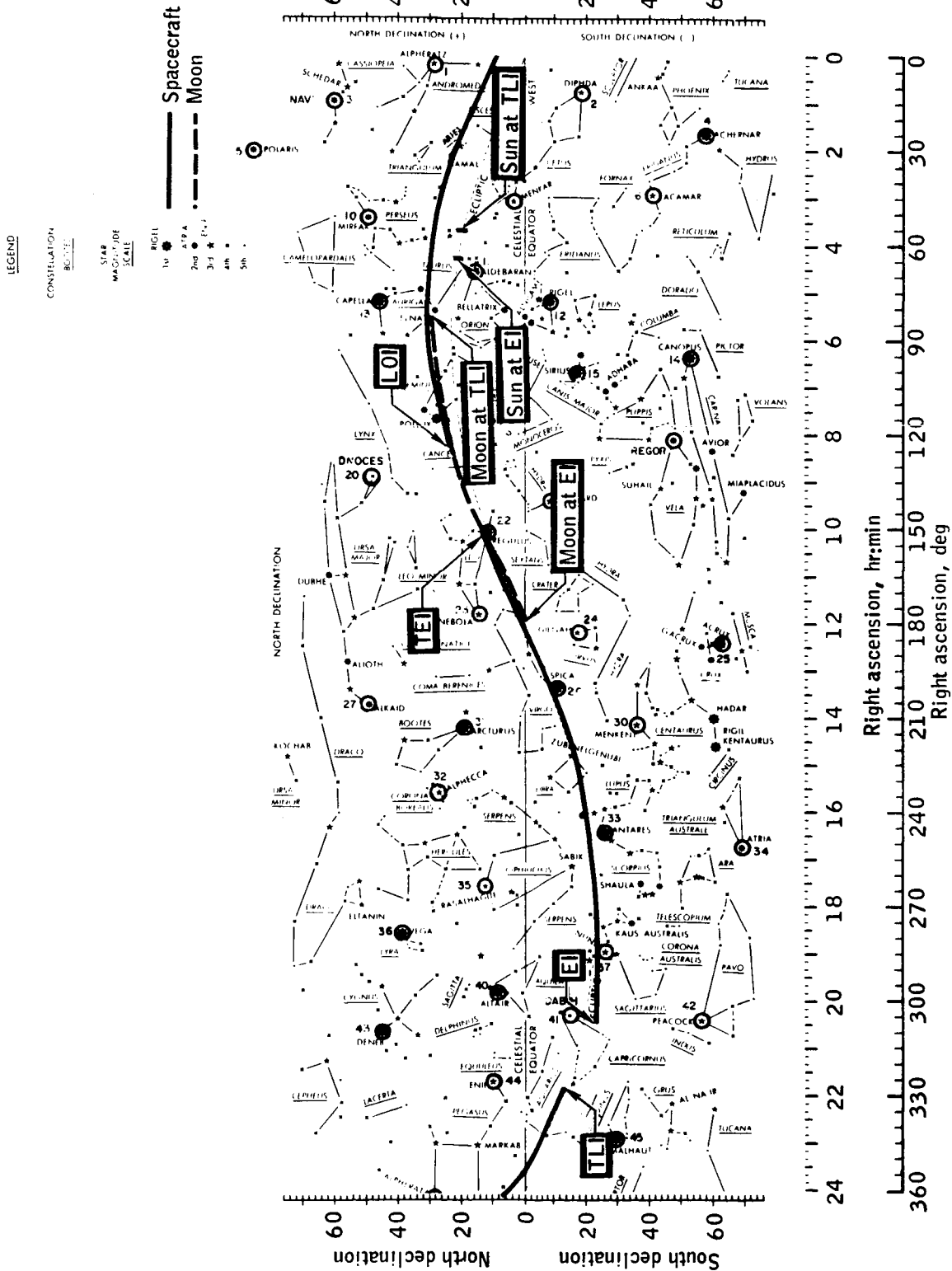


Figure 4. - Nominal Apollo 10 (Mission F) projected on a map of the celestial sphere.

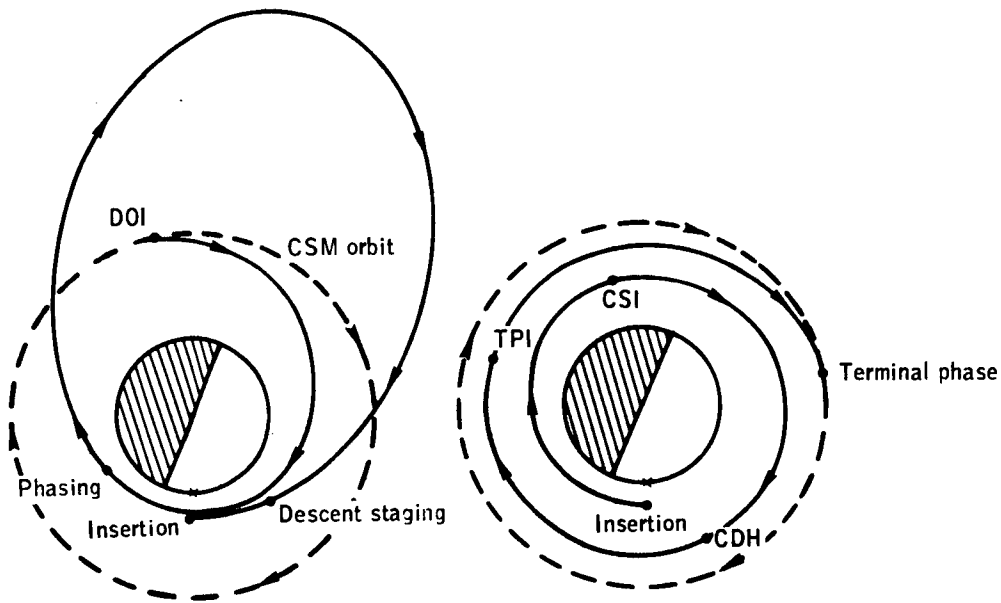


Figure 5. - F mission nominal rendezvous.

TRANSLUNAR INJECTION  
BURN

SEC	4	5	7	15	22	25	41	63	75	80	984	1044	1046
X	9	20	3	-23	18	=13	8	C	0	=12	12	13	8
Y	=4	5	=8	=20	6	=13	2	3	5	0	-24	=10	=14

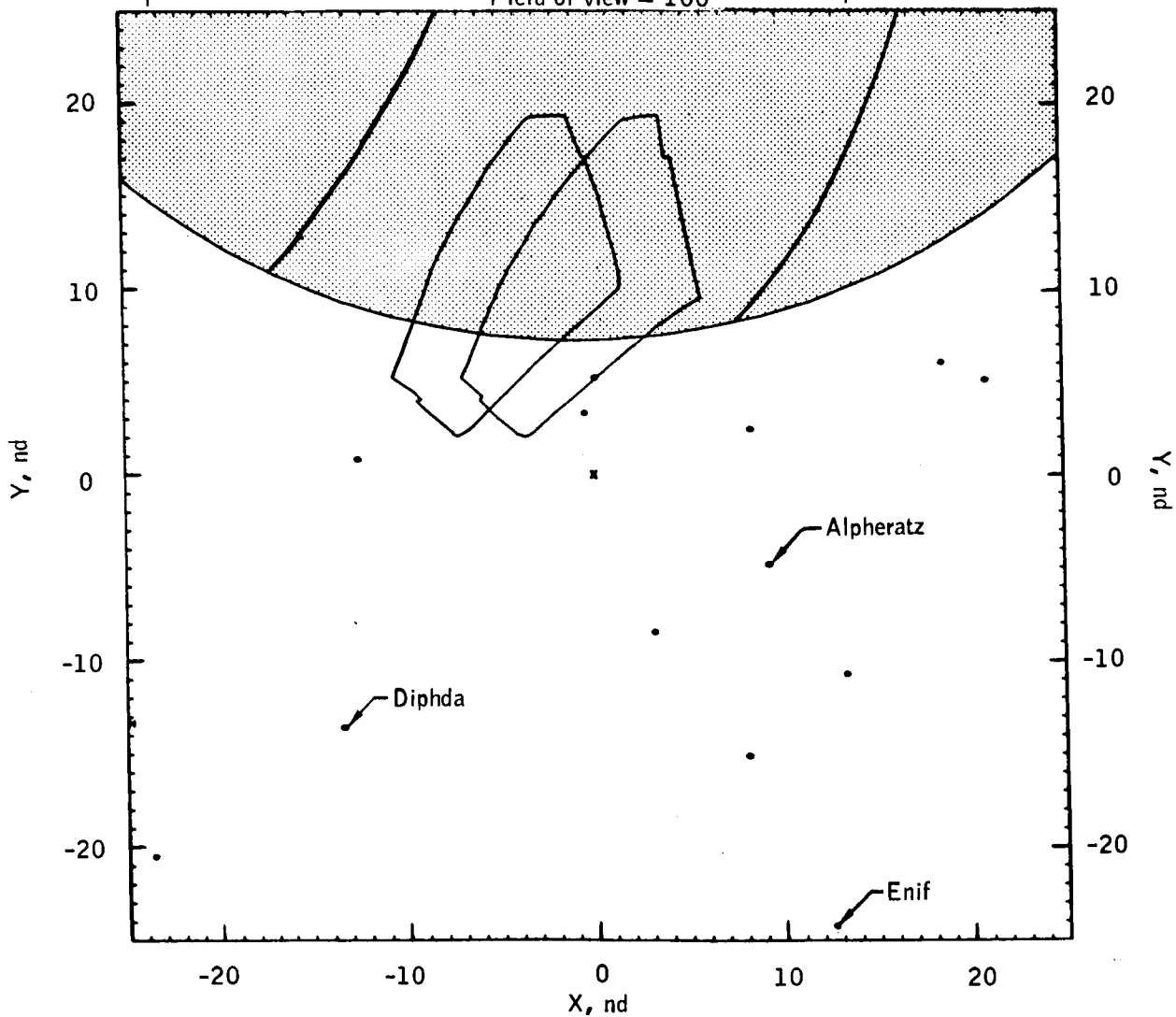
$R_E = 3547$  n. mi.

$V_i = 25\,568$  fps

$h_E = 121$  stat. mi.

$V_i = 17\,433$  mph

Field of view =  $100^\circ$



(a) Begin TLI (g.e.t. = 2:33:17.7).

Figure 6. - Translunar injection burn.



SEQ	4	5	7	15	22	25	31	41	47	63	73	75	80
X	11	22	5	=23	20	-11	21	10	19	1	10	2	-10
Y	-10	0	-14	=24	1	-19	3	-3	5	-2	3	0	=4

SEQ	108	1044	1046
X	-9	15	10
Y	1	-16	-20

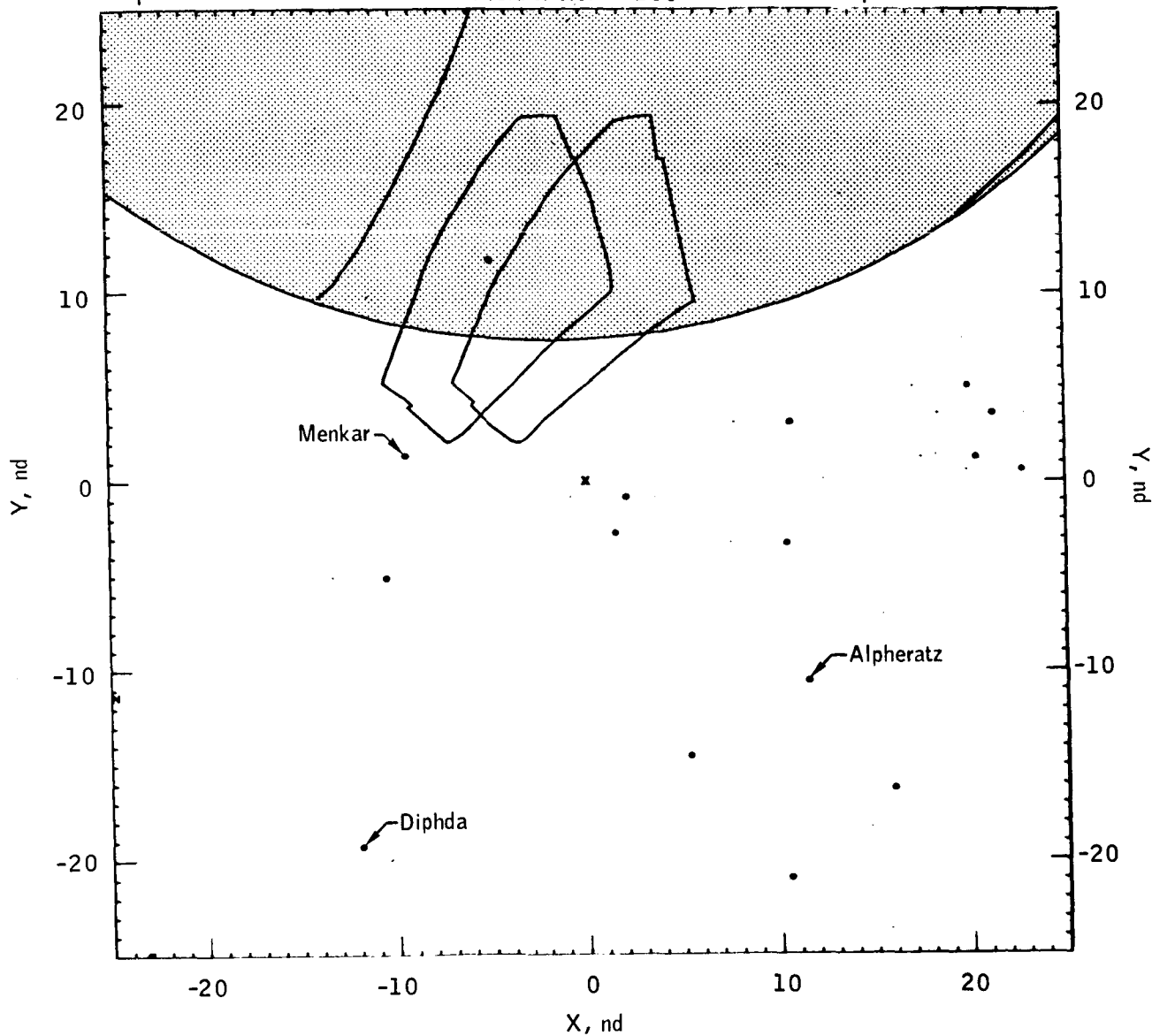
$R_E = 3552$  n. mi.

$h_E = 127$  stat. mi.

$V_i = 29\ 517$  fps

$V_i = 20\ 125$  mph

Field of view =  $100^\circ$



(b) Middle of TLI (g.e.t. = 2:36:08.0).

Figure 6. - Continued.

SEQ	4	5	7	22	25	31	41	47	63	73	75	80	100
X	13	24	6	22	-11	22	12	21	3	12	3	-8	-9
Y	-14	-2	-18	=2	=22	0	=7	1	-6	=1	=5	=8	=2
SEQ	111	112	120	144	150	151	186	215	1044				
X	8	9	13	0	3	7	-4	-16	17				
Y	3	4	7	5	7	8	10	11	-20				

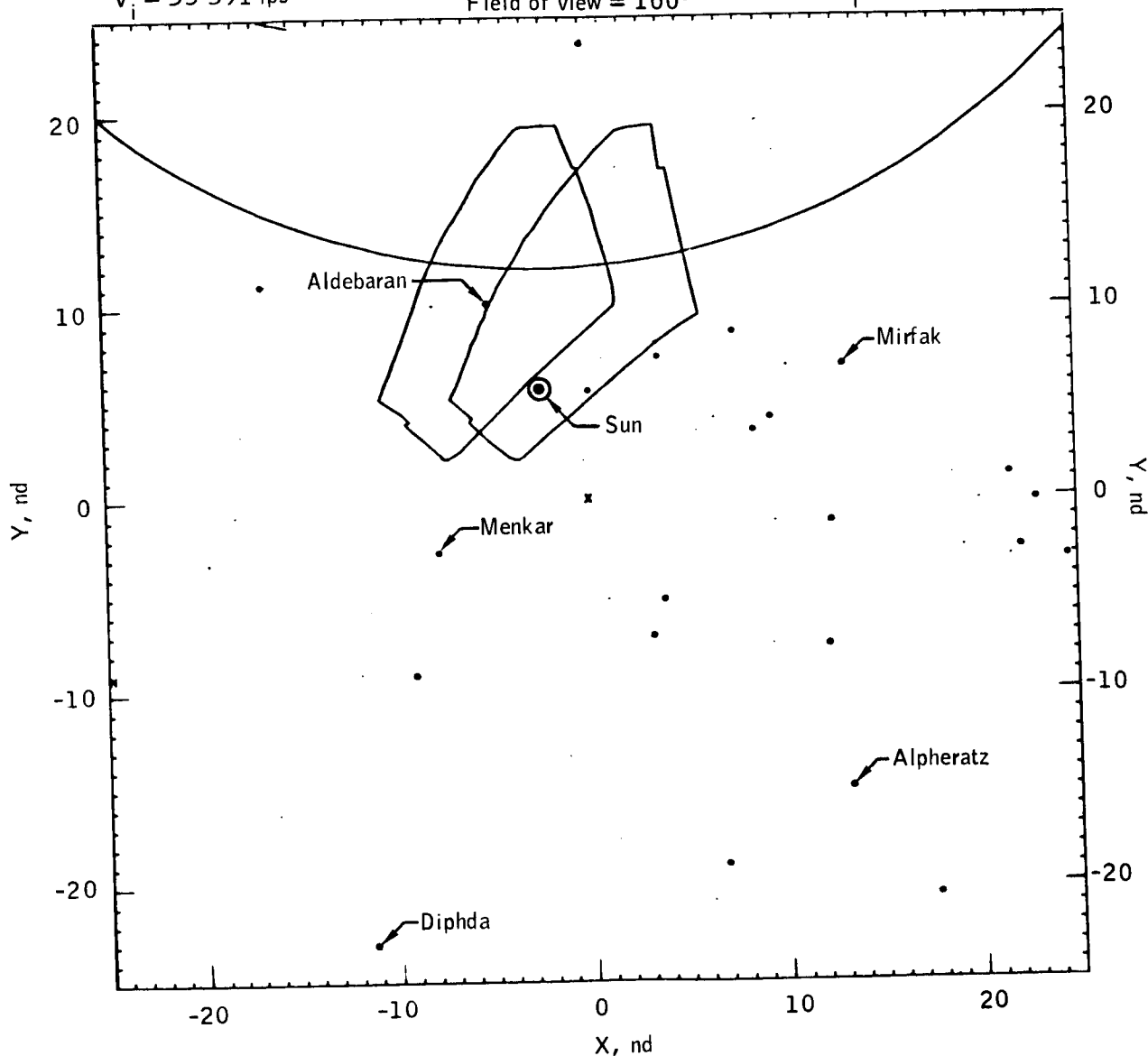
$R_E = 3613$  n. mi.

$V_i = 35\,591$  fps

$h_E = 196$  stat. mi.

$V_i = 24\,267$  mph

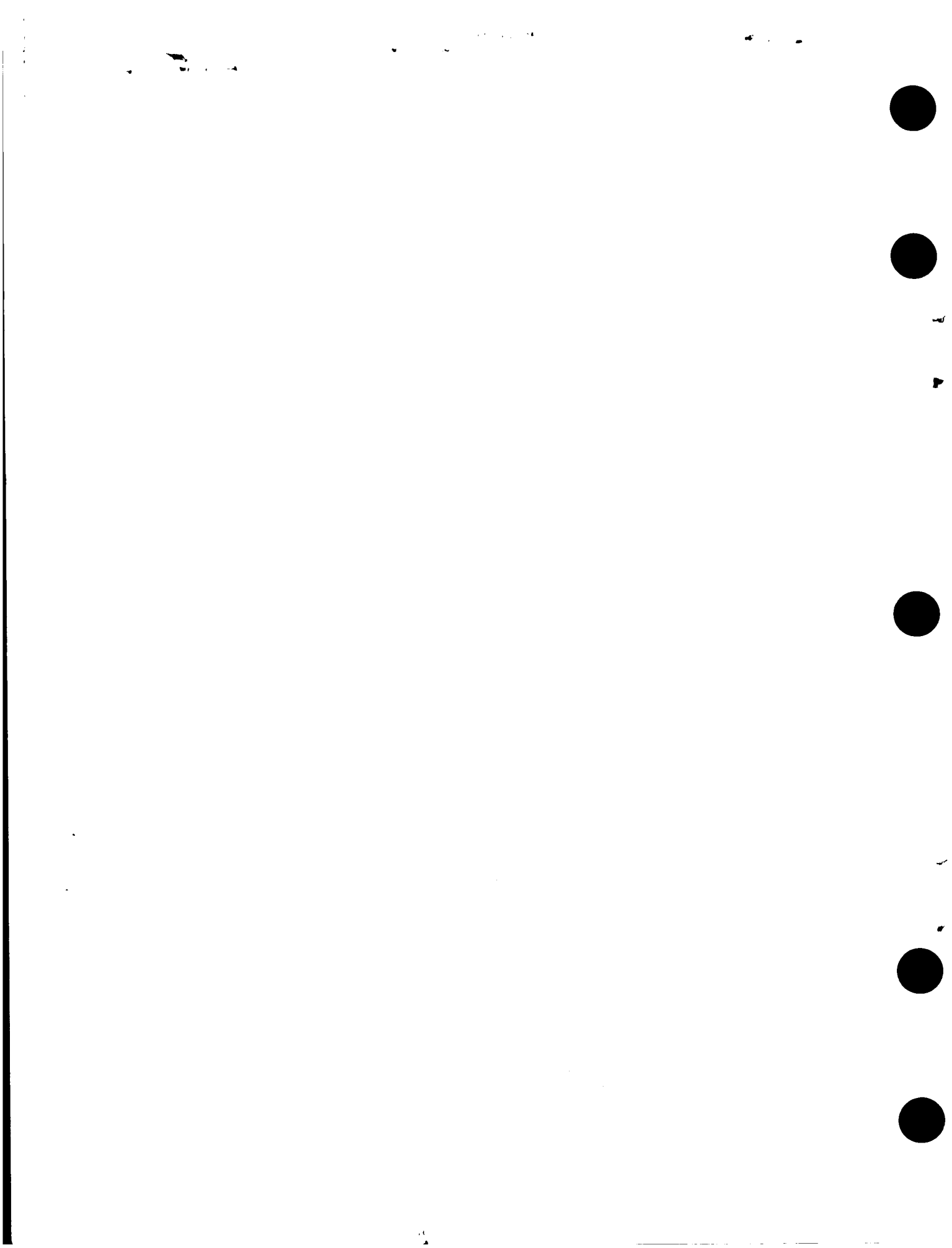
Field of view =  $100^\circ$



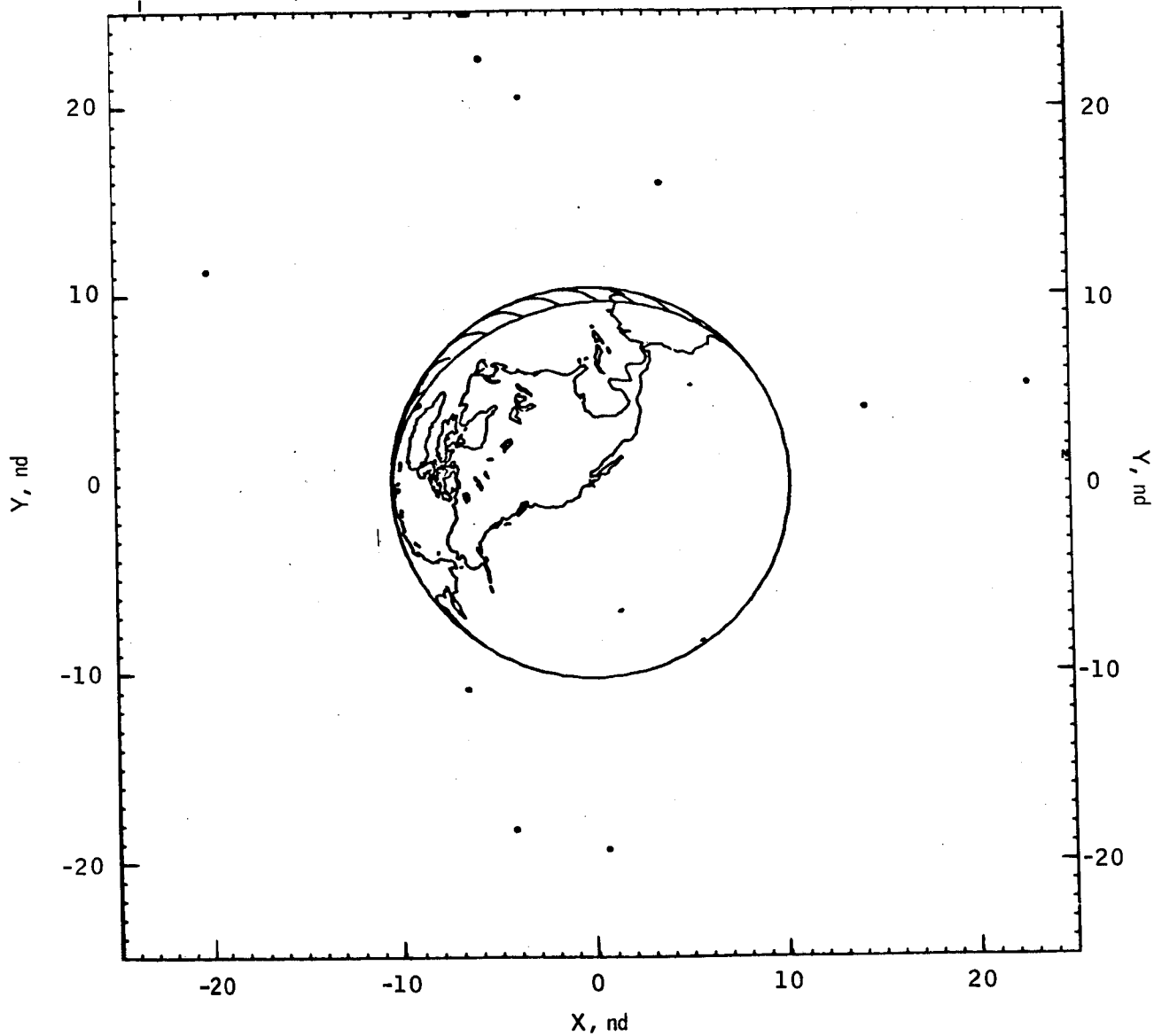
(c) End of TLI (g.e.t. = 2:38:59.5).

Figure 6. - Concluded.

TRANSLUNAR COAST



EARTH VIEWS

$R_E = 24\,019 \text{ n. mi.}$ 
 $V_i = 13\,352 \text{ fps}$ 
 $h_E = 23\,681 \text{ stat. mi.}$ 
 $V_i = 9104 \text{ mph}$ 
Field of view =  $40^\circ$ 

(a) G.e.t. = 5 hours.

Figure 7.- Translunar coast - constant field of view (earth).

SEQ	790	793	797	802	836	841	844
X	23	6	14	9	-1	4	-6
Y	25	25	24	22	12	12	9

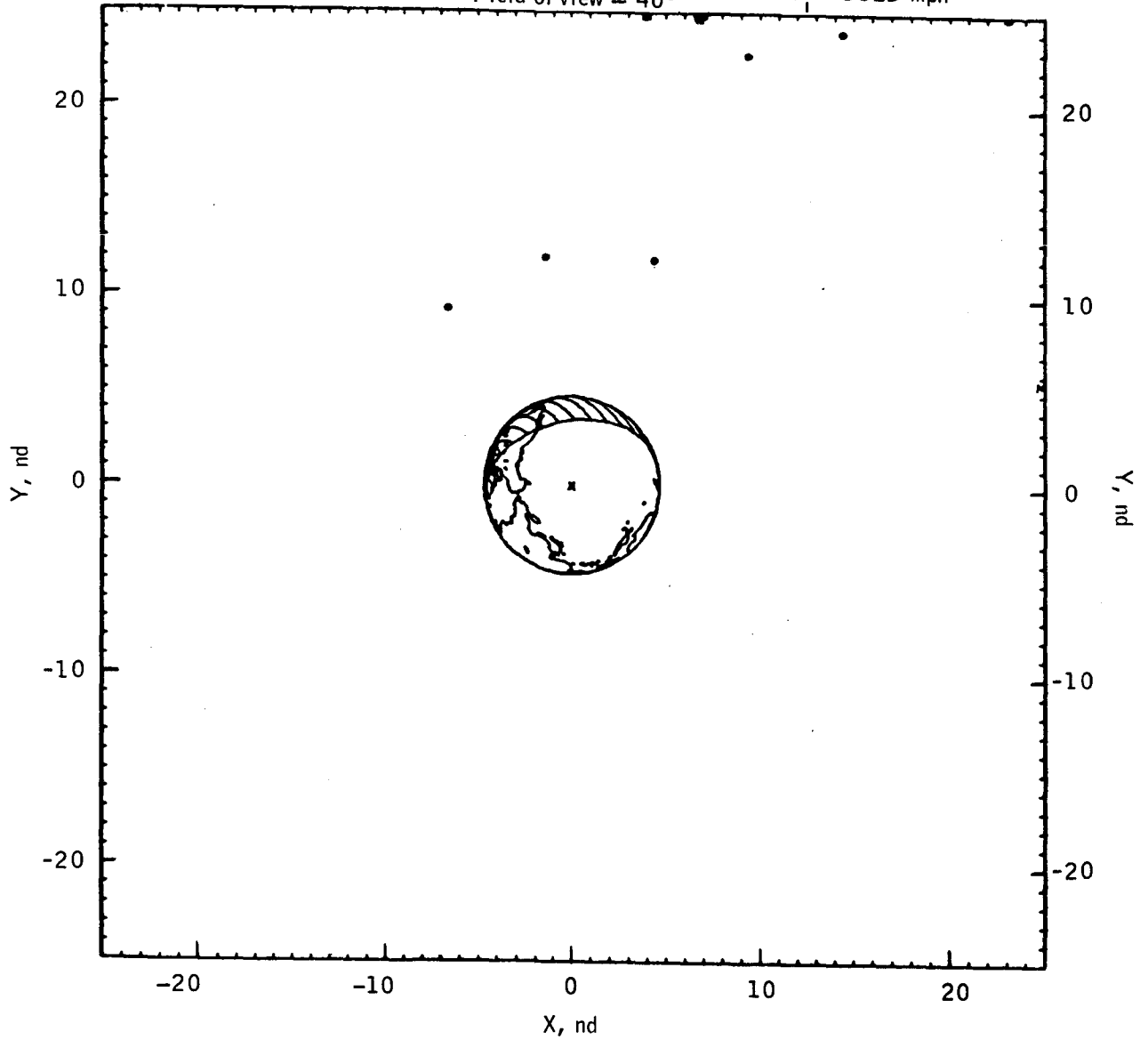
$R_E = 52\,882$  n.mi.

$V_i = 8541$  fps

$h_E = 56\,896$  stat. mi.

$V_i = 5823$  mph

Field of view =  $40^\circ$



(b) G.e.t. = 10 hours.

Figure 7.- Continued.

SEQ	836	841	844	861	871
X	-1	4	-6	-4	0
Y	22	22	19	12	11

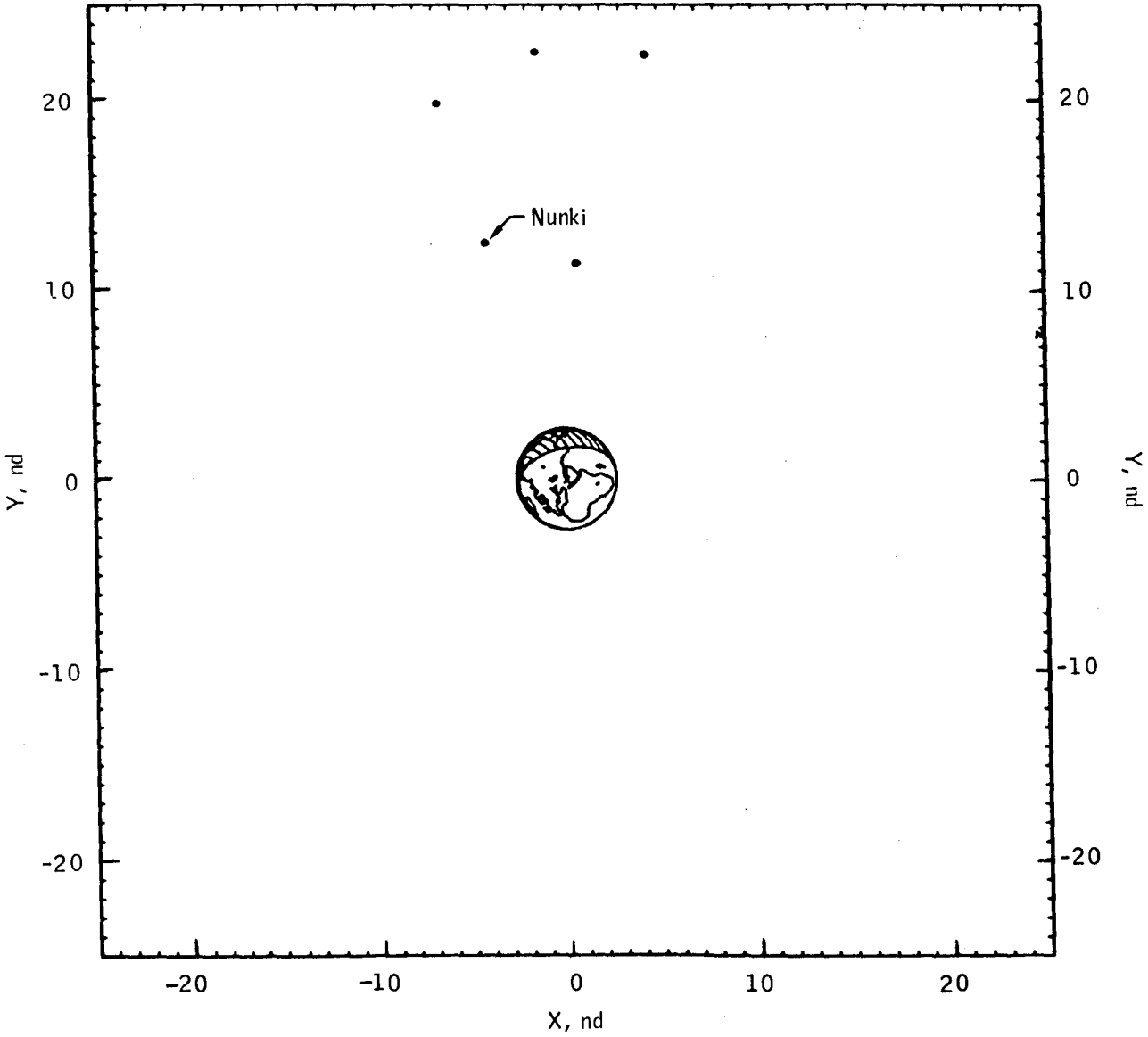
$R_E = 93\,028$  n. mi.

$h_E = 103\,440$  stat. mi.

$V_i = 5930$  fps

Field of view =  $40^\circ$

$V_i = 4043$  mph



(c) G.e.t. = 20 hours.

Figure 7.- Continued.

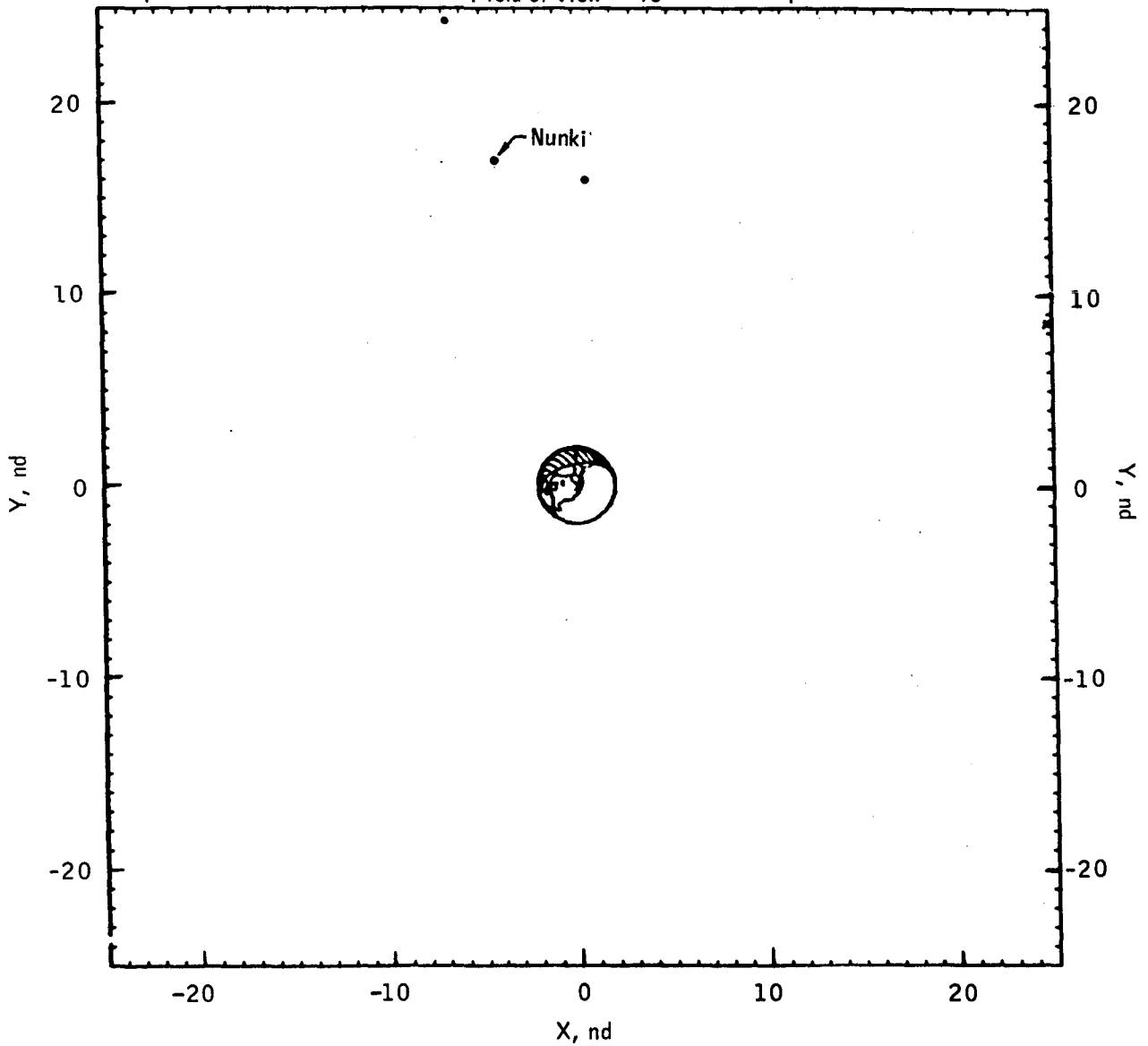


SEQ	044	061	071
X	-6	74	0
Y	24	17	16

 $R_E = 123\,687$  n. mi.

 $V_i = 4782$  fps

 $h_E = 138\,375$  stat. mi.

 $V_i = 3260$  mph
Field of view =  $40^\circ$ 

(d) G.e.t. = 30 hours.

Figure 7.- Continued.

SEQ 061 071  
 X -4 0  
 Y 19 18

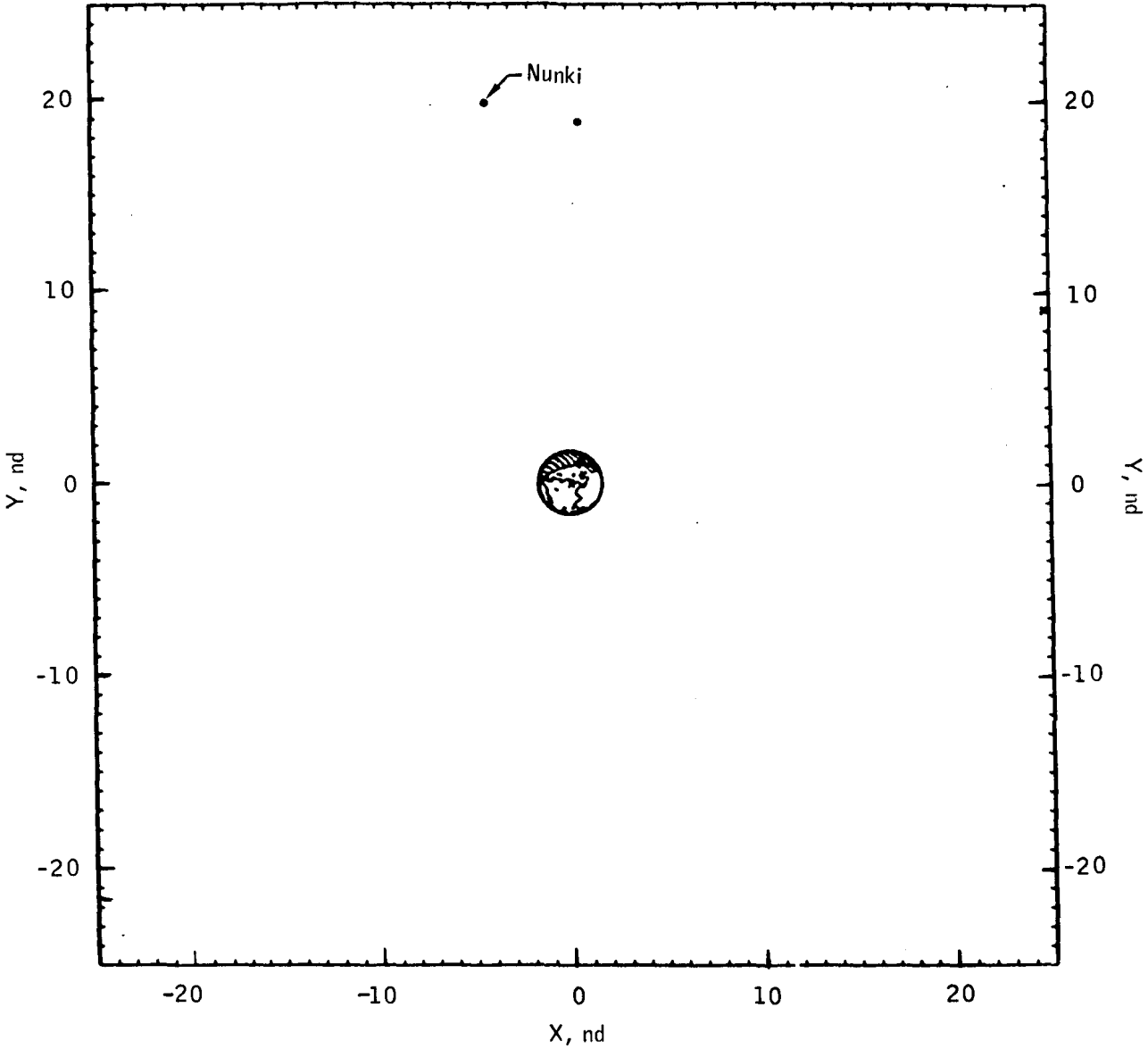
$R_E = 149\,206$  n. mi.

$h_E = 167\,742$  stat. mi.

$V_i = 4067$  fps

$V_i = 2773$  mph

Field of view =  $40^\circ$



(e) G.e.t. = 40 hours.

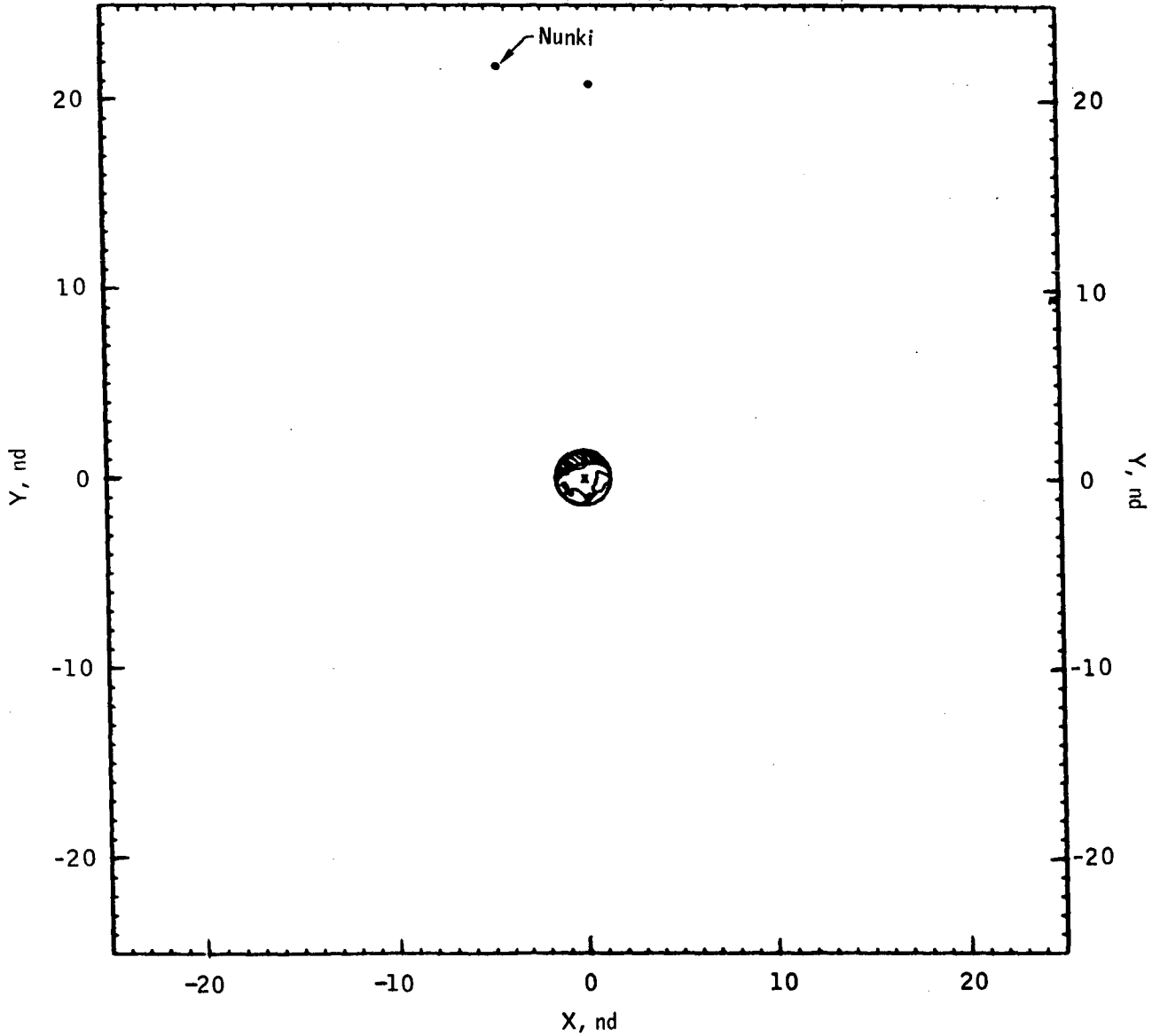
Figure 7.- Continued.

SEQ 061 071  
 X =4 0  
 Y 21 20

$R_E = 171\,265$  n. mi.  
 $V_i = 3557$  fps

$h_E = 193\,127$  stat. mi.  
 $V_i = 2425$  mph

Field of view =  $40^\circ$



(f) G.e.t. = 50 hours.

Figure 7.- Continued.

SEQ 061 071  
 X -4 0  
 Y 23 22

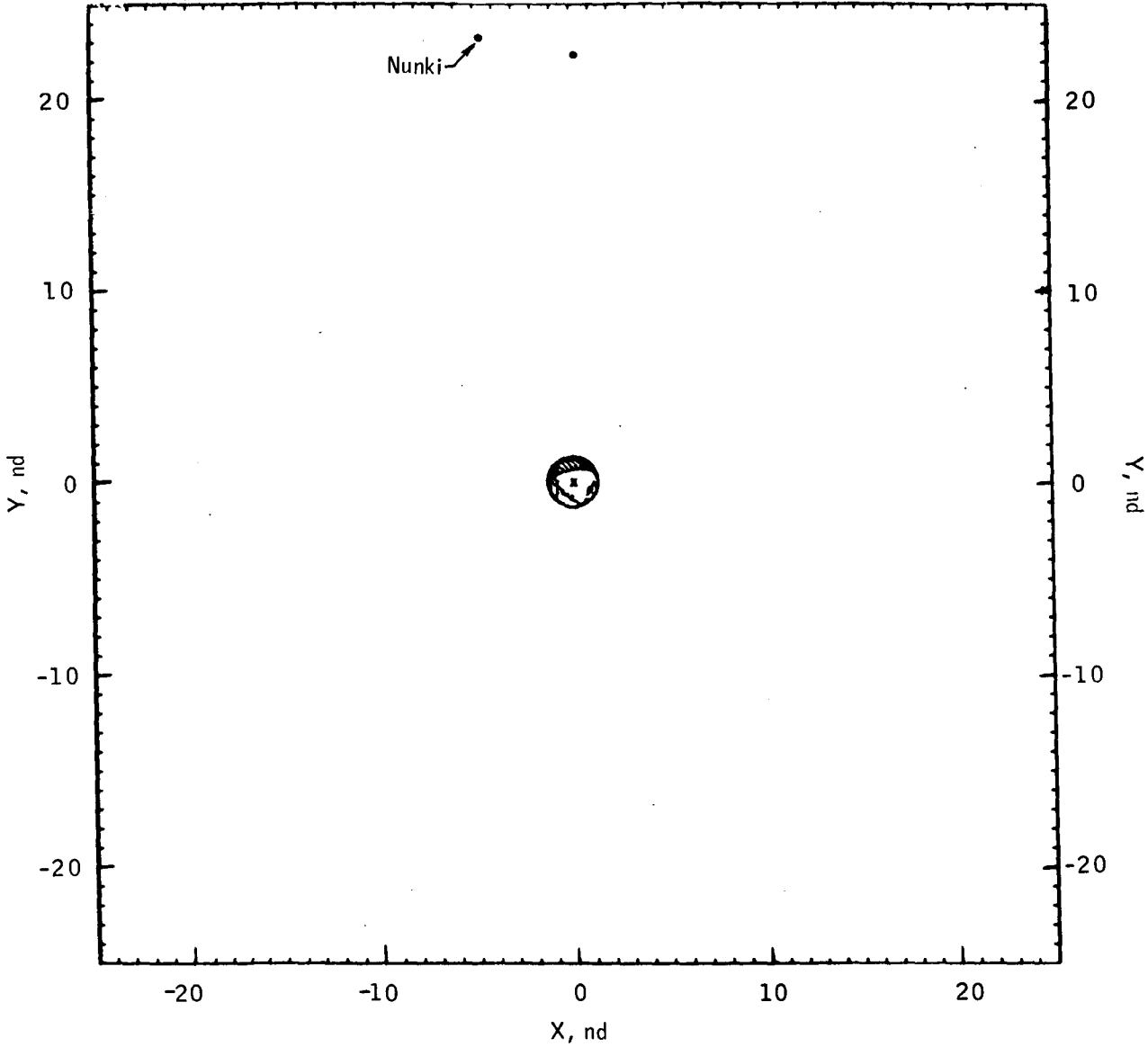
$R_E = 190\,809$  n. mi.

$V_i = 3182$  fps

$h_E = 187\,368$  stat. mi.

$V_i = 2170$  mph

Field of view =  $40^\circ$



(g) G.e.t. = 60 hours.

Figure 7.- Continued.

SEQ	844	861	871	990
X	-22	-16	-12	16
Y	23	18	20	-21

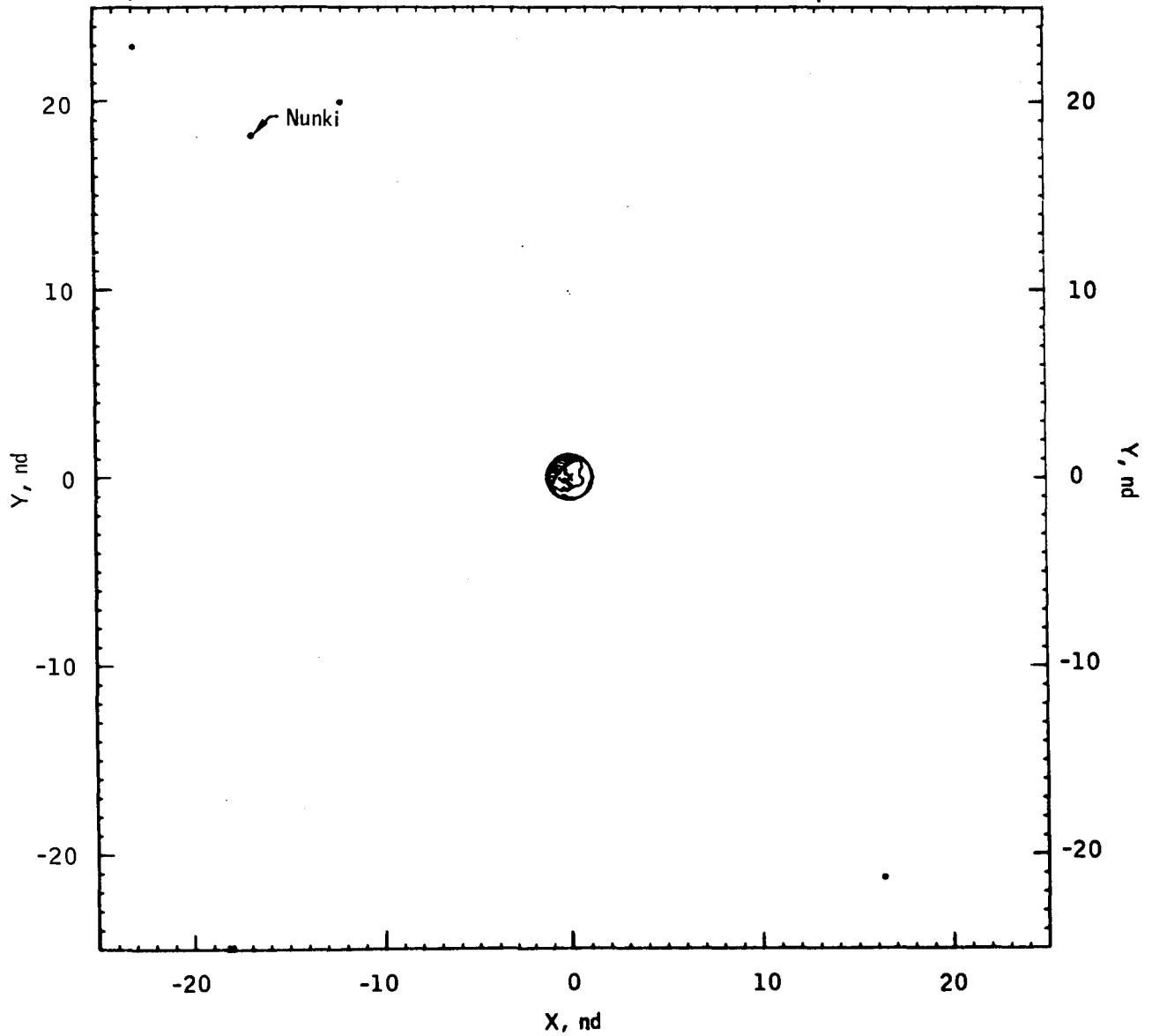
$R_M = 15\,709$  n. mi.

$V_i = 4031$  fps

Field of view =  $40^\circ$

$h_M = 16\,997$  stat. mi.

$V_i = 2748$  mph



(h) G.e.t. = 70 hours.

Figure 7.- Concluded.

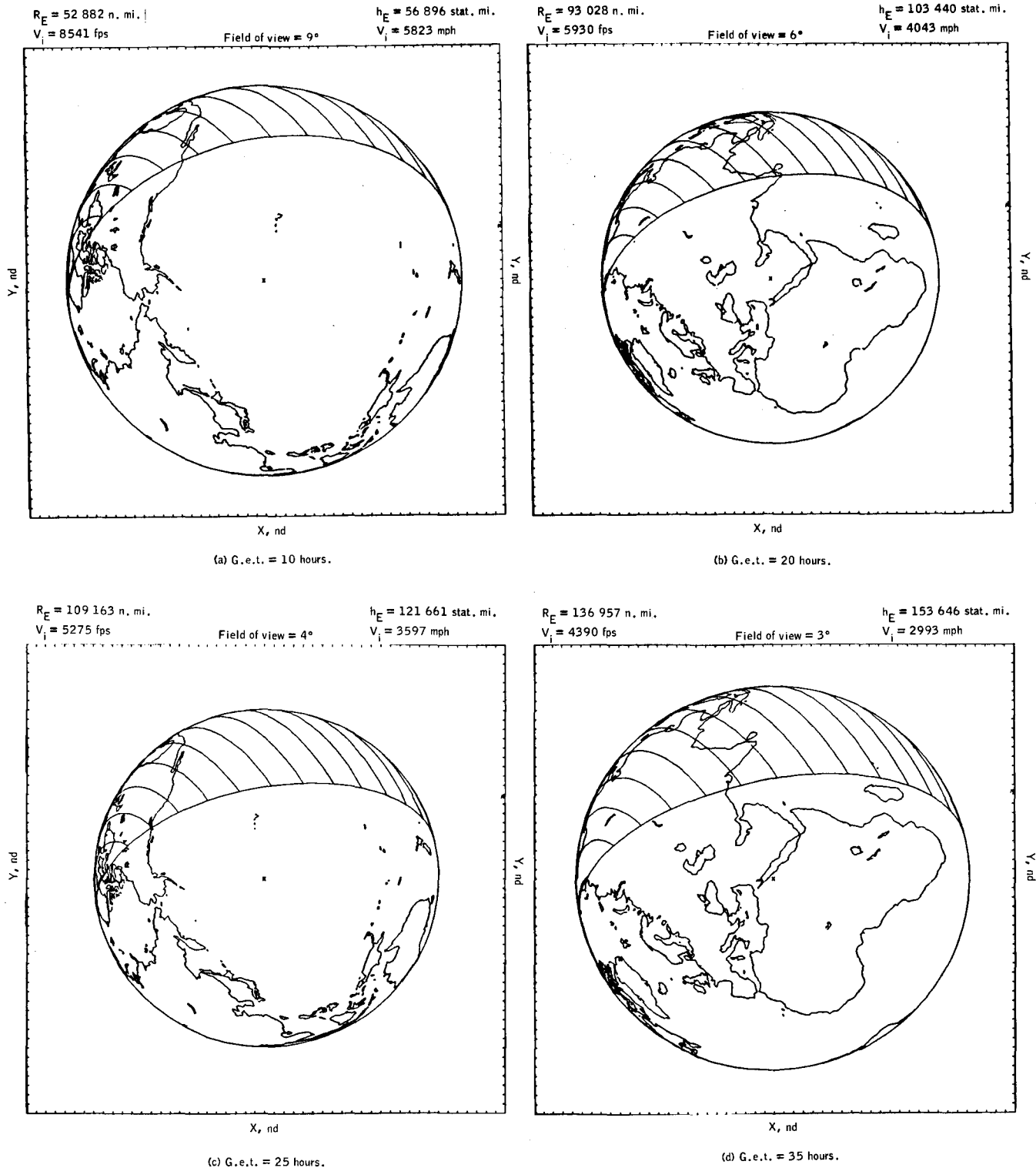
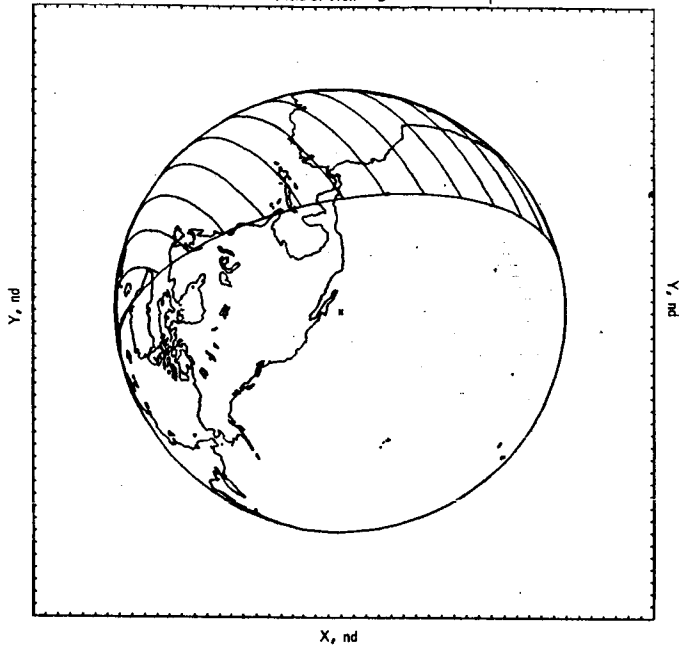


Figure 8.- Translunar coast - variable field of view (earth).

$R_E = 160\,600$  n. mi.       $h_E = 180\,853$  stat. mi.  
 $V_i = 3793$  fps       $V_i = 2586$  mph  
 Field of view =  $3^\circ$

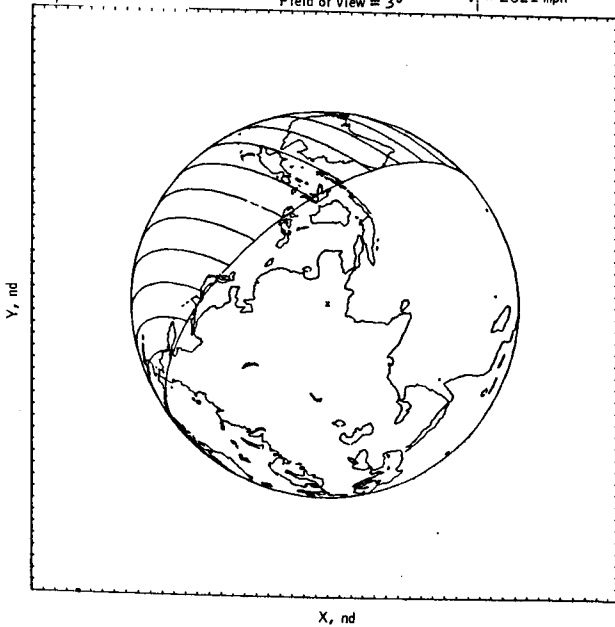


(e) G.e.t. = 45 hours.

$R_M = 27\,254$  n. mi.  
 $V_i = 3844$  fps

Field of view =  $3^\circ$

$h_M = 30\,284$  stat. mi.  
 $V_i = 2621$  mph

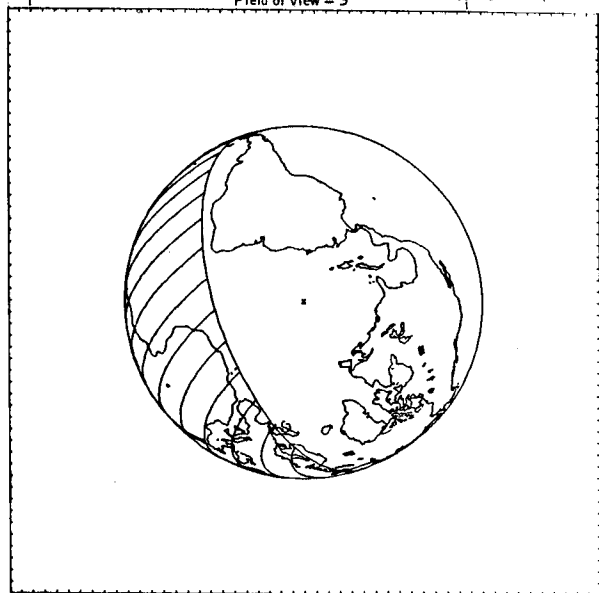


(f) G.e.t. = 65 hours.

$R_M = 3055$  n. mi.  
 $V_i = 5591$  fps

Field of view =  $3^\circ$

$h_M = 2436$  stat. mi.  
 $V_i = 3821$  mph



(g) G.e.t. = 75 hours.

Figure 8.- Concluded.

MOON VIEWS



SEQ	150	186	205	207	222	230	231	248	265	270	271	281	301
X	21	0	11	20	21	-20	2	-7	-24	14	6	-11	-21
Y	-17	-21	-3	5	9	-17	-1	-3	-9	17	12	6	8

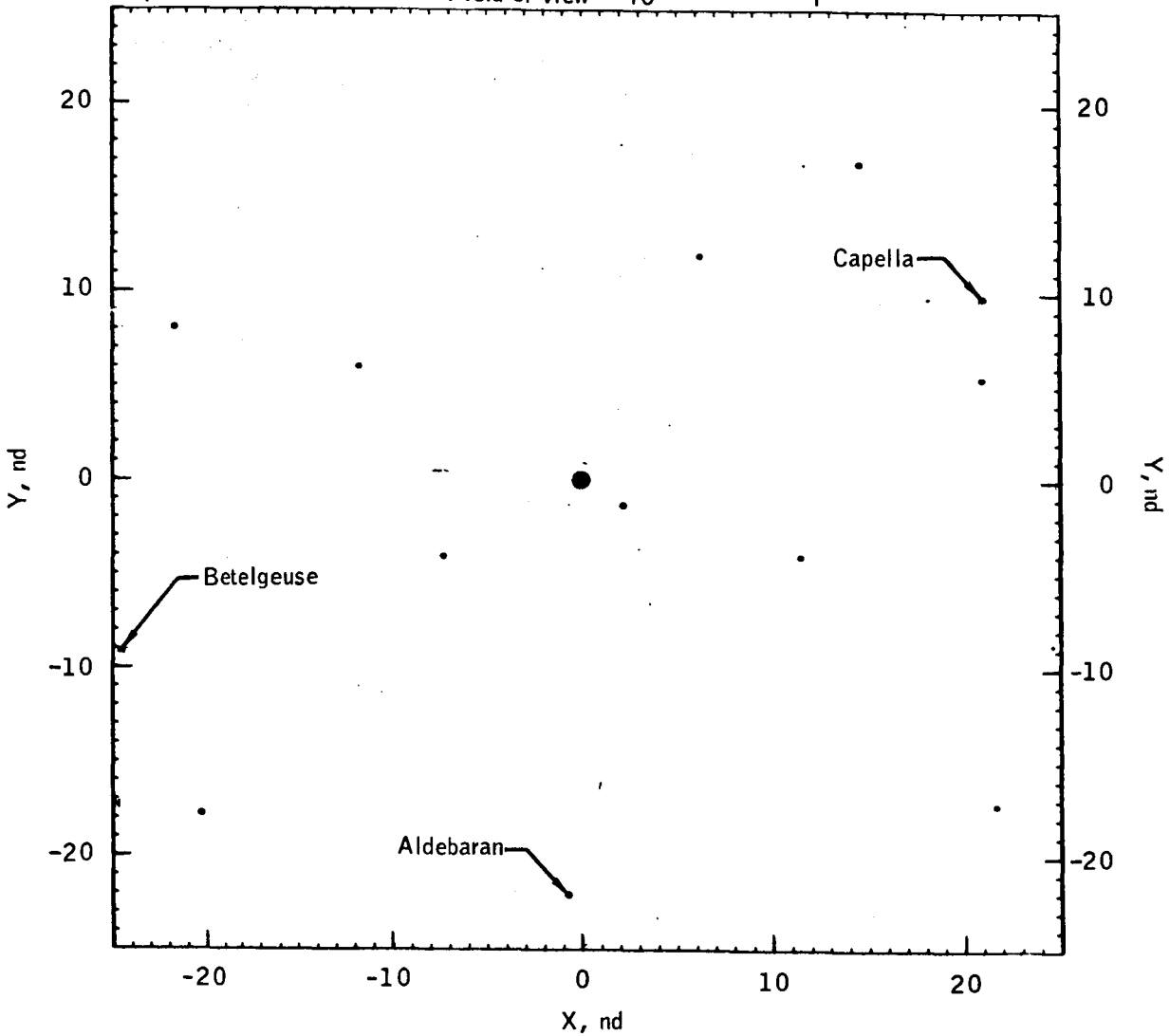
$R_E = 52\,882$  n. mi.

$h_E = 56\,896$  stat. mi.

$V_i = 8541$  fps

$V_i = 5823$  mph

Field of view =  $40^\circ$



(a) G.e.t. = 10 hours.

Figure 9.- Translunar coast-constant field of view (moon).

SEQ	144	150	186	205	207	222	230	231	248	270	271	281	301
X	16	21	0	9	17	17	-20	0	-9	10	2	-14	-24
Y	-20	-11	-18	0	11	15	-17	2	-1	21	15	7	6

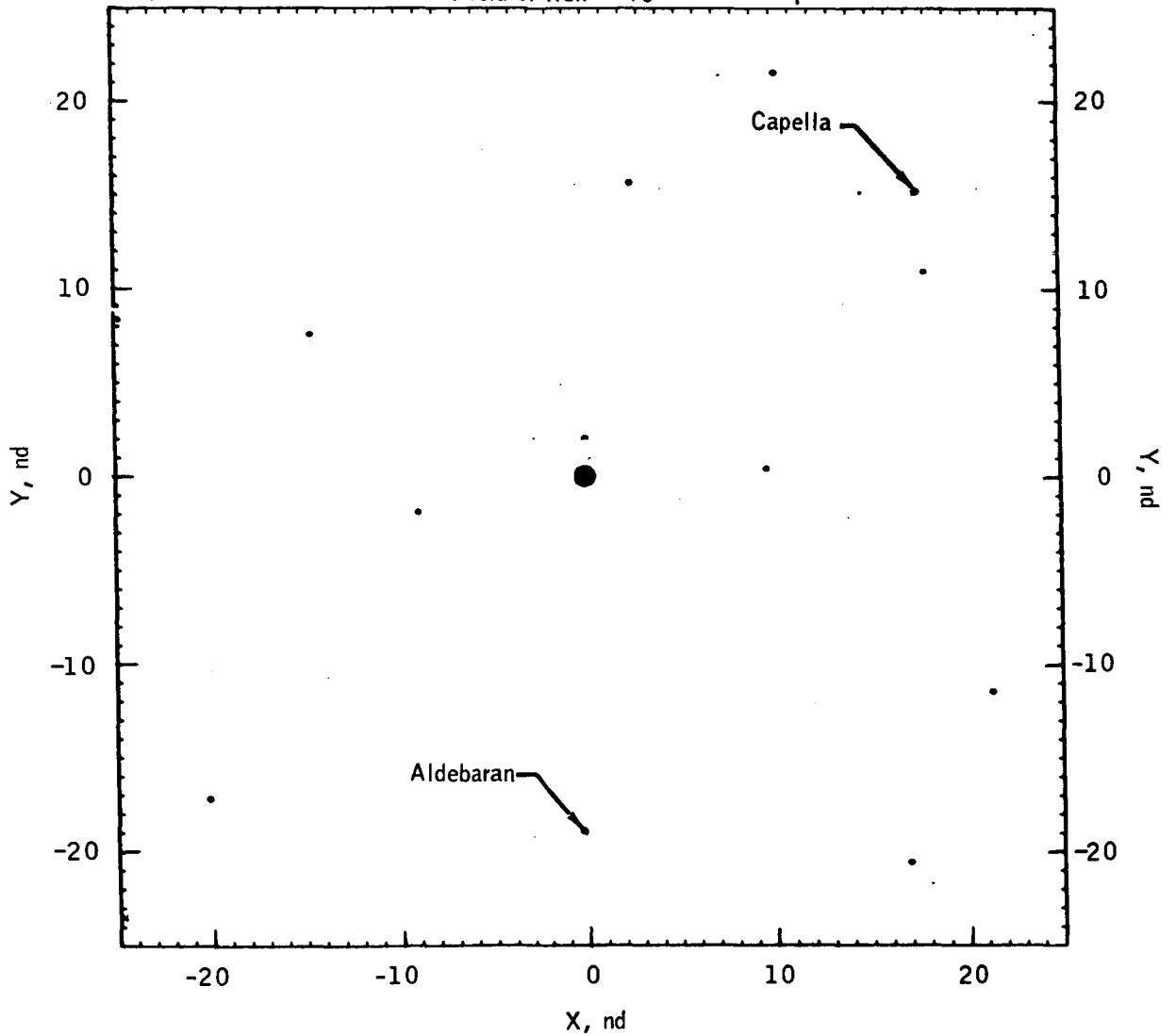
$R_E = 93\,028$  n. mi.

$h_E = 103\,440$  stat. mi.

$V_i = 5930$  fps

Field of view =  $40^\circ$

$V_i = 4043$  mph



(b) G.e.t. = 20 hours.

Figure 9.- Continued.

SEQ	144	150	151	184	205	207	222	230	231	248	270	271	281
X	16	20	24	0	7	15	14	-20	-2	-10	6	0	-17
Y	-16	-7	1	-16	3	14	18	-16	4	0	24	18	8

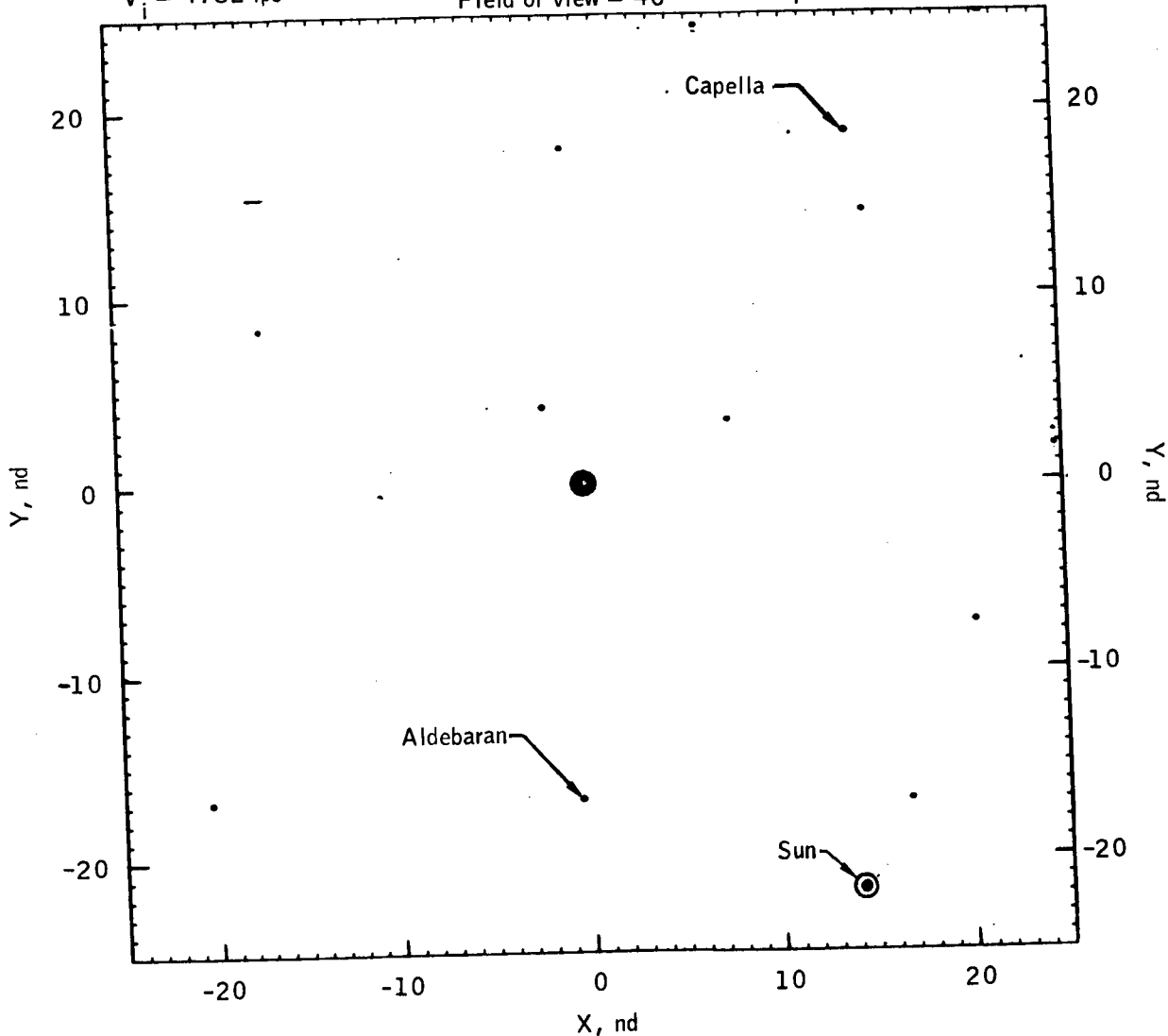
$R_E = 123\,687$  n. mi.

$V_i = 4782$  fps

Field of view =  $40^\circ$

$h_E = 138\,375$  stat. mi.

$V_i = 3260$  mph



(c) G.e.t. = 30 hours.

Figure 9.- Continued.

SEQ	144	150	151	186	205	207	222	230	231	248	270	271	281
X	16	20	24	0	7	15	14	-20	-2	-10	6	0	-17
Y	-16	-7	1	-16	3	14	18	-16	4	0	24	18	8

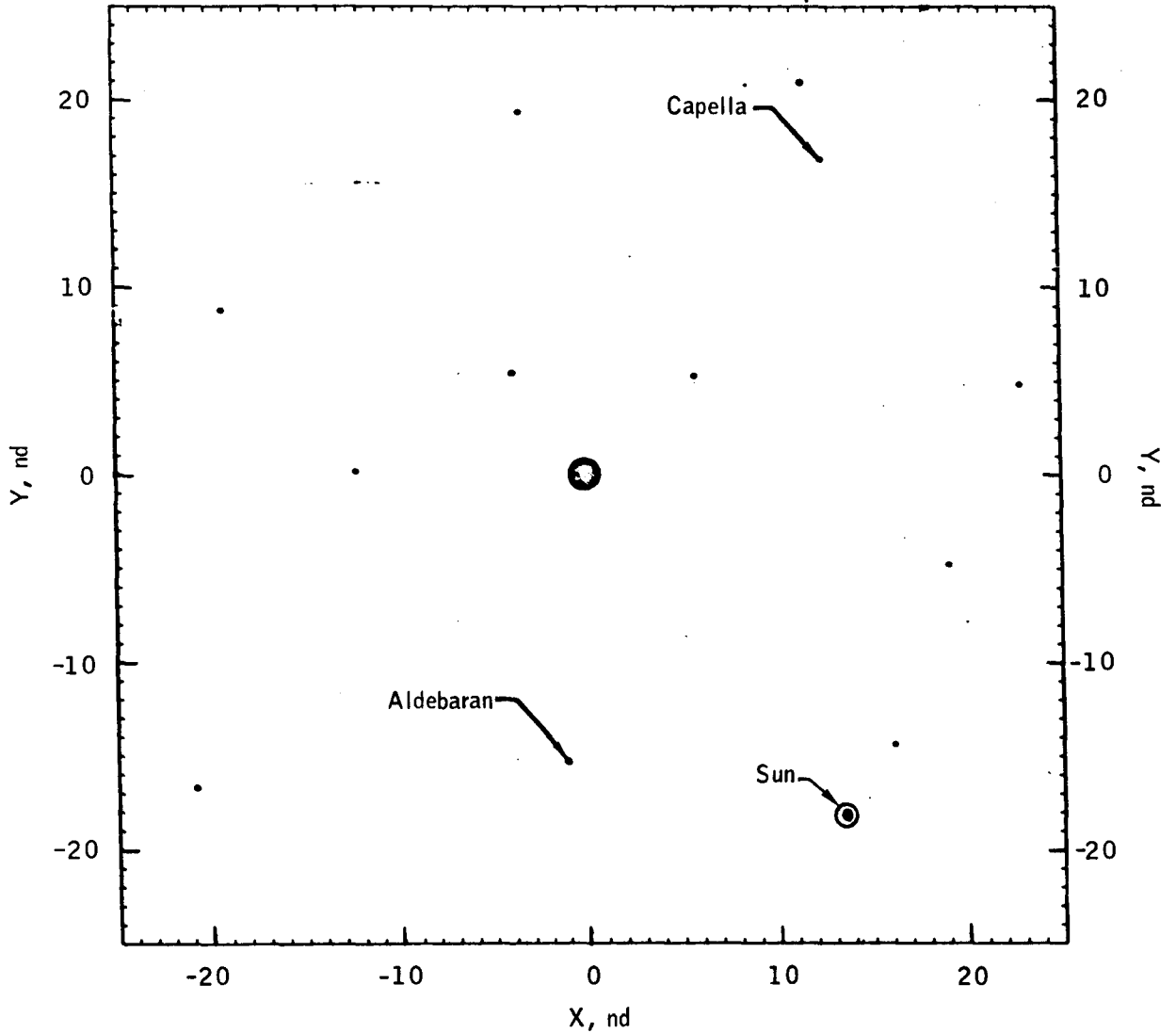
$R_E = 149\,206$  n. mi.

$h_E = 167\,742$  stat. mi.

$V_i = 4067$  fps

Field of view =  $40^\circ$

$V_i = 2773$  mph



(d) G.e.t. = 40 hours.

Figure 9.- Continued.

SEQ	144	150	151	186	205	207	222	230	231	248	271	281
X	15	17	21	-1	4	10	9	-21	-5	-13	-5	-21
Y	-12	-2	6	-13	6	18	22	-16	6	1	20	9

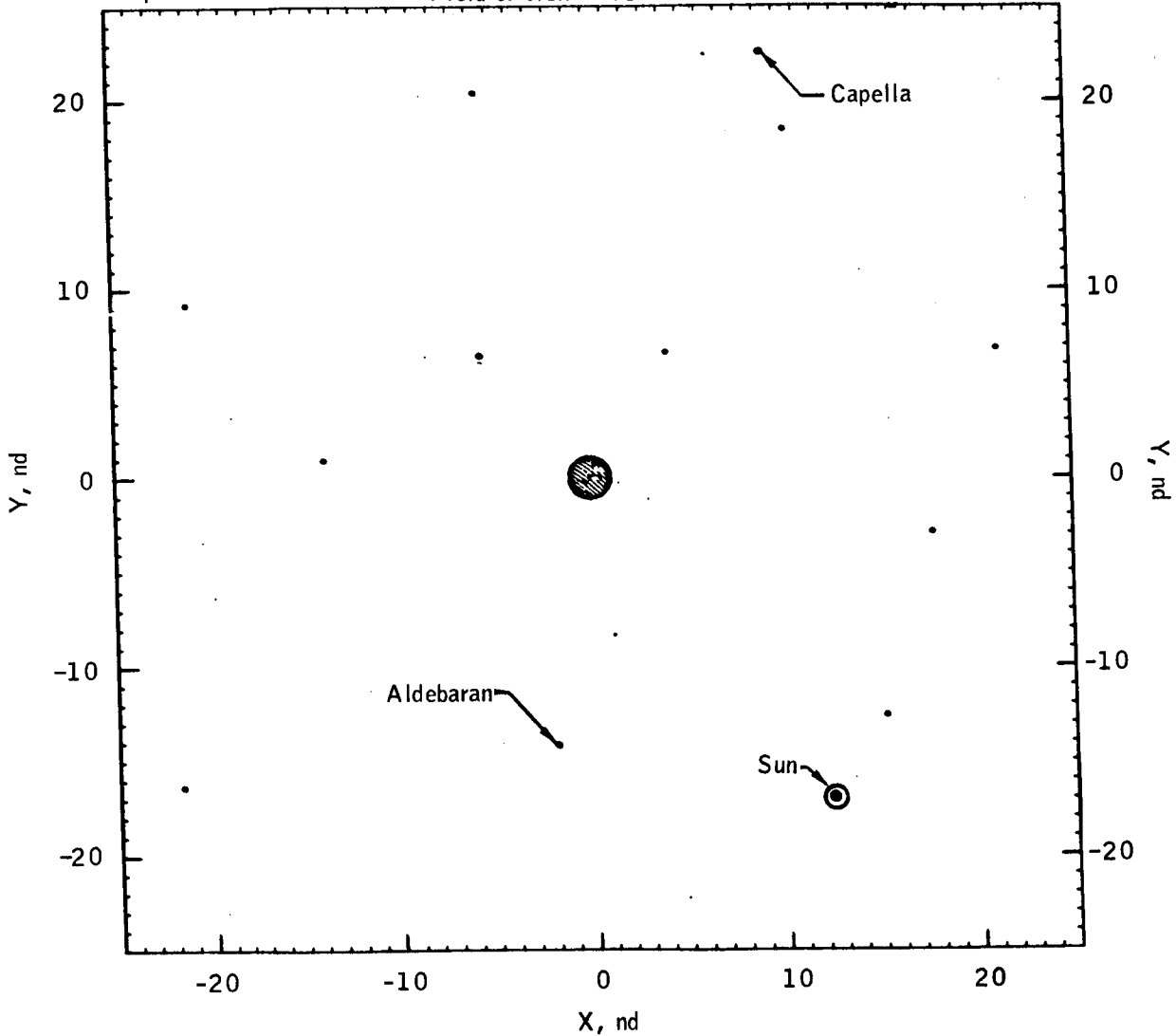
$R_E = 171\,265$  n. mi.

$h_E = 193\,127$  stat. mi.

$V_i = 3557$  fps

$V_i = 2425$  mph

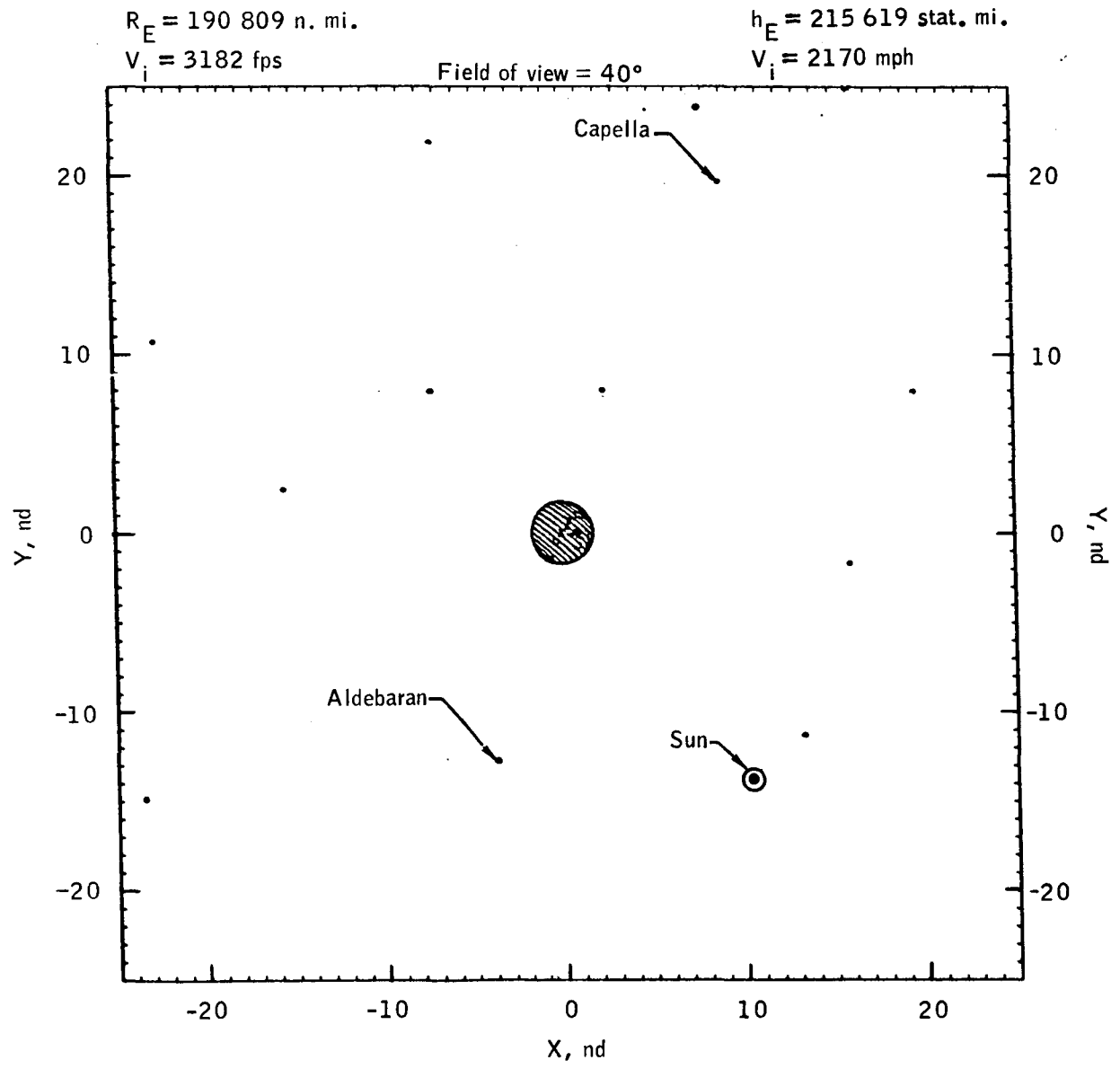
Field of view =  $40^\circ$



(e) G.e.t. = 50 hours.

Figure 9.- Continued.

SEW	144	150	151	186	205	207	222	230	231	248	271	281
X	15	17	21	-1	4	10	9	-21	-5	-13	-5	-21
Y	-12	-2	6	-13	6	18	22	-16	6	1	20	9



(f) G.e.t. = 60 hours.  
 Figure 9.- Continued.

SEC	111	112	144	150	151	186	205	207	222	231	248	270	271
X	18	21	-1	7	17	12	7	21	24	2	-7	23	13
Y	-18	-16	-11	-7	-5	2	8	10	13	16	20	22	24

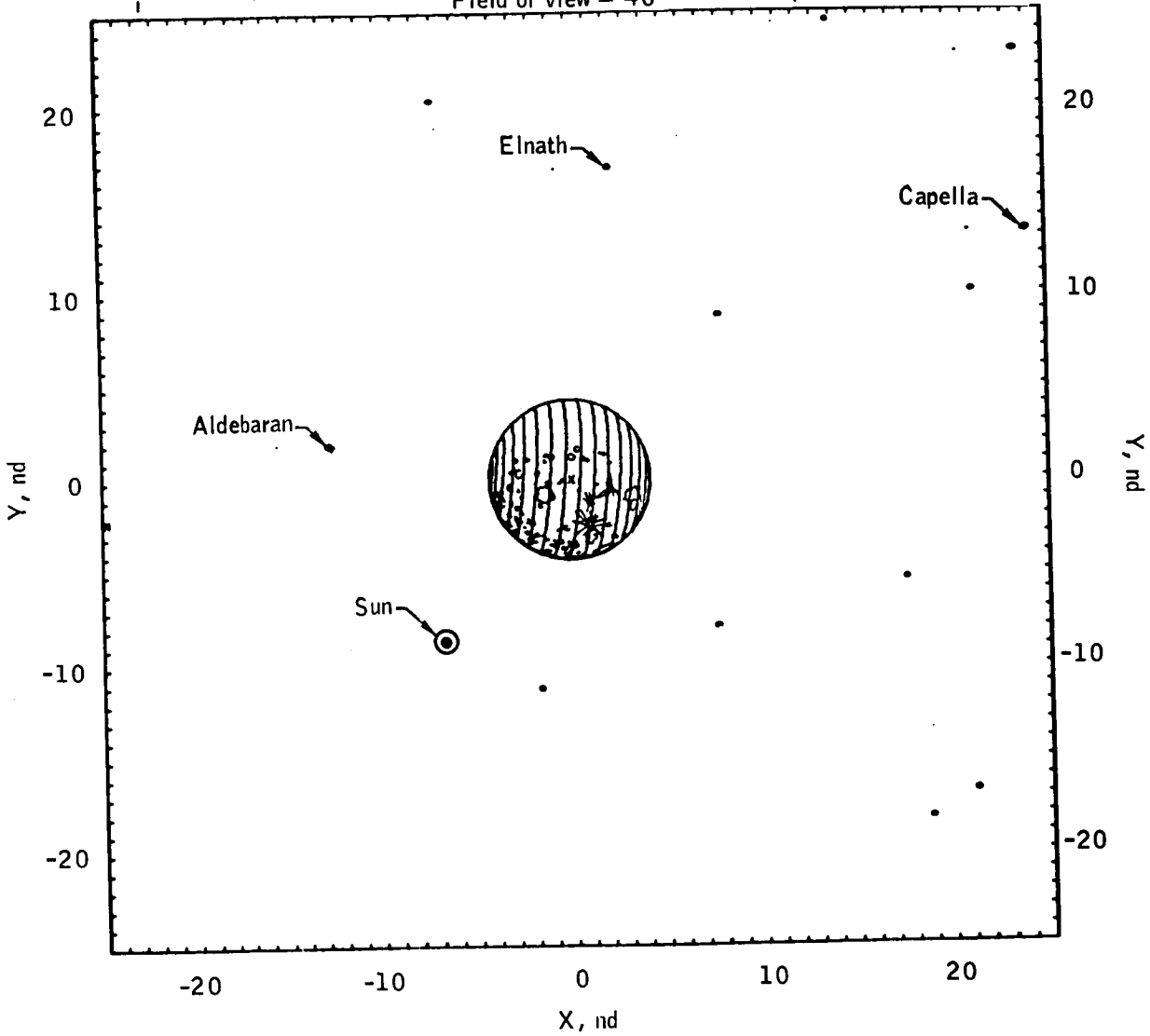
$R_M = 15\,709$  n. mi.

$V_i = 4031$  fps

$h_M = 16\,997$  stat. mi.

$V_i = 2748$  mph

Field of view =  $40^\circ$



(g) G.e.t. = 70 hours.

Figure 9. - Concluded.

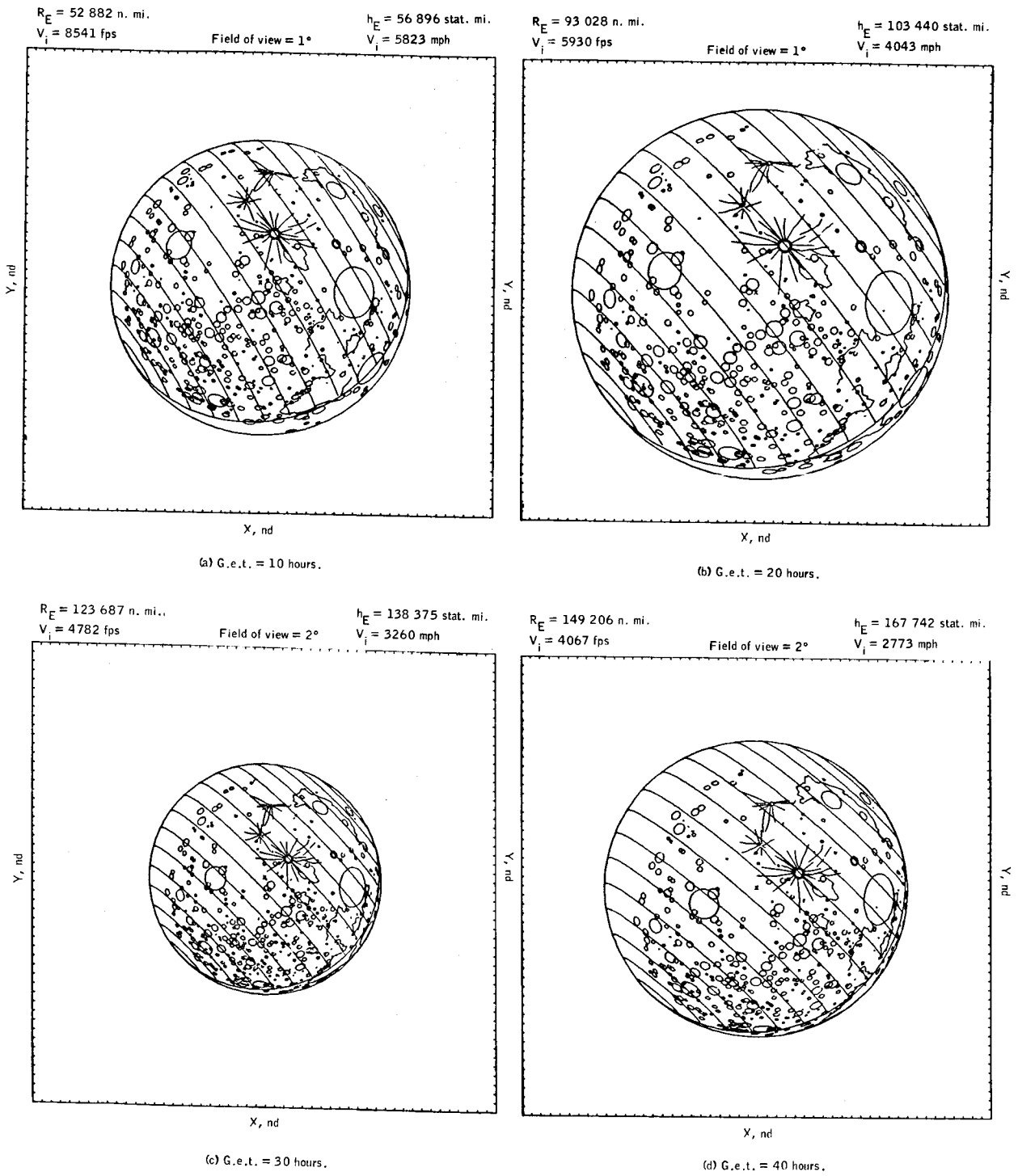
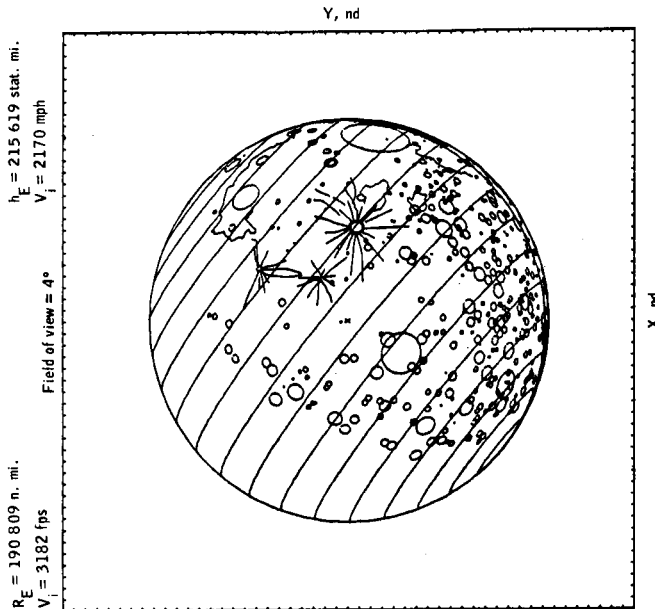
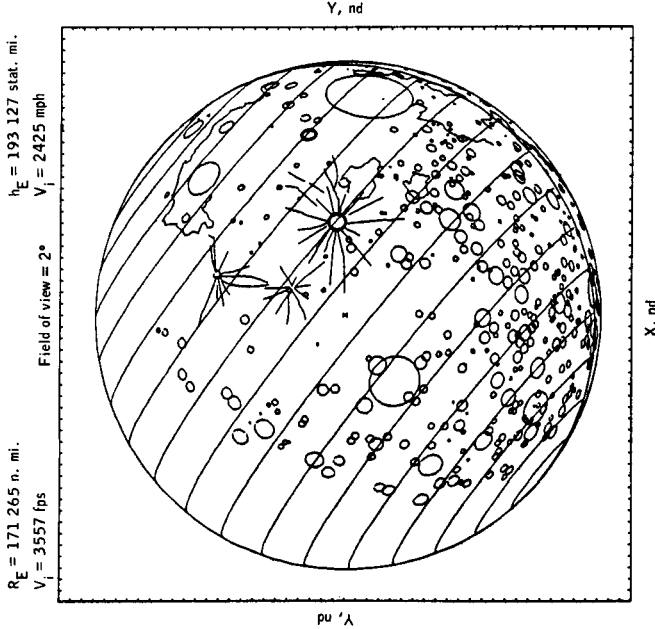


Figure 10.- Translunar coast - variable field of view (moon).





(f) G.e.t. = 60 hours.



(e) G.e.t. = 50 hours.

Figure 10. - Concluded.

LUNAR ORBIT  
INSERTION BURN

SEQ	535	551	569	580	589	599	610	639	641	645	651
X	0	-10	-23	19	-16	-23	11	22	-16	-18	17
Y	-20	-11	0	-14	0	4	-5	-4	7	8	-1

SEQ	660	688	690	736	743	745	751	755	759
X	-16	-14	19	-5	-5	18	-6	24	-9
Y	10	13	4	17	18	11	19	10	20

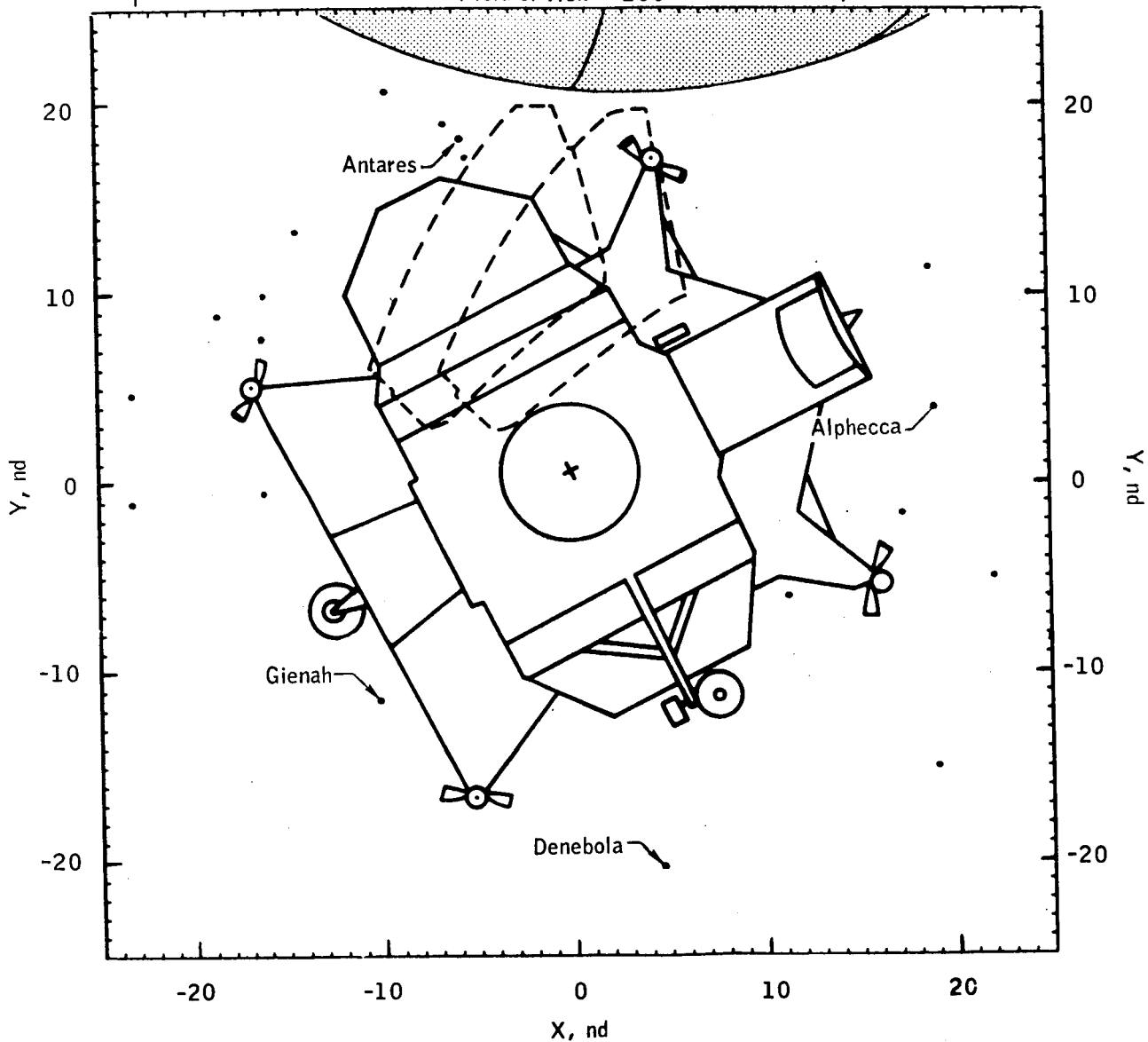
$R_M = 1028$  n. mi.

$V_i = 8251$  fps

$h_M = 102$  stat. mi.

$V_i = 5626$  mph

Field of view = 100°



(a) Begin LOI (g.e.t. = 75:45:43.2).

Figure 11.- Lunar orbit insertion burn.

SEQ	535	540	551	566	570	577	580	589	604
X	1	22	-13	-14	-4	24	15	-18	82
Y	-20	-21	-10	-7	-11	-16	-15	0	-11

SEQ	610	639	645	651	660	695	744	789
X	8	19	-20	14	-18	16	18	21
Y	-6	-5	10	-2	11	3	18	8

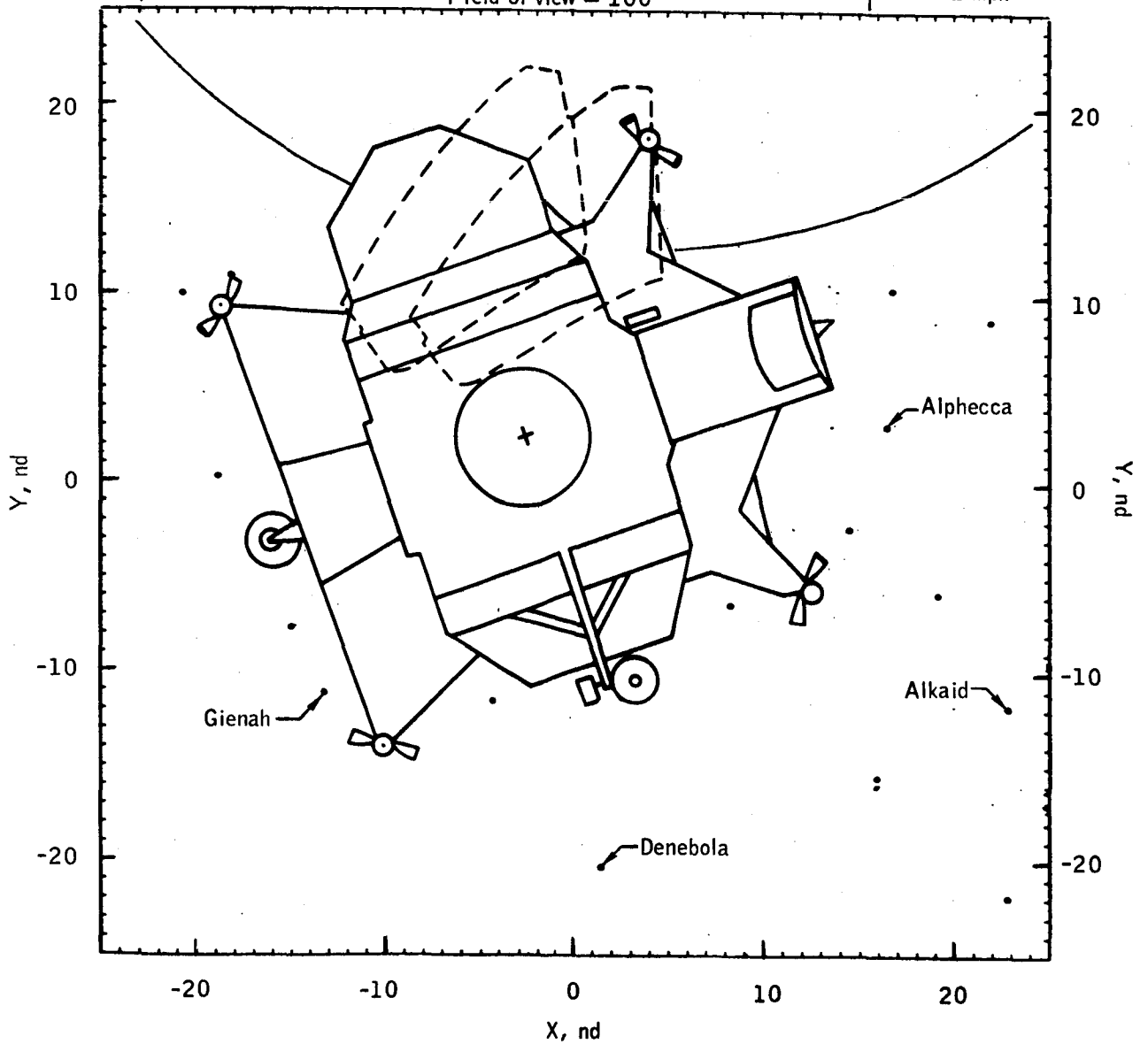
$R_M = 1001$  n. mi.

$V_i = 7013$  fps

$h_M = 71$  stat. mi.

$V_i = 4782$  mph

Field of view = 100°



(b) Middle of LOI (g.e.t. = 75:48:43.2).

SEQ	535	540	551	566	577	580	582	589	592	595	604	621	639	690
X	-2	18	-17	-19	20	11	-1	-22	20	-16	18	-20	14	120
Y	-20	-22	-10	-6	-17	-15	-11	1	-15	0	-12	9	-6	2

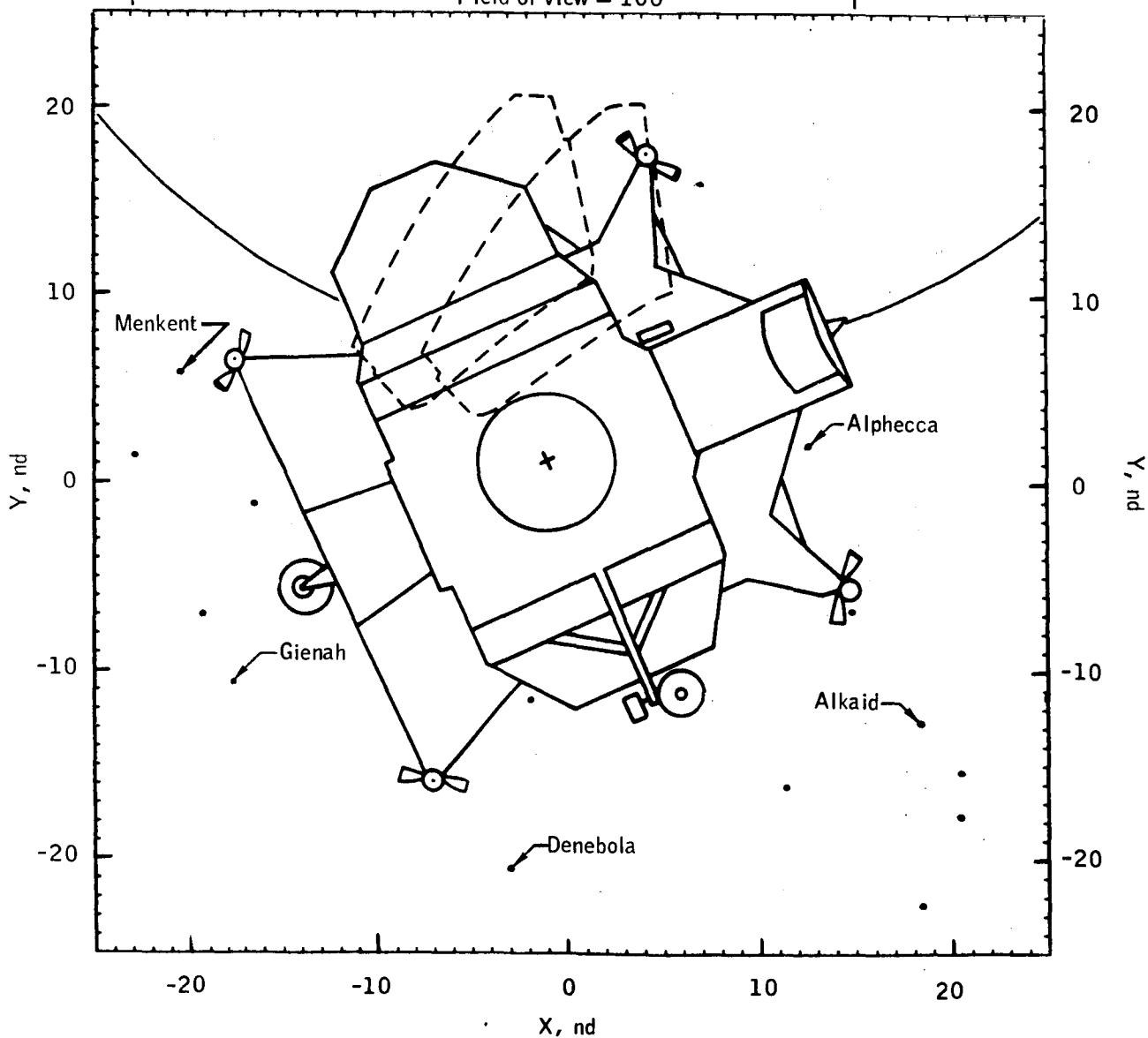
$R_M = 997$  n. mi.

$V_i = 5485$  fps

$h_M = 67$  stat. mi.

$V_i = 3740$  mph

Field of view =  $100^\circ$



(c) End of LOI (g.e.t. = 75:51:44.7).

Figure 11.- Concluded.

LUNAR ORBIT PHASE

SEQ	271	281	301	342	349	356	362	376	377	381	427	440	473	480
X	24	17	12	-14	17	3	14	-20	-12	-24	-23	-7	1	5
Y	-19	-24	-23	-24	-13	-19	-13	-19	-19	-19	-13	28	0	1
SEQ	507	509	515	535	540	551	566	570	577	580	582	592	593	595
X	22	24	3	0	20	-16	-20	-9	21	11	-2	21	-15	-21
Y	9	9	8	11	13	11	12	16	18	19	20	20	20	18
SEQ	604	1081												
X	18	-5												
Y	23	10												

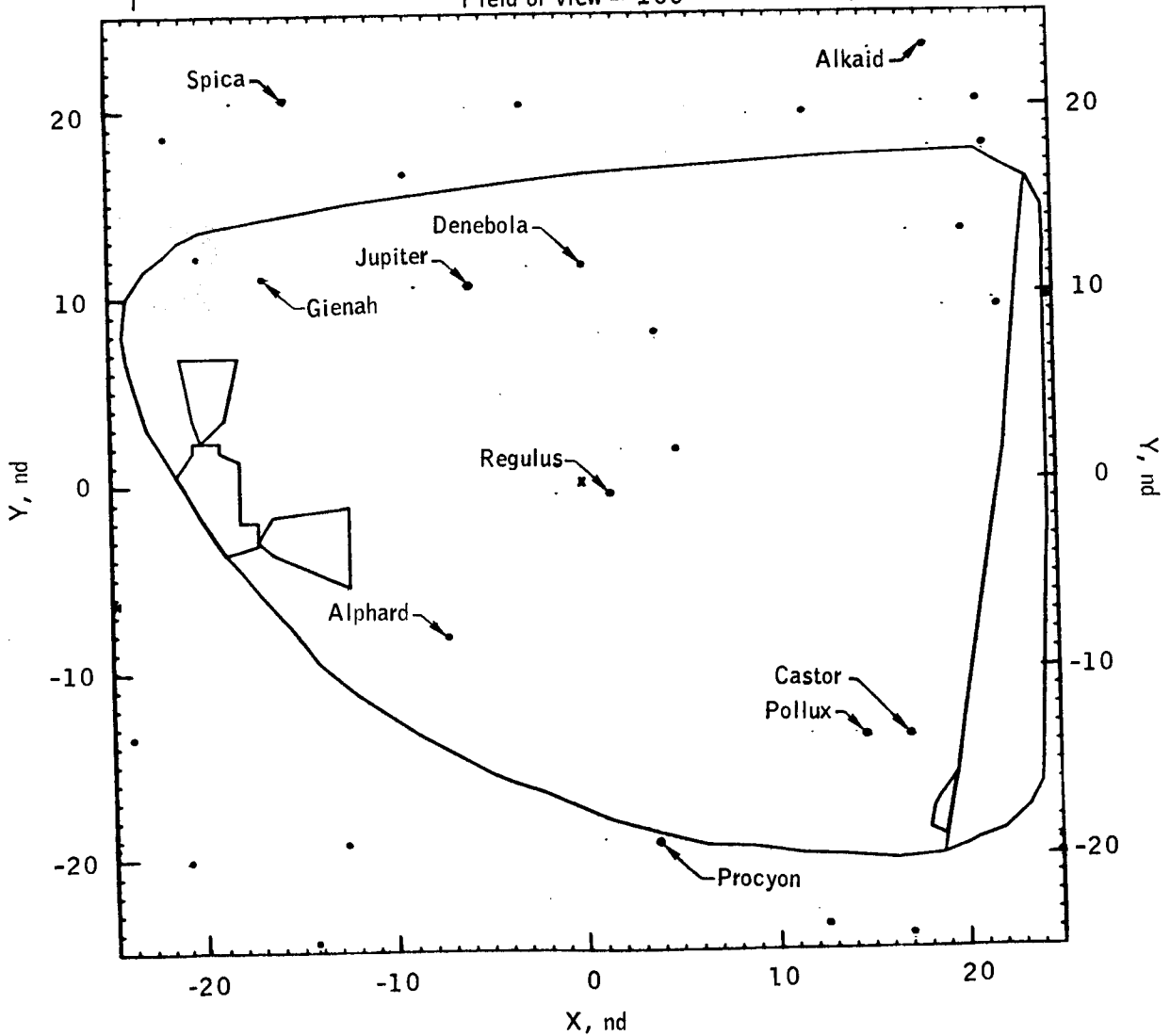
$R_M = 996$  n. mi.

$V_i = 5349$  fps

$h_M = 67$  stat. mi.

$V_i = 3647$  mph

Field of view = 100°



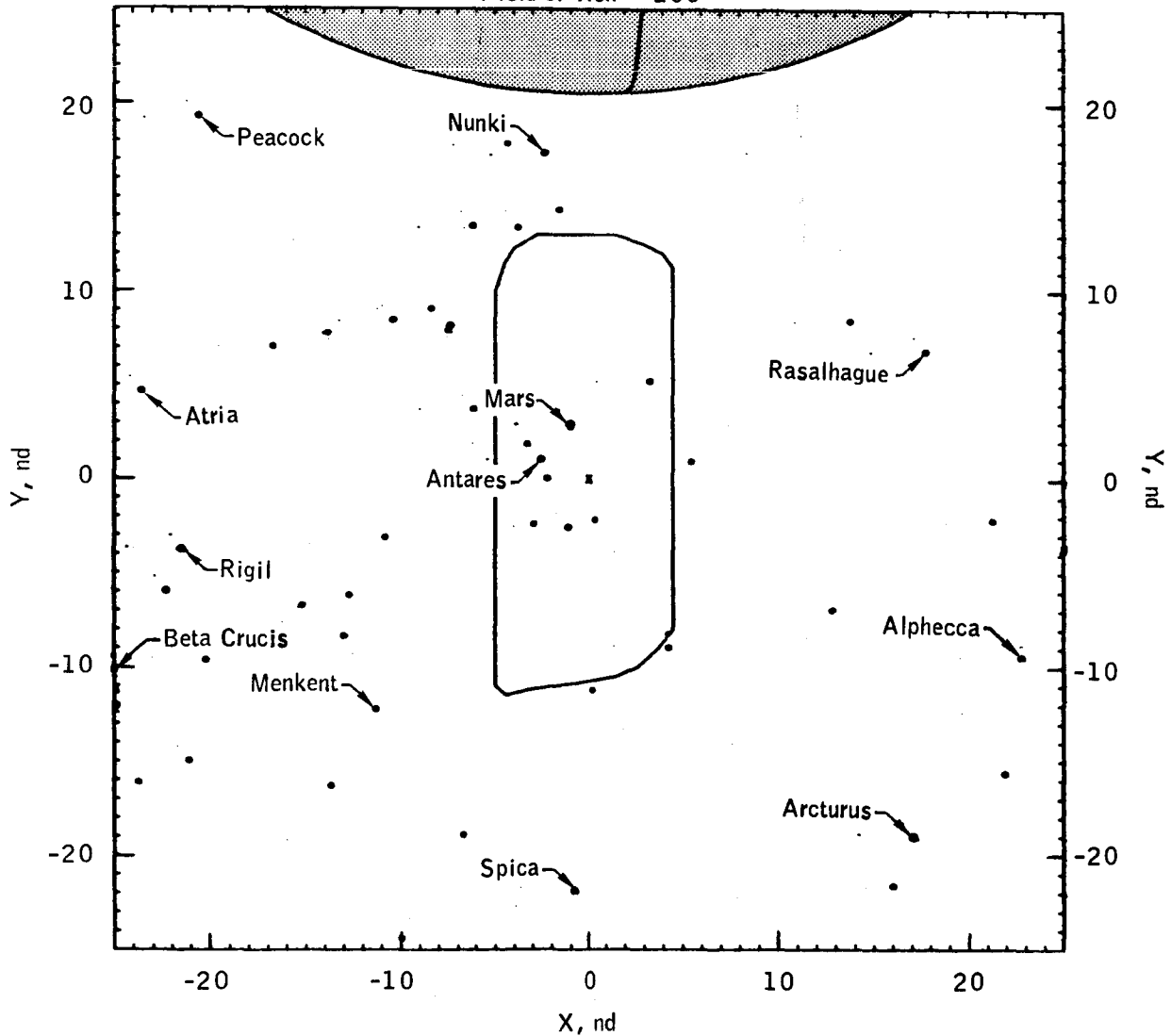
(a) Begin DOI burn - front window (g.e.t. = 99:33:51).

Figure 12.- Lunar orbit phase.

SEQ	545	561	566	569	574	589	593	595	599	610	617	621	624	641
X	-23	-24	-9	-21	-24	-13	0	-6	-20	16	-22	-11	17	-12
Y	-15	-11	-24	-14	-10	-16	-21	-18	-9	-21	-5	-12	-18	-8
SEQ	643	645	651	655	660	673	688	690	700	717	719	724	736	743
X	-21	-15	21	0	-12	4	-10	22	12	-2	-1	0	-2	-2
Y	-3	-6	-15	-11	-6	-8	-2	-9	-6	-2	-2	-2	0	1
SEQ	745	751	753	757	759	770	781	789	790	793	795	797	802	803
X	21	-3	5	-23	-6	3	-16	-7	-13	-7	17	-10	-8	13
Y	-2	2	1	4	3	5	7	8	7	8	6	8	9	8
SEQ	836	841	844	861	871	933	1000							
X	-3	-6	-1	-2	-4	-20	-1							
Y	13	13	14	17	17	19	3							

 $R_M = 996 \text{ n. mi.}$ 
 $V_i = 5349 \text{ fps}$ 
 $h_M = 67 \text{ stat. mi.}$ 
 $V_i = 3647 \text{ mph}$ 

Field of view = 100°



(b) Begin DOI burn - docking window (g.e.t. = 99:33:51).



SEQ	271	281	301	342	346	356	362	376	377	381	427	440	473	480	507
X	24	17	12	14	17	13	14	-20	-12	-24	-23	-7	1	5	22
Y	-1	-24	-23	-24	-13	-19	-13	-19	-19	-19	-13	-8	0	1	9
SEQ	509	515	535	540	551	566	570	577	580	582	592	593	595	604	1081
X	24	3	0	20	-16	-20	-9	21	11	-2	21	-15	-21	18	5
Y	9	4	11	13	11	12	16	18	19	20	20	20	18	23	10

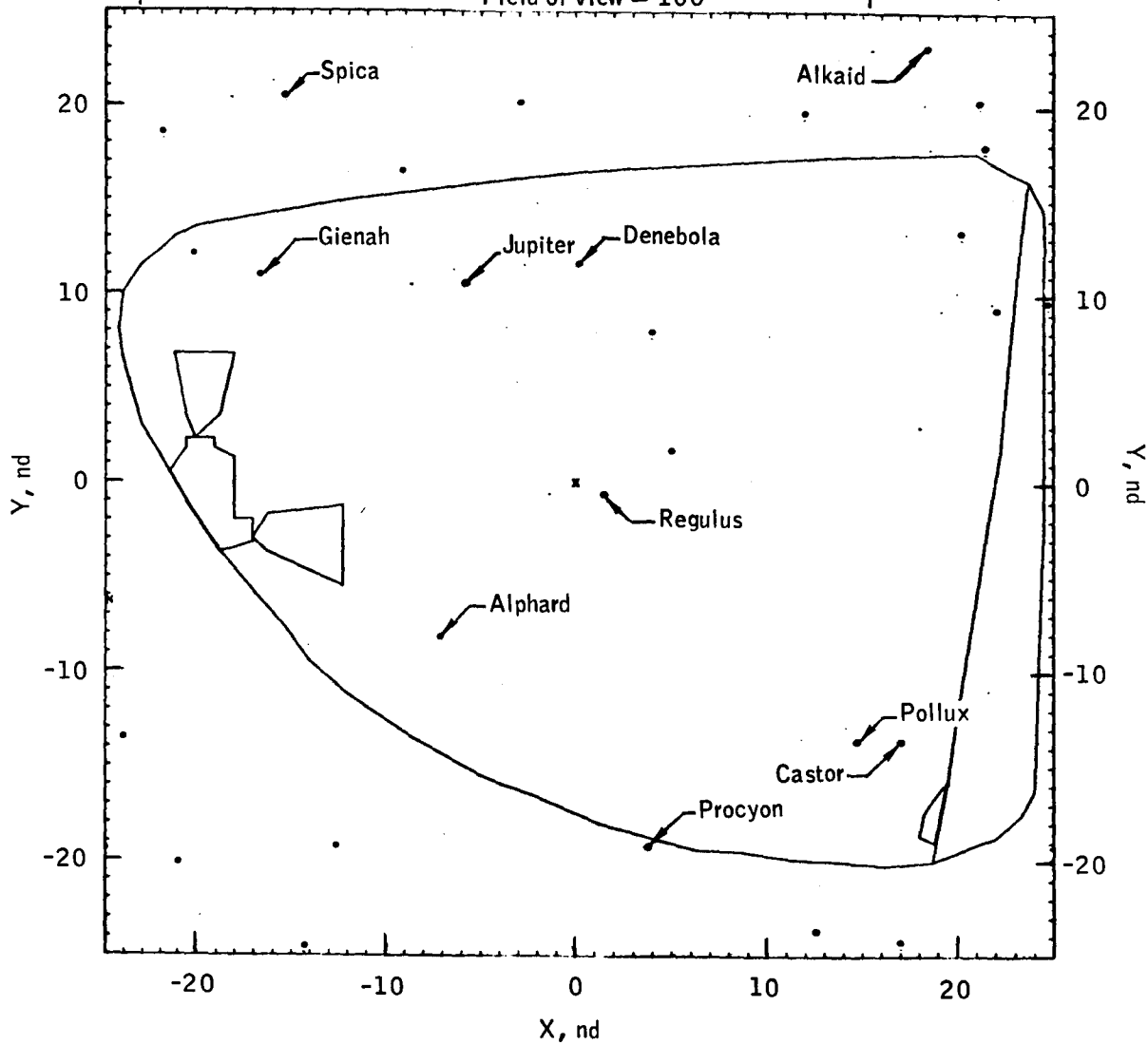
$R_M = 996$  n. mi.

$h_M = 67$  stat. mi.

$V_i = 5278$  fps

$V_i = 3599$  mph

Field of view =  $100^\circ$



(c) End DOI burn - Front window (g.e.t. = 99:34:26).

Figure 12.- Continued.

SEQ	545	561	566	569	574	589	593	595	599	610	617	621	624	641	643
X	-25	-24	-9	-21	-24	-13	0	-6	-20	16	-22	-11	17	-12	-21
Y	-15	-11	-24	-14	-10	-16	-21	-18	-9	-21	-9	-12	-18	-8	-3
SEQ	645	651	655	660	673	688	690	700	717	719	724	736	743	745	751
X	-15	21	0	-12	4	-10	22	12	-2	-1	0	-2	2	21	-3
Y	-6	-15	-11	-6	-8	-2	-9	-6	-2	-2	-2	0	1	2	2
SEQ	753	757	759	770	781	789	790	793	795	797	802	803	836	841	844
X	5	-23	-6	3	-16	-7	-13	-7	17	-10	-8	13	-3	-6	-1
Y	1	4	3	5	7	8	7	4	6	8	9	8	13	13	14
SEQ	861	871	1080												
X	-2	-4	-1												
Y	17	17	3												

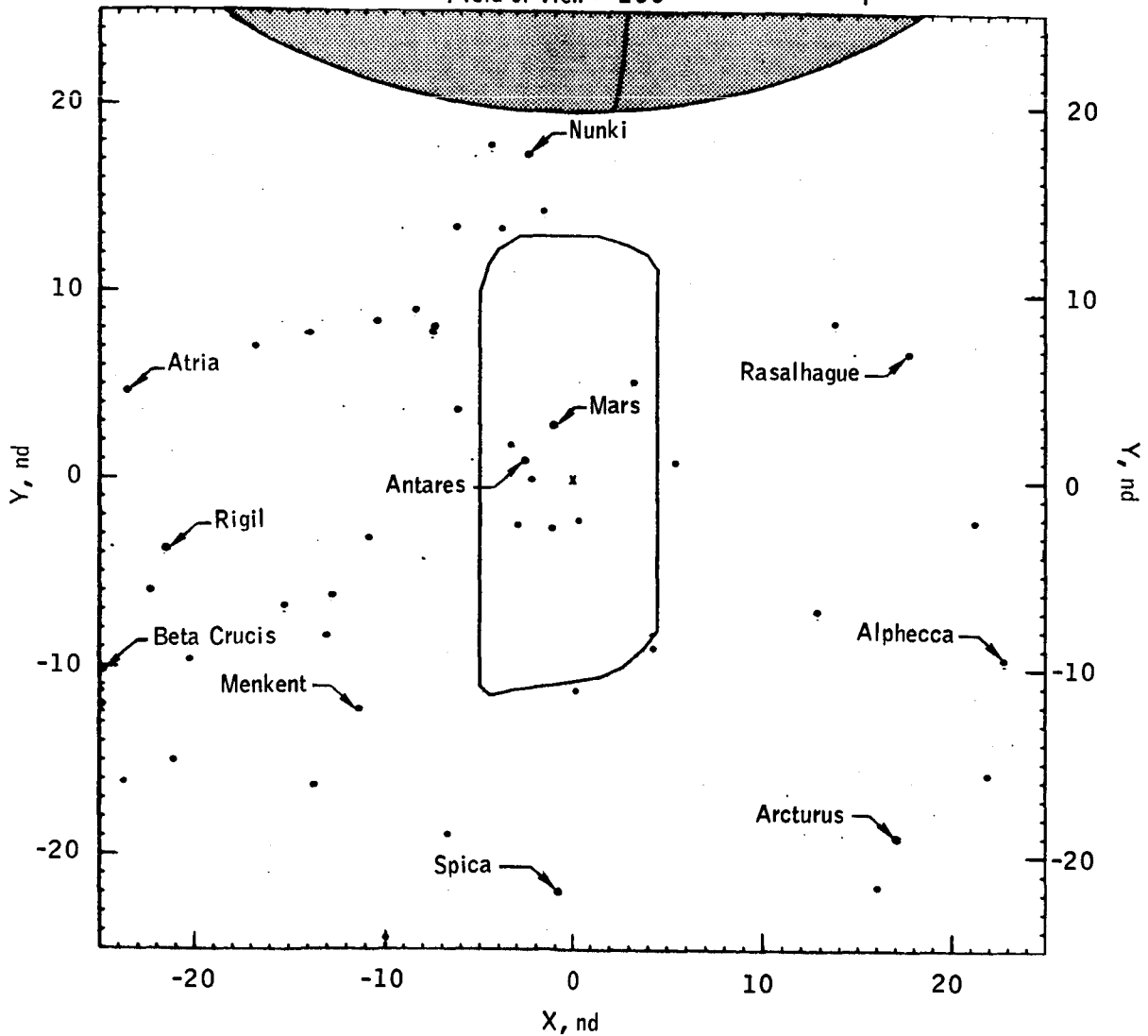
$R_M = 996$  n. mi.

$V_i = 5278$  fps

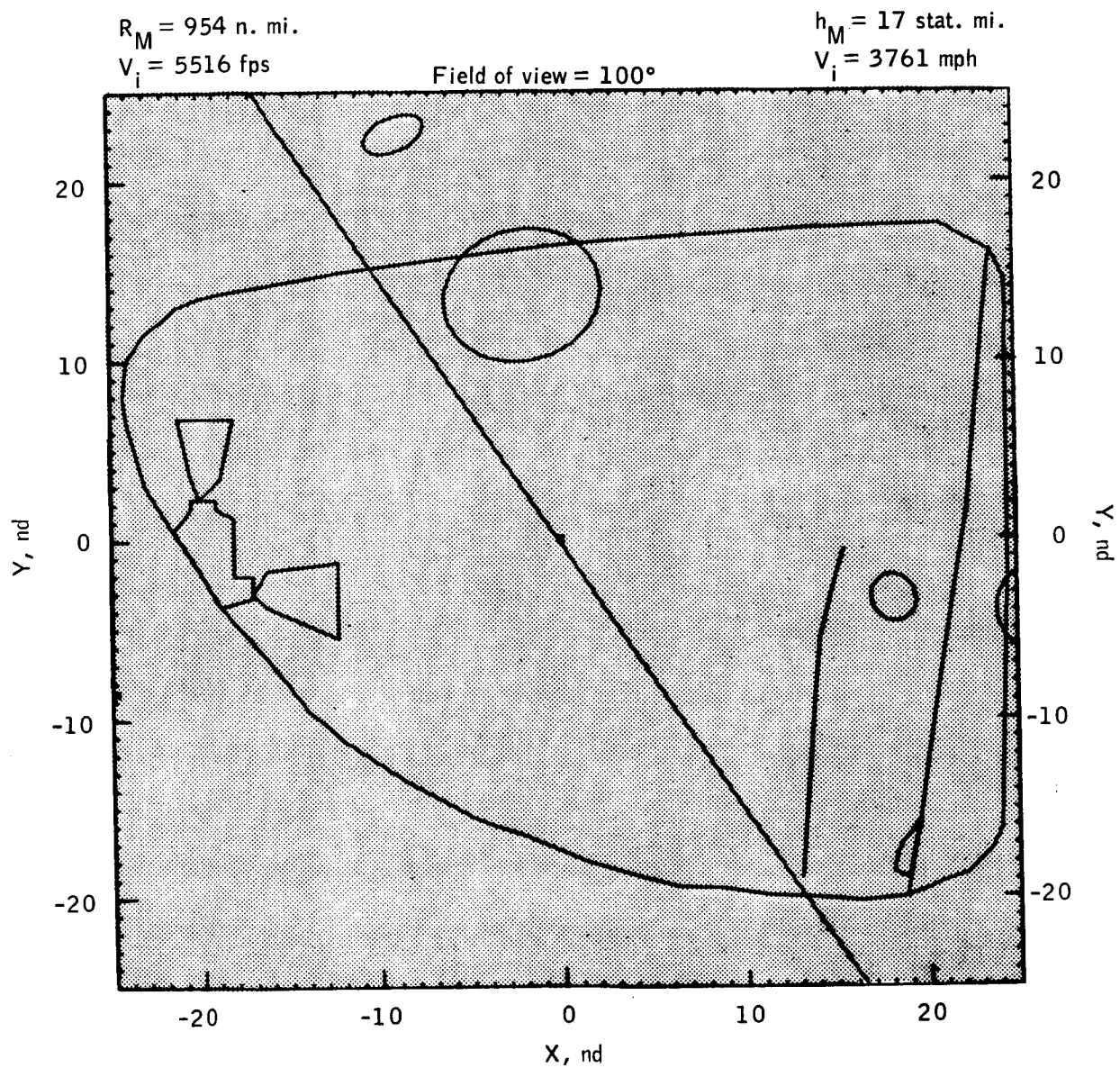
$h_M = 67$  stat. mi.

$V_i = 3599$  mph

Field of view =  $100^\circ$



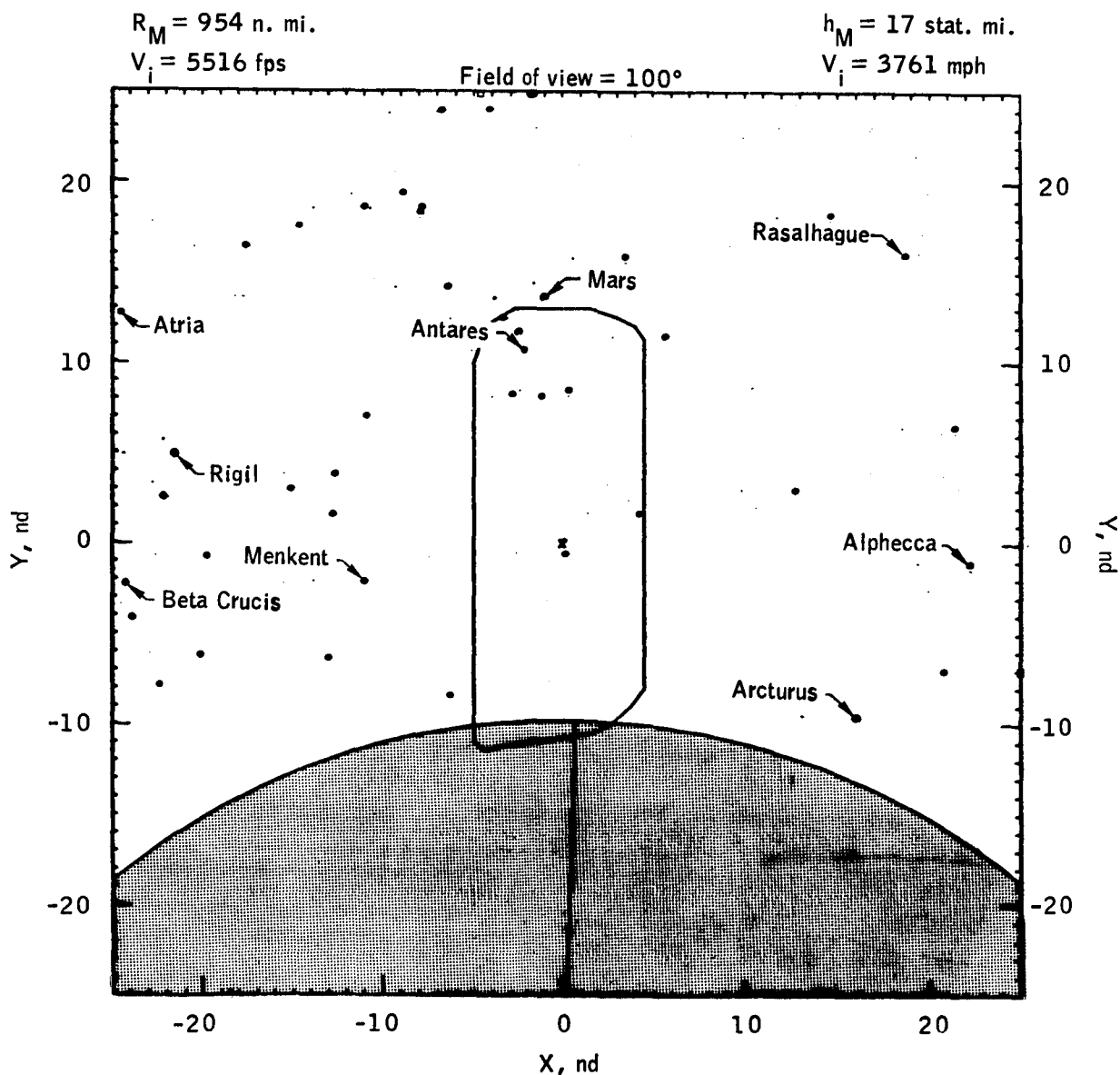
(d) End DOI burn - docking window (g.e.t. = 99:34:26).



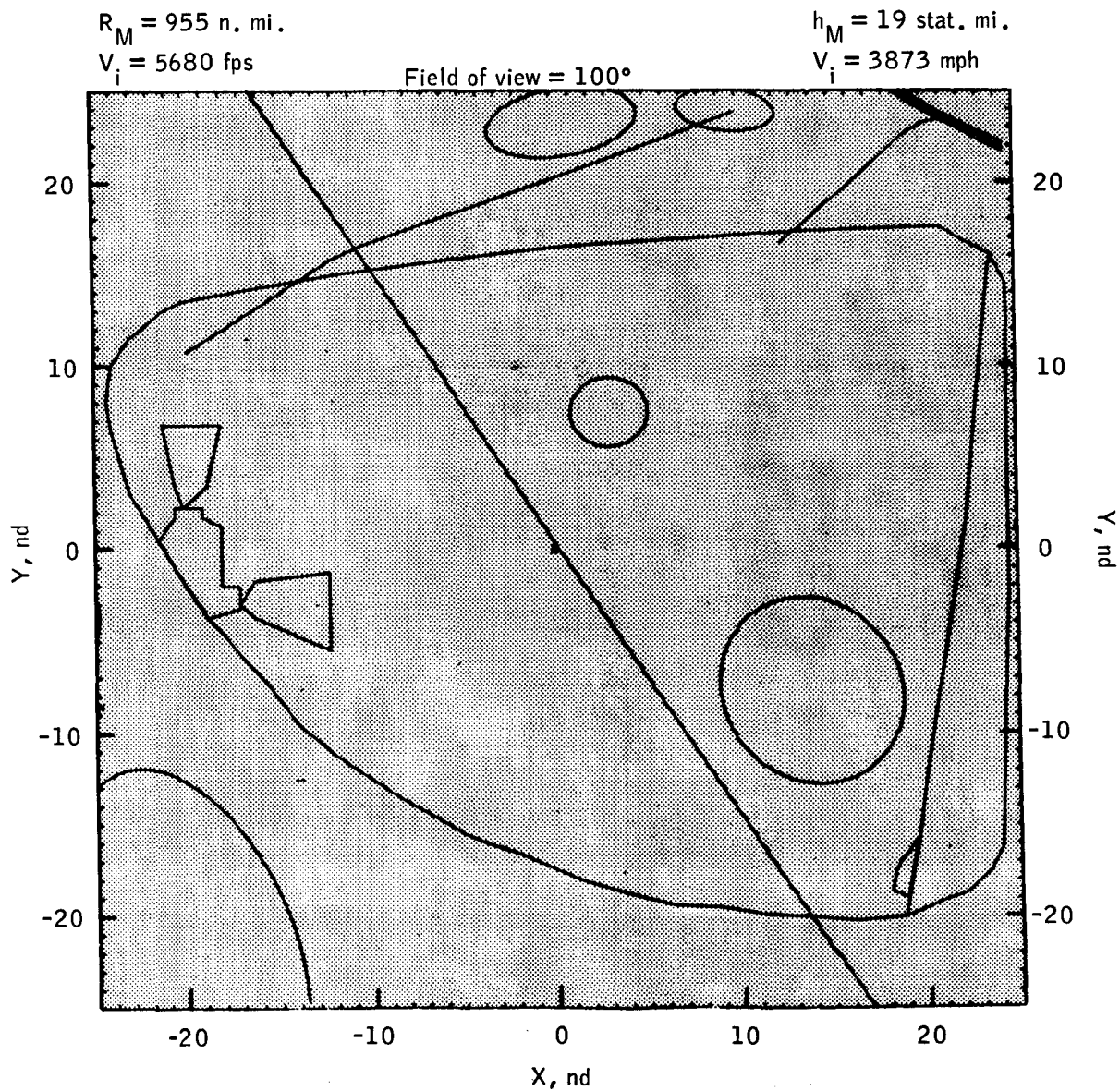
(e) Begin phasing burn - front window (g.e.t. = 100:64:21).

Figure 12.- Continued.

SEQ	545	561	569	574	589	595	599	617	621	624	641	643	645	651
X	-22	-23	-20	-24	-12	-6	-19	-22	-10	15	-12	-21	-15	20
Y	-7	-3	-6	-2	-6	-8	0	2	-1	-9	1	8	3	-6
SEQ	658	660	673	688	690	700	717	719	724	736	743	748	751	753
X	0	-12	4	-10	22	12	-2	-1	0	-2	-2	21	-3	5
Y	0	3	1	7	0	3	8	8	8	10	11	6	12	11
SEQ	757	759	770	781	789	790	793	795	797	802	803	836	841	844
X	-24	-6	3	-17	-7	-14	-7	18	-10	-8	14	-4	-6	-1
Y	12	14	16	16	18	17	18	16	18	19	18	24	24	25
SEQ	1080													
X	-1													
Y	13													



(f) Begin phasing burn - docking window (g.e.t. = 100:46:21).



(g) End phasing burn - front window (g.e.t. = 100:47:03).

Figure 12.- Continued.

SEQ	545	561	569	574	589	595	599	617	621	624	641	643	645
X	-22	-23	-20	-24	-12	-6	-19	-22	-10	15	-12	-21	-15
Y	27	-3	26	-2	26	-8	0	2	-1	-9	1	5	3
SEQ	651	655	660	673	688	690	700	717	719	724	736	743	745
X	20	0	-12	4	-10	22	12	-2	-1	0	-2	-2	21
Y	-6	0	3	1	7	0	3	8	8	8	11	11	6
SEQ	751	753	757	759	770	781	786	790	793	795	797	802	803
X	-3	5	-24	-6	3	-17	-7	-14	-7	18	-10	-8	14
Y	12	11	12	14	16	16	18	17	18	18	18	19	18
SEQ	836	841	844	1080									
X	-4	-6	-1	-1									
Y	24	24	25	13									

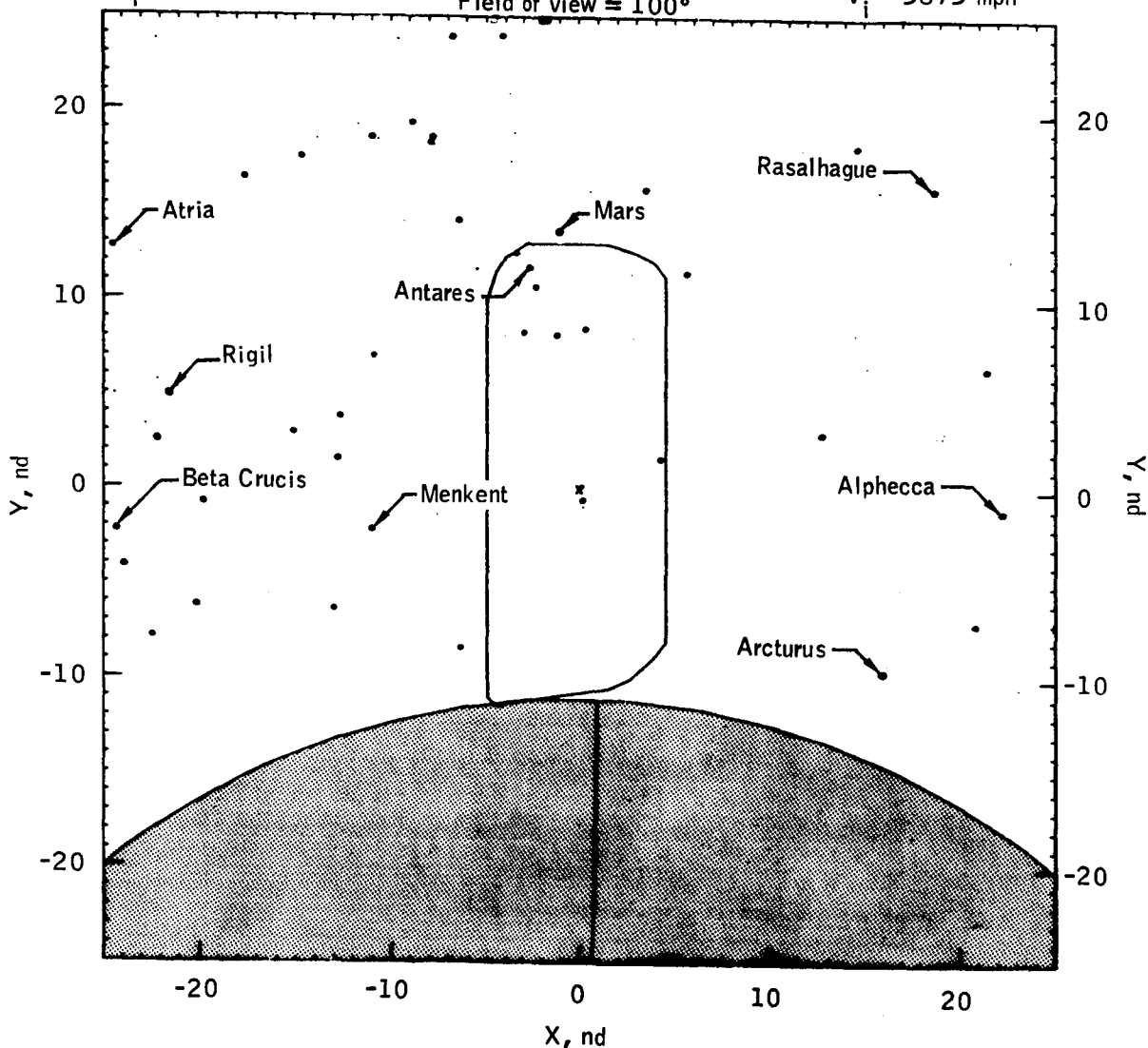
$R_M = 955$  n. mi.

$V_i = 5680$  fps

$h_M = 19$  stat. mi.

$V_i = 3873$  mph

Field of view = 100°



(h) End phasing burn - docking window (g.e.t. = 100:47:03).

SEG 349 362  
 X 21 19  
 Y -18 -19

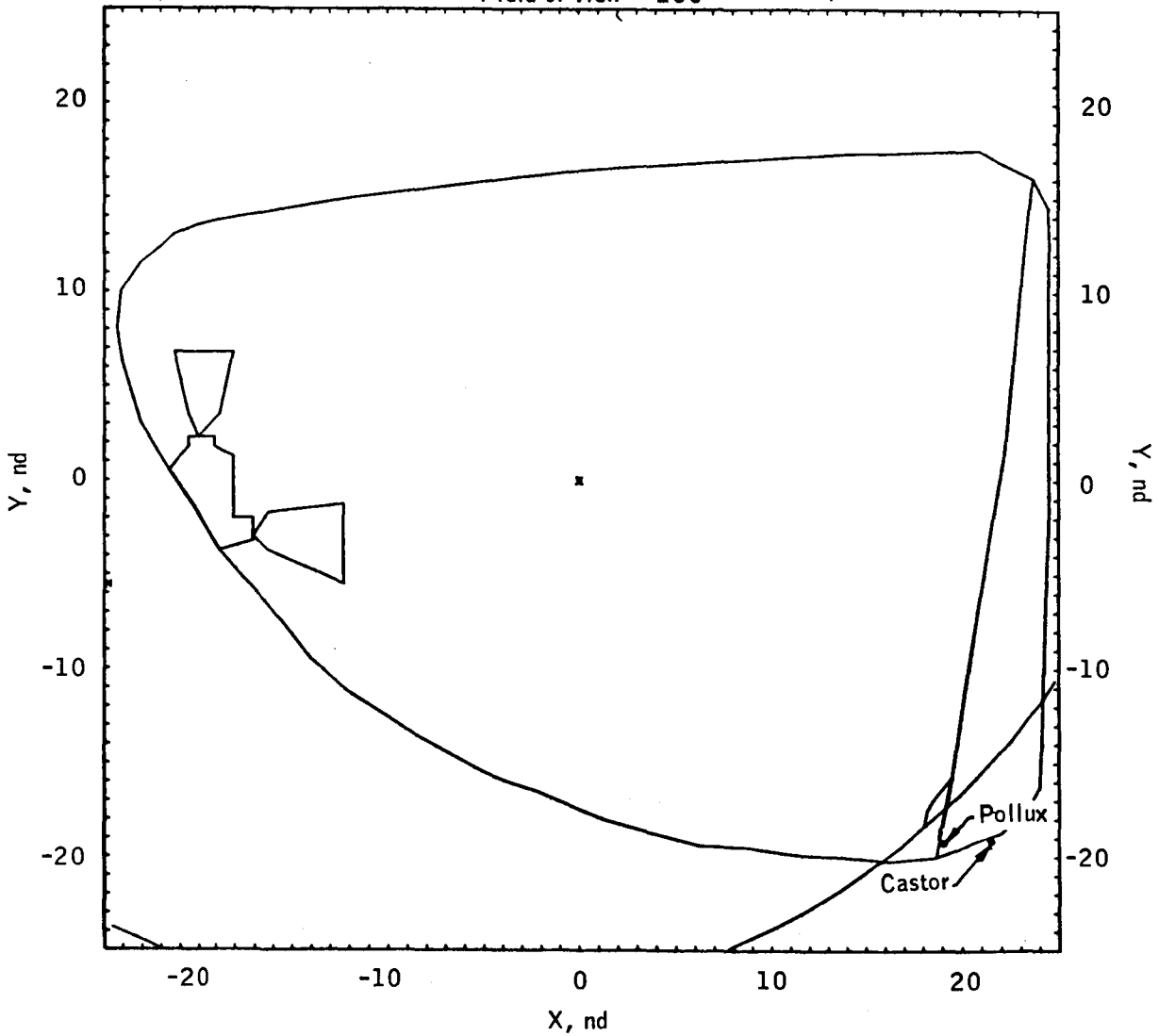
$R_M = 964$  n. mi.

$V_i = 5631$  fps

$h_M = 29$  stat. mi.

$V_i = 3839$  mph

Field of view =  $100^\circ$



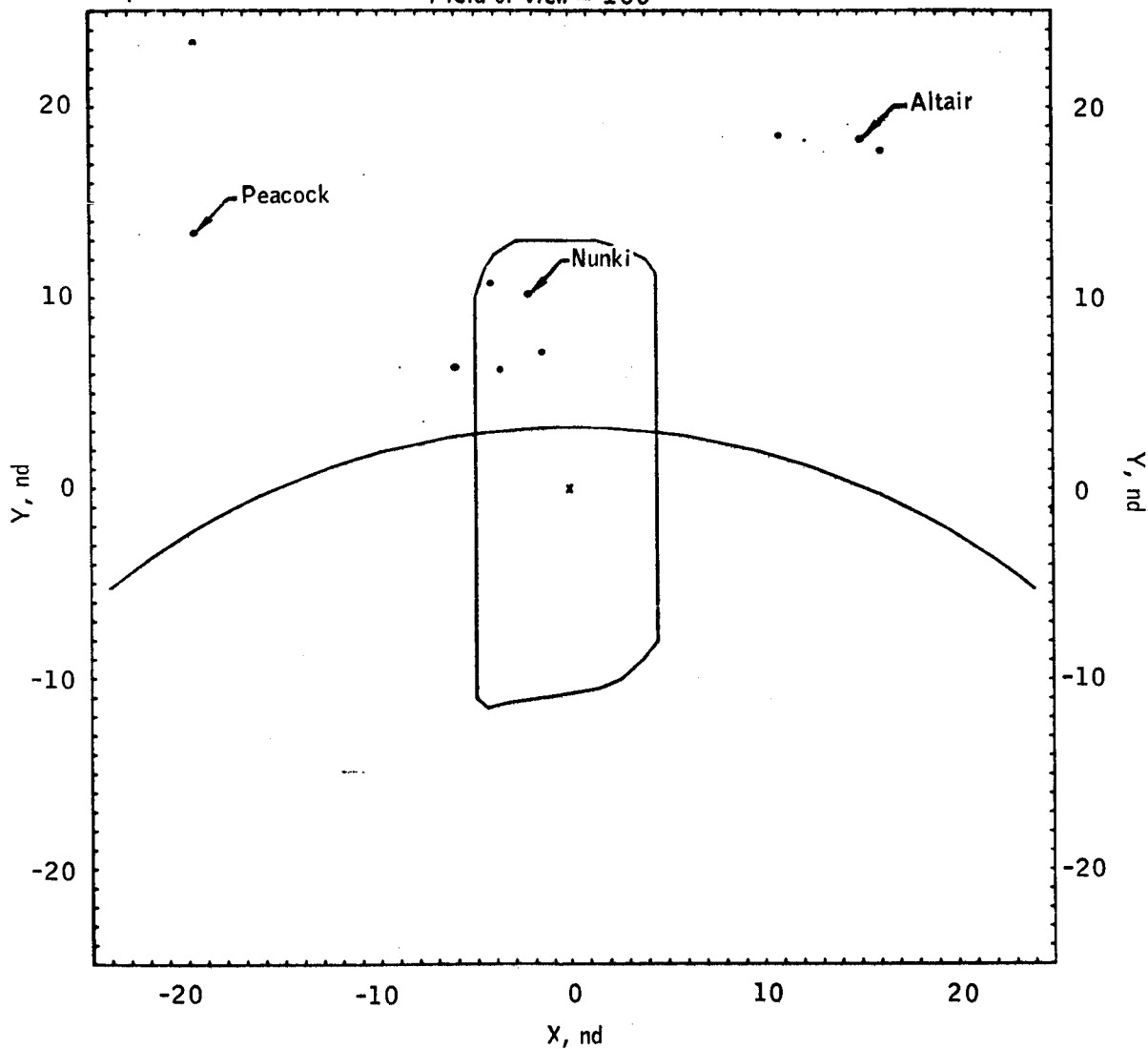
(i) Descent stage jettison (end burn)- front window (g.e.t.= 102:33:28).

SEC	834	841	844	861	871	904	907	909	913	1001
X	-3	-6	-1	-2	-4	16	15	10	-19	-19
Y	6	6	7	10	10	17	18	18	13	23

$R_M = 964$  n. mi.  
 $V_i = 5631$  fps

$h_M = 29$  stat. mi.  
 $V_i = 3839$  mph

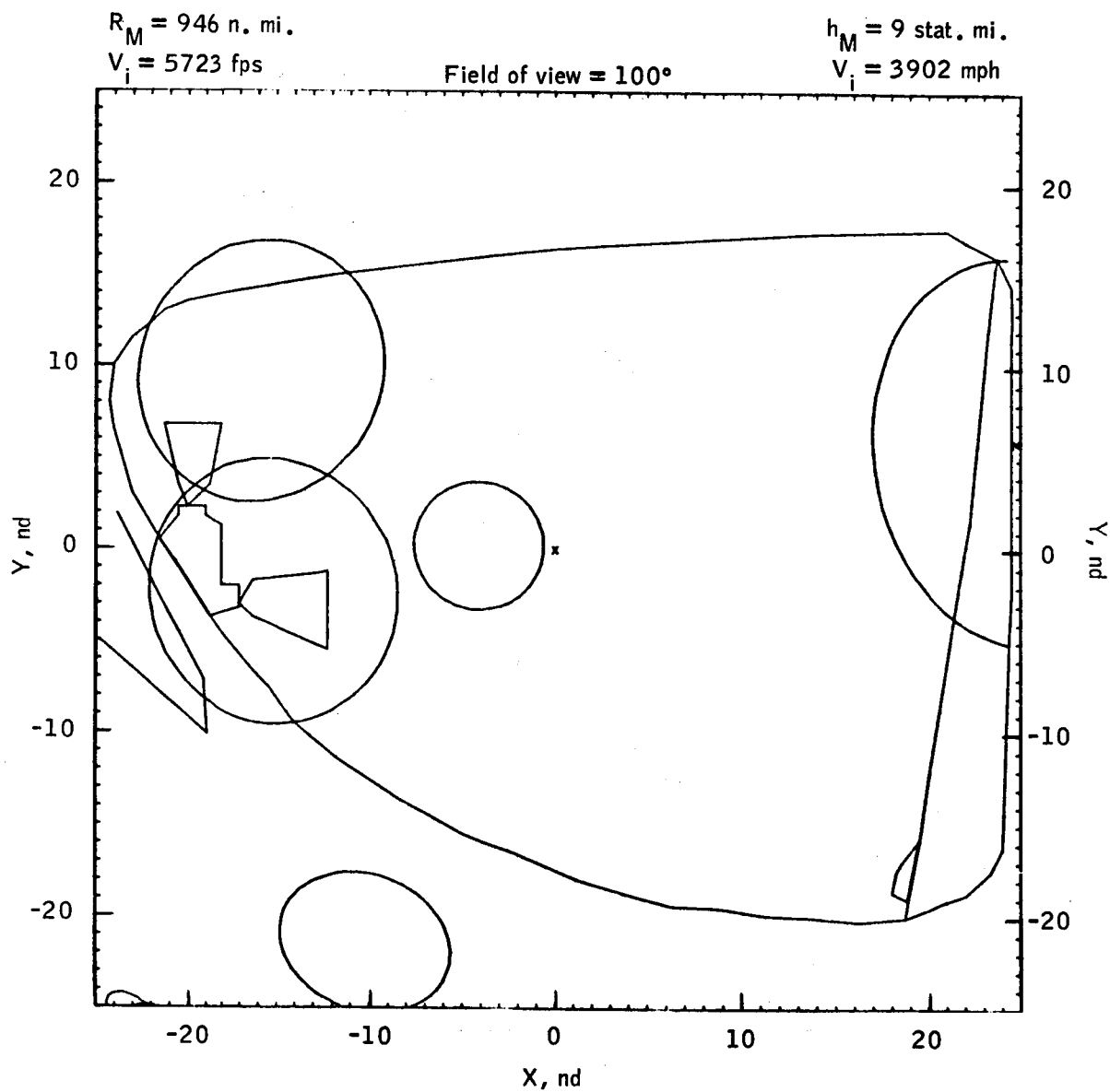
Field of view = 100°



(j) Descent stage jettison (end burn)- docking window (g.e.t. =102:33:28).

Figure 12. - Continued.





(k) Begin insertion burn - front window (g.e.t. = 102:43:18).

Figure 12.- Continued.

SEQ	4	22	31	41	47	63	73	75	80	108	111	112
X	-14	-23	-24	-13	-23	-4	-14	-5	8	6	-10	-11
Y	23	10	8	16	7	15	9	13	16	10	5	4

SEQ	120	144	150	151	186	205	215	221	1079	1082
X	-15	-2	-5	-9	2	-5	13	15	0	1
Y	1	2	1	0	-2	-5	-5	-5	22	15

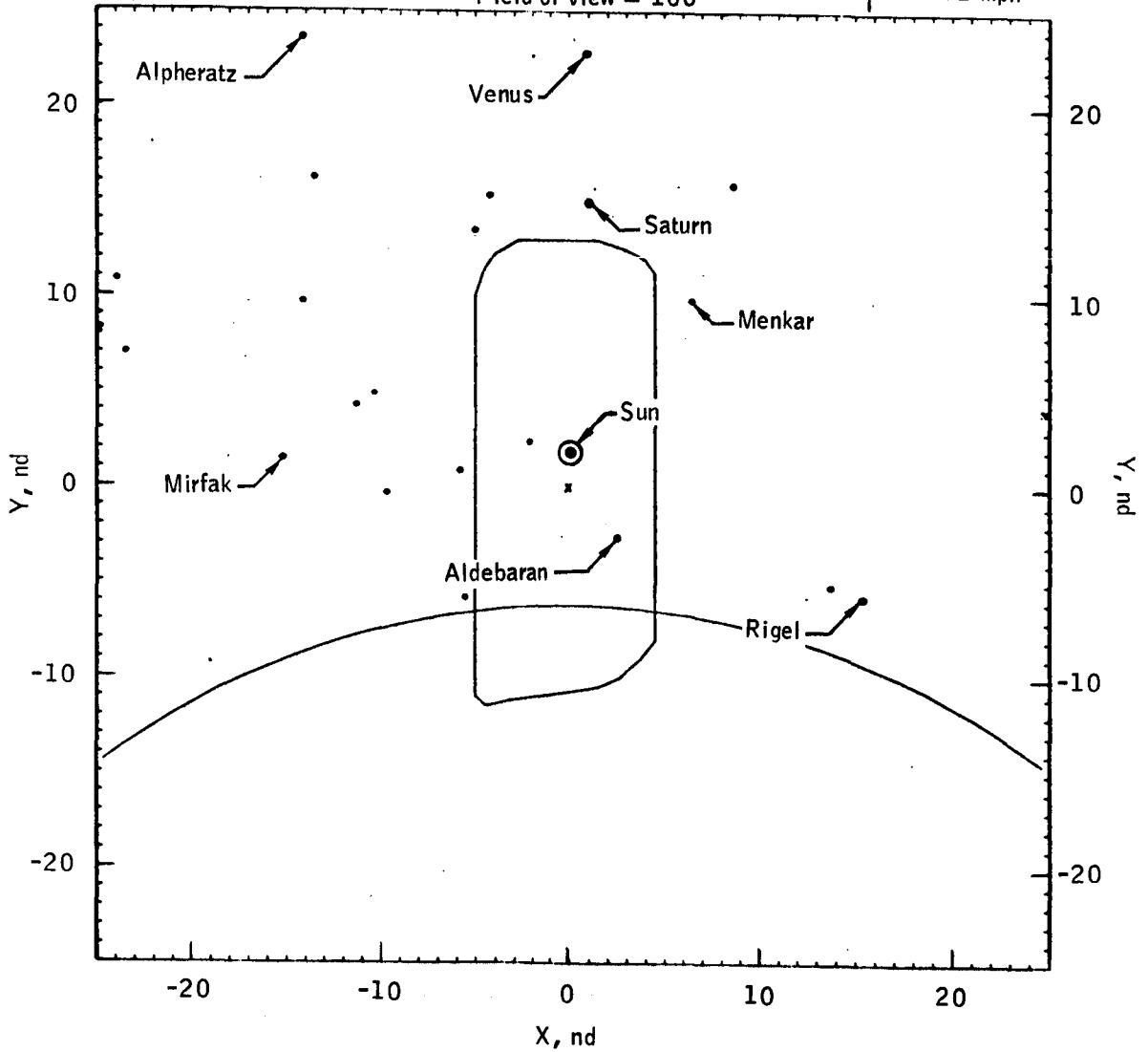
$R_M = 946$  n. mi.

$V_i = 5723$  fps

$h_M = 9$  stat. mi.

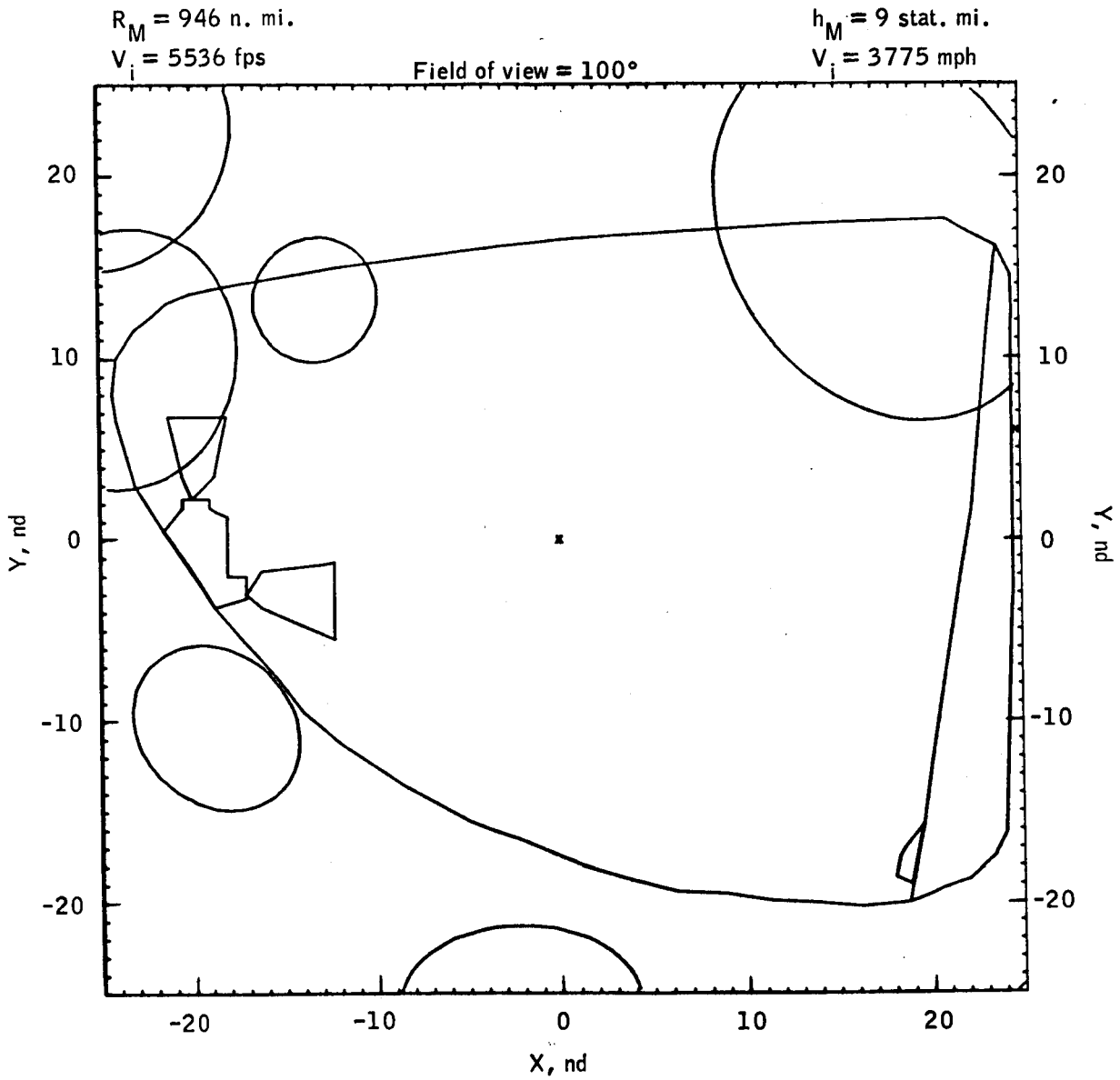
$V_i = 3902$  mph

Field of view = 100°



(I) Begin insertion burn - docking window (g.e.t. = 102:43:18).

Figure 12.- Continued.



(m) End insertion burn - front window (g.e.t. = 102:43:33).

Figure 12.- Continued.

SEQ	4	22	31	41	47	63	73	75	80	108	111	112
X	-14	-23	-24	-13	-23	-4	-14	-5	8	6	-10	-11
Y	23	10	8	16	7	15	9	13	16	10	5	4

SEQ	120	144	150	151	186	215	221	1079	1082
X	-15	-2	-5	-9	2	13	15	0	1
Y	1	2	1	0	-2	-5	-5	22	15

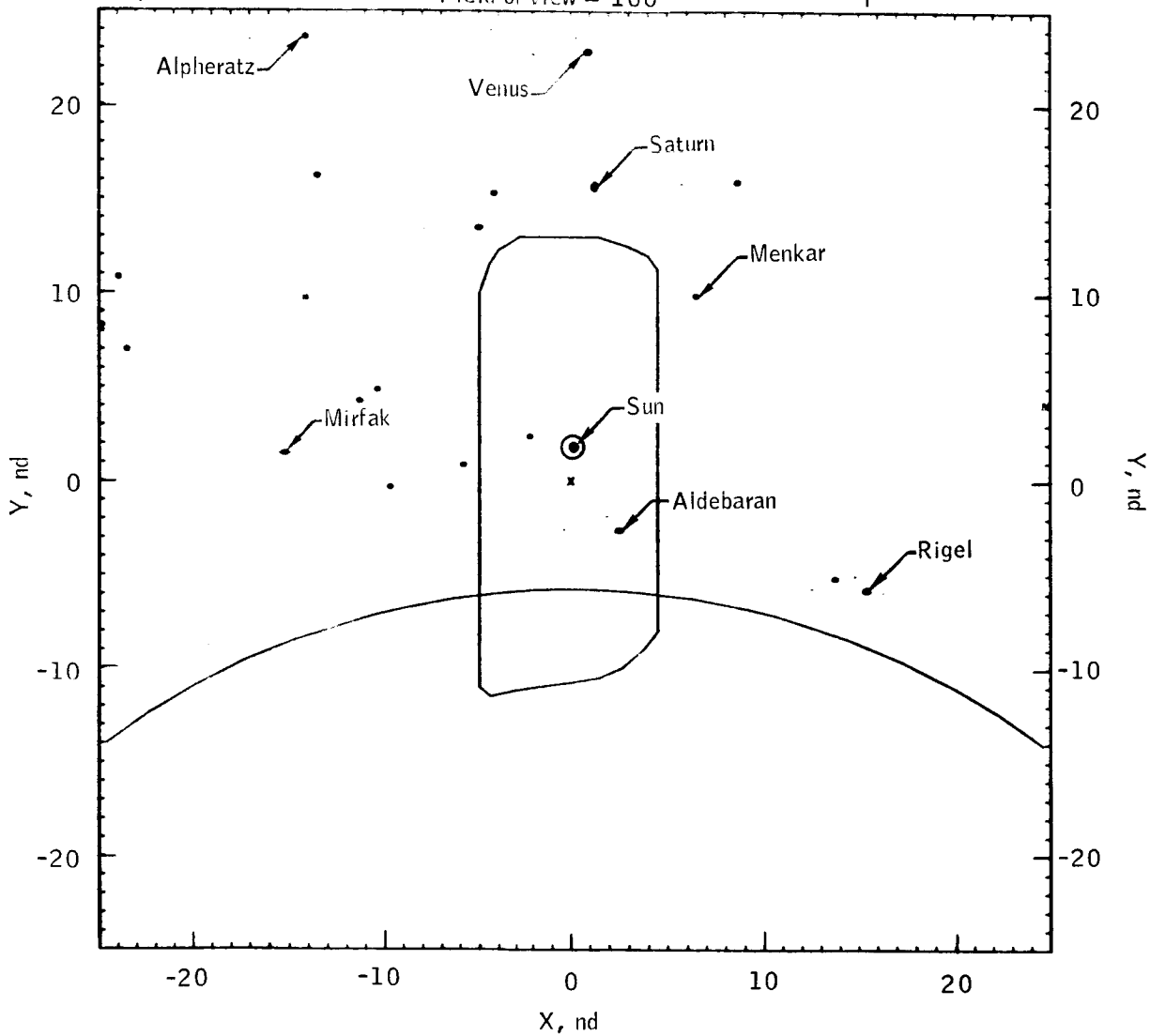
$R_M = 946$  n. mi.

$V_i = 5536$  fps

$h_M = 9$  stat. mi.

$V_i = 3775$  mph

Field of view = 100°

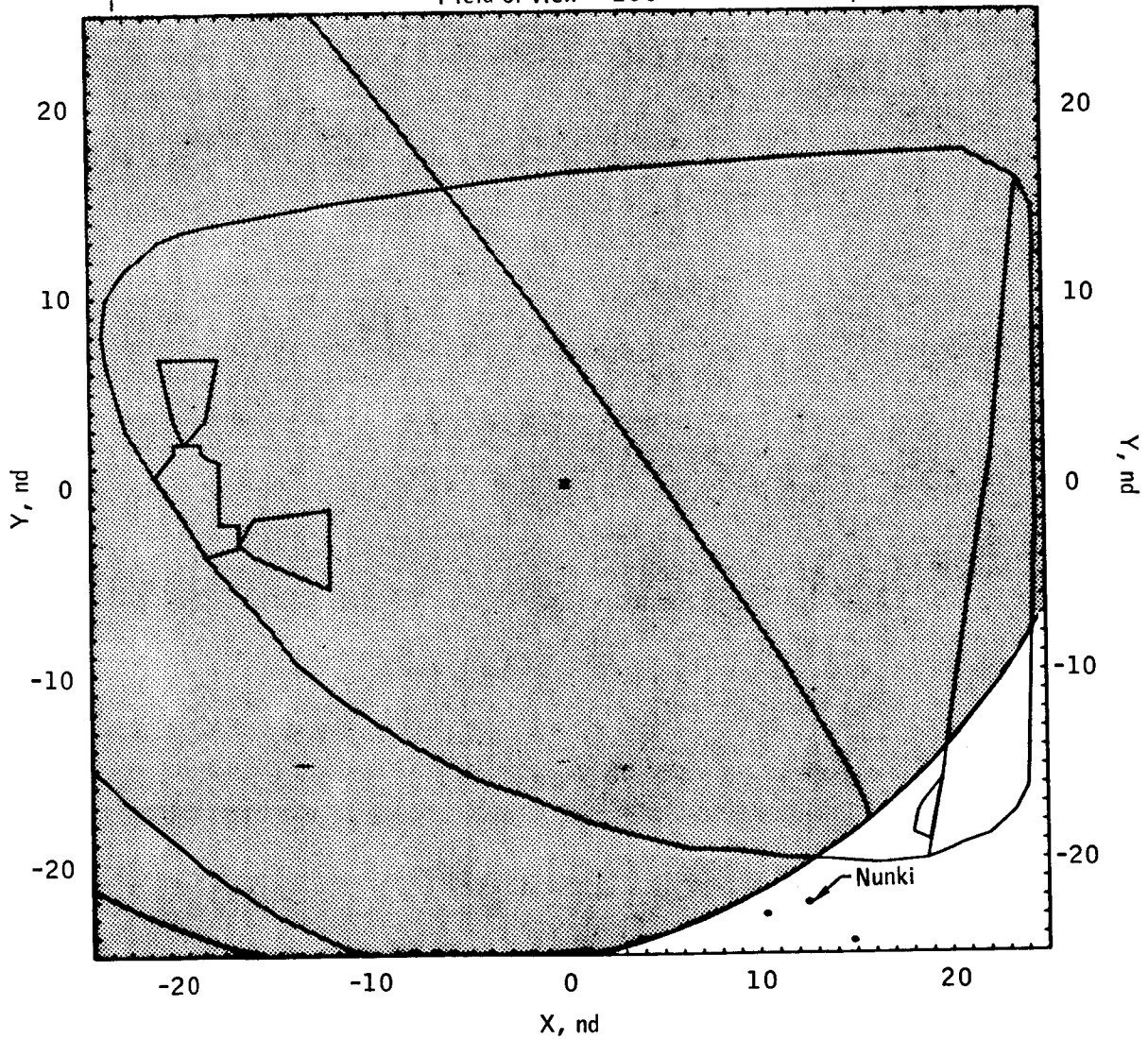


(n) End insertion burn - docking window (g.e.t. = 102:43:33).

Figure 12.- Continued.

SEQ	844	861	871
X	14	12	10
Y	-24	-22	-22

 $R_M = 982 \text{ n. mi.}$ 
 $V_i = 5338 \text{ fps}$ 

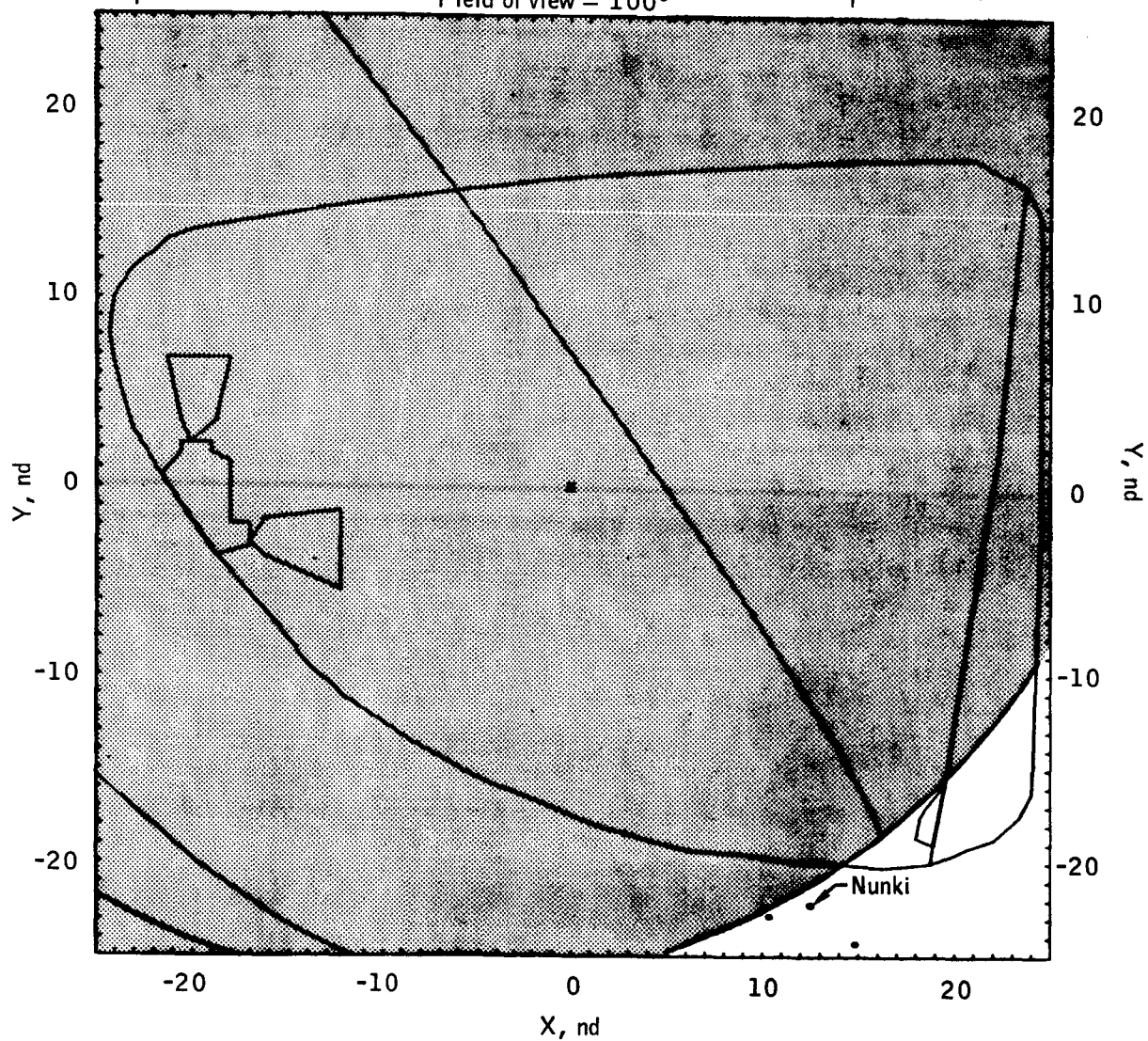
 Field of view =  $100^\circ$ 
 $h_M = 50 \text{ stat. mi.}$ 
 $V_i = 3640 \text{ mph}$ 


(o) Begin CSI burn - front window (g.e.t. = 103:33:46).

Figure 12.- Continued.

SEC	044	041	071
X	14	12	10
Y	-24	-22	-22

 $R_M = 982 \text{ n. mi.}$ 
 $V_i = 5388 \text{ fps}$ 
 $h_M = 50 \text{ stat. mi.}$ 
 $V_i = 3670 \text{ mph}$ 

 Field of view =  $100^\circ$ 


(p) End CSI burn - front window (g.e.t. = 103:34:18).

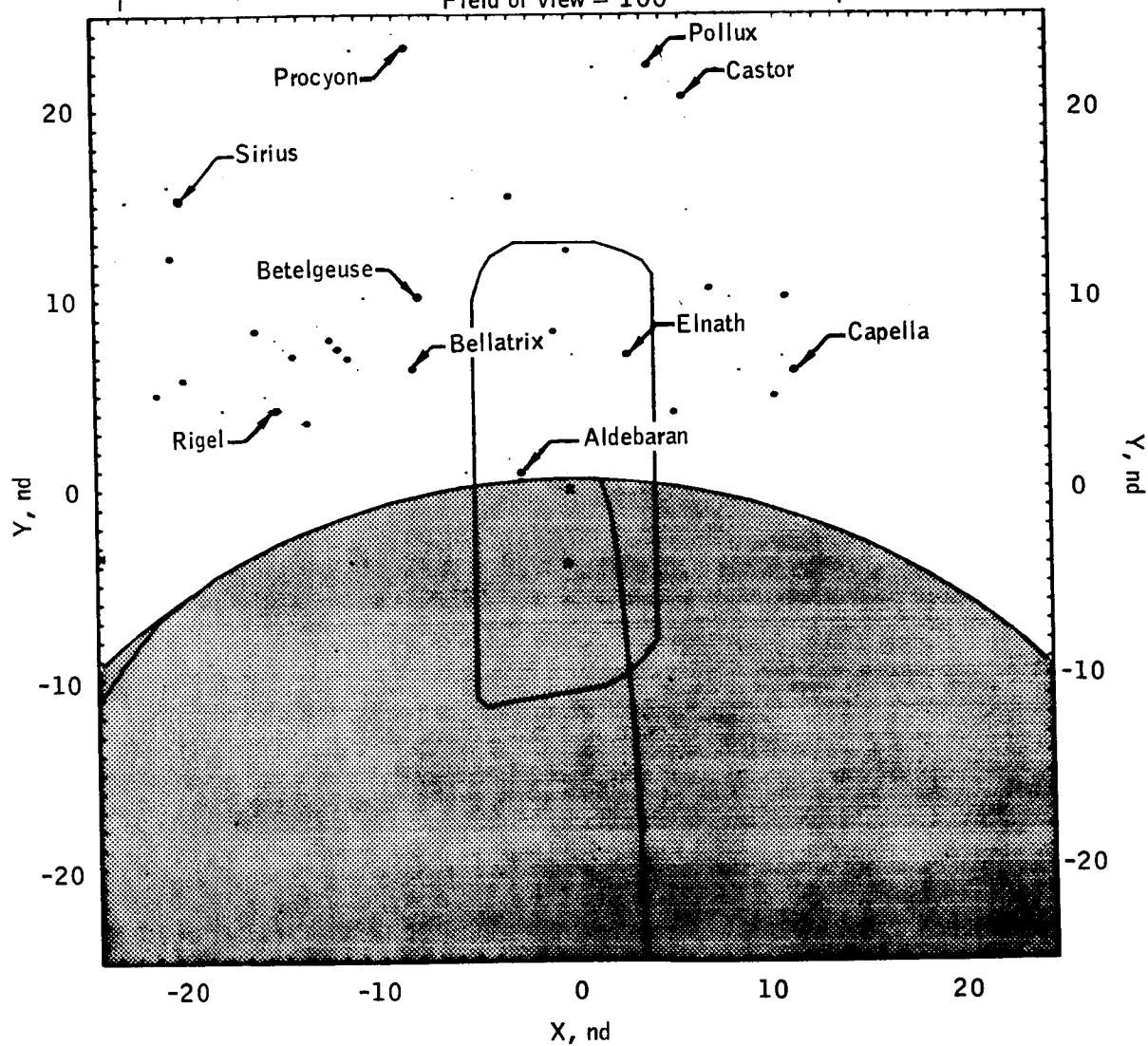
Figure 12.- Continued.

SEQ	106	205	207	215	221	222	230	231	233	237	239	245	246
X	-2	5	10	-13	-15	11	-8	3	-21	-11	-20	-19	-12
Y	1	4	5	3	4	6	6	7	5	7	5	7	7

SEQ	248	252	256	265	270	271	281	290	301	308	349	356	362
X	0	-12	-16	-7	11	7	0	-20	3	-20	6	-8	4
Y	8	8	8	10	10	10	12	12	15	15	20	23	22

 $R_M = 982 \text{ n. mi.}$ 
 $V_i = 5388 \text{ fps}$ 
 $h_M = 50 \text{ stat. mi.}$ 
 $V_i = 3670 \text{ mph}$ 

Field of view = 100°



(q) End CSI burn - docking window (g.e.t. = 103:34:18).

SEQ	751	755	757	759	770	781	789	790	793	795
X	-4	21	-22	-8	-1	-18	-11	-16	-11	9
Y	1	15	-8	1	8	-2	4	0	4	17
SEQ	797	802	803	836	841	844	861	871	1080	
X	-14	-13	5	-12	-14	-10	-13	-15	-3	
Y	2	4	16	10	9	12	14	14	3	

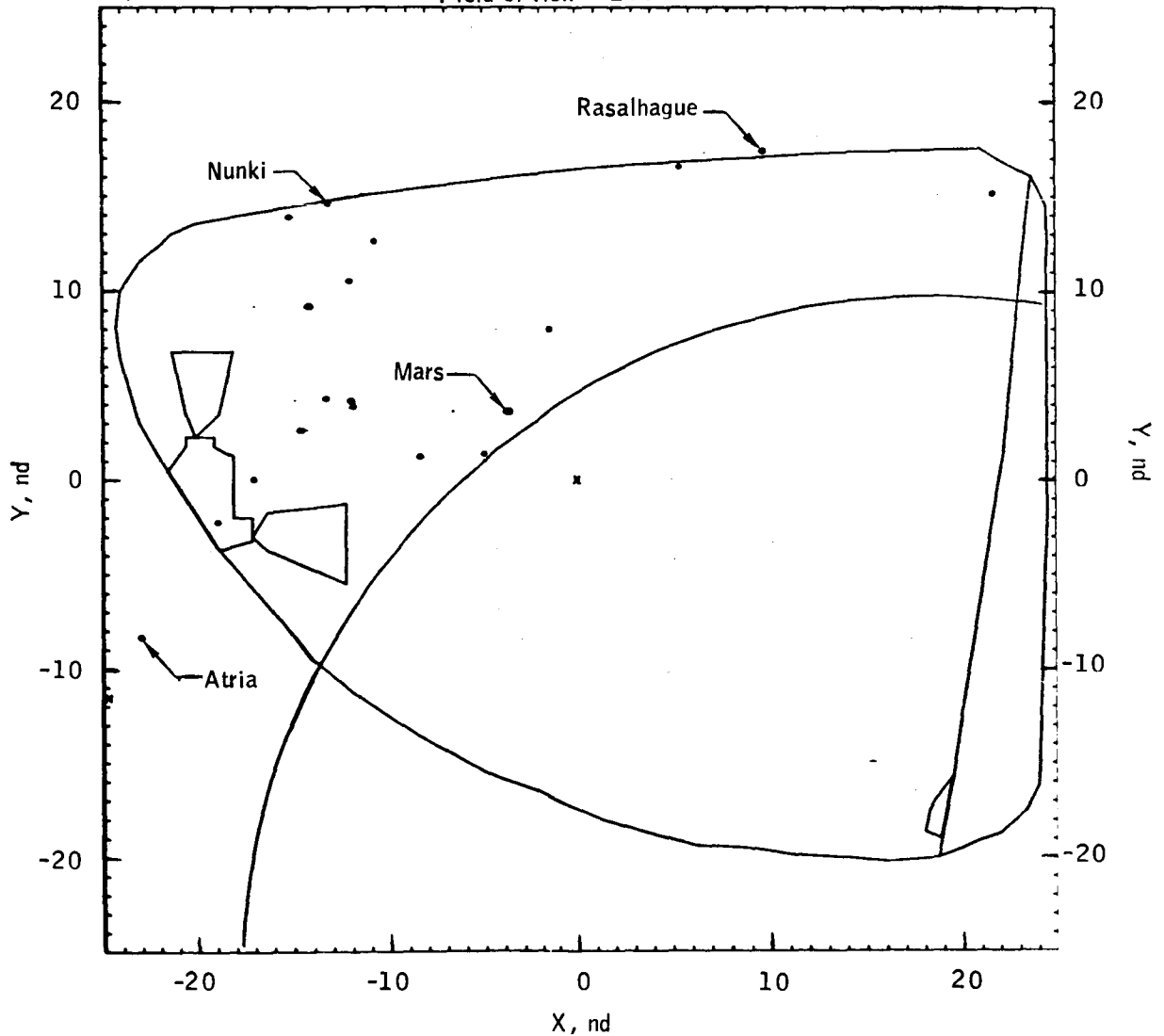
$R_M = 981$  n. mi.

$V_i = 5391$  fps

$h_M = 49$  stat. mi.

$V_i = 3676$  mph

Field of view =  $100^\circ$



(r) Begin CDH burn - front window (g.e.t. = 104:31:42).

Figure 12.- Continued.



SEQ	4	7	15	25	41	904	907	909	933	950
X	13	6	-20	-11	14	16	14	10	-20	24
Y	16	15	3	11	24	-16	-16	-17	-18	-3
SEQ	984	990	1001	1010	1028	1041	1044	1046	1079	
X	10	-1	-17	-24	-18	-11	15	9	0	
Y	-2	-7	-9	-10	-6	-1	9	7	20	

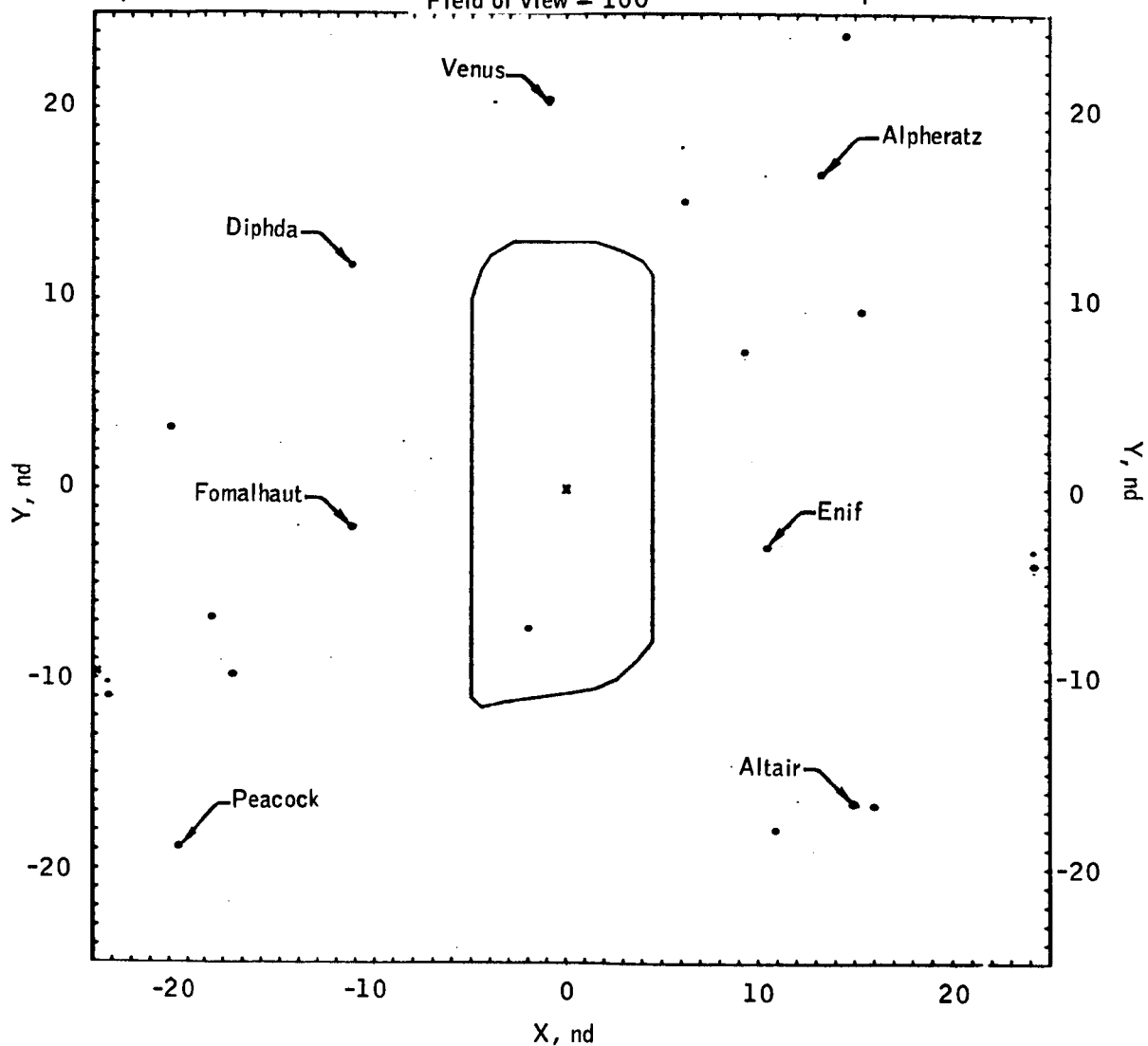
$R_M = 981$  n. mi.

$V_i = 3591$  fps

$h_M = 49$  stat. mi.

$V_i = 3676$  mph

Field of view =  $100^\circ$



(s) Begin CDH burn - docking window (g.e.t. = 104:31:42).

Figure 12.- Continued.

SEQ	751	755	759	770	781	789	790	793	795
X	-10	18	-13	-6	-24	-17	-22	-17	5
Y	9	20	8	15	4	11	6	11	24
SEQ	797	802	803	836	841	844	861	871	1080
X	-20	-18	1	-17	-19	-16	-18	-20	-9
Y	9	11	24	18	16	20	22	21	11

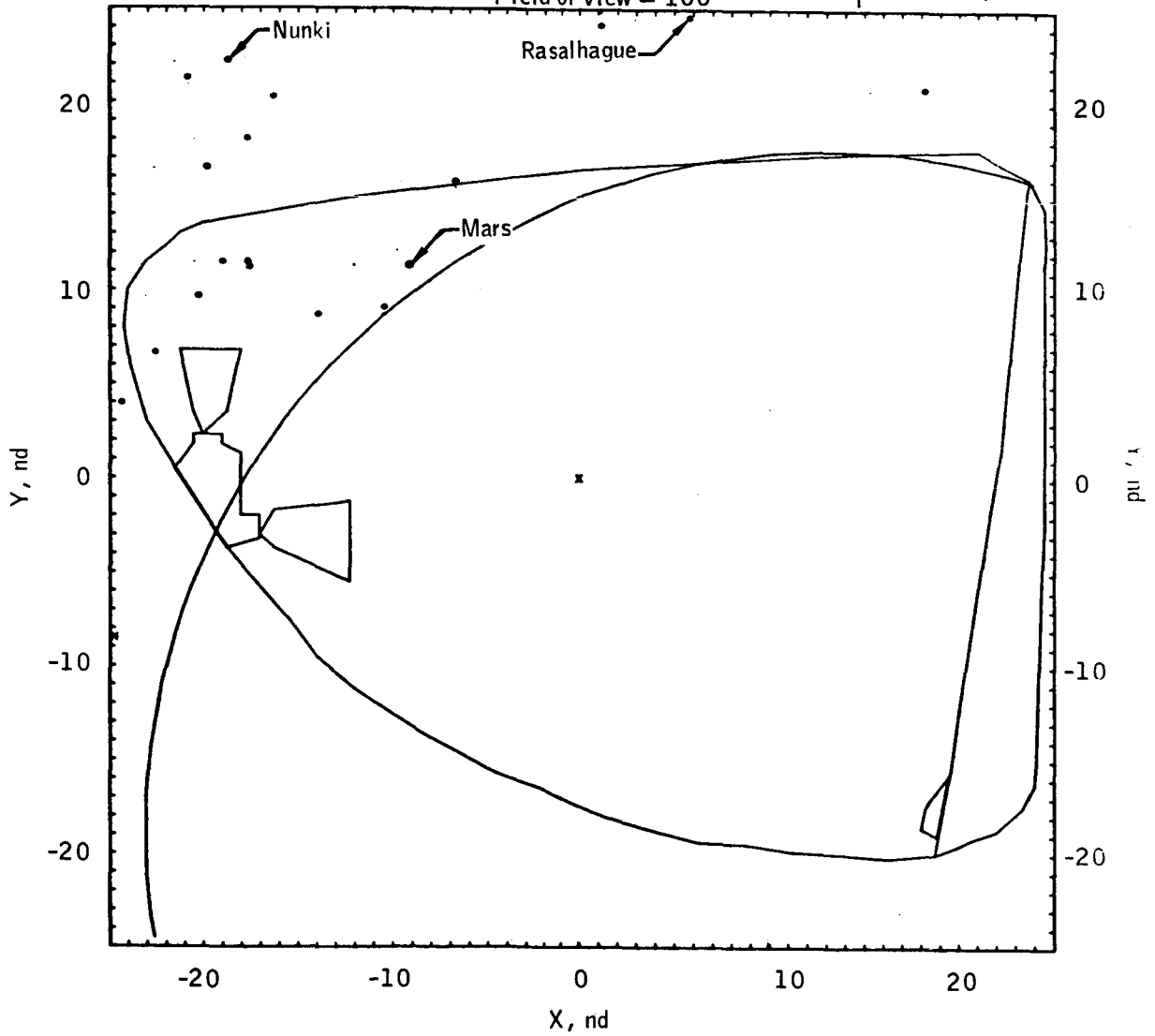
$R_M = 981$  n. mi.

$V_i = 5390$  fps

$h_M = 49$  stat. mi.

$V_i = 3675$  mph

Field of view =  $100^\circ$



(t) End of CDH burn - front window (g.e.t. = 104:31:45).

Figure 12.- Continued.

SEQ	7	15	25	781	795	803	836	841	844	861	871	904
X	6	-21	-11	-19	20	15	-4	-6	-1	-2	-4	15
Y	24	10	20	-24	-23	-24	-22	-21	-21	-18	-17	-8
SEQ	907	909	933	950	984	990	1001	1010	1028	1041	1044	1046
X	14	10	-19	24	10	-1	-17	-23	-18	-11	16	9
Y	-7	-8	-10	3	6	2	-1	-3	1	7	17	16

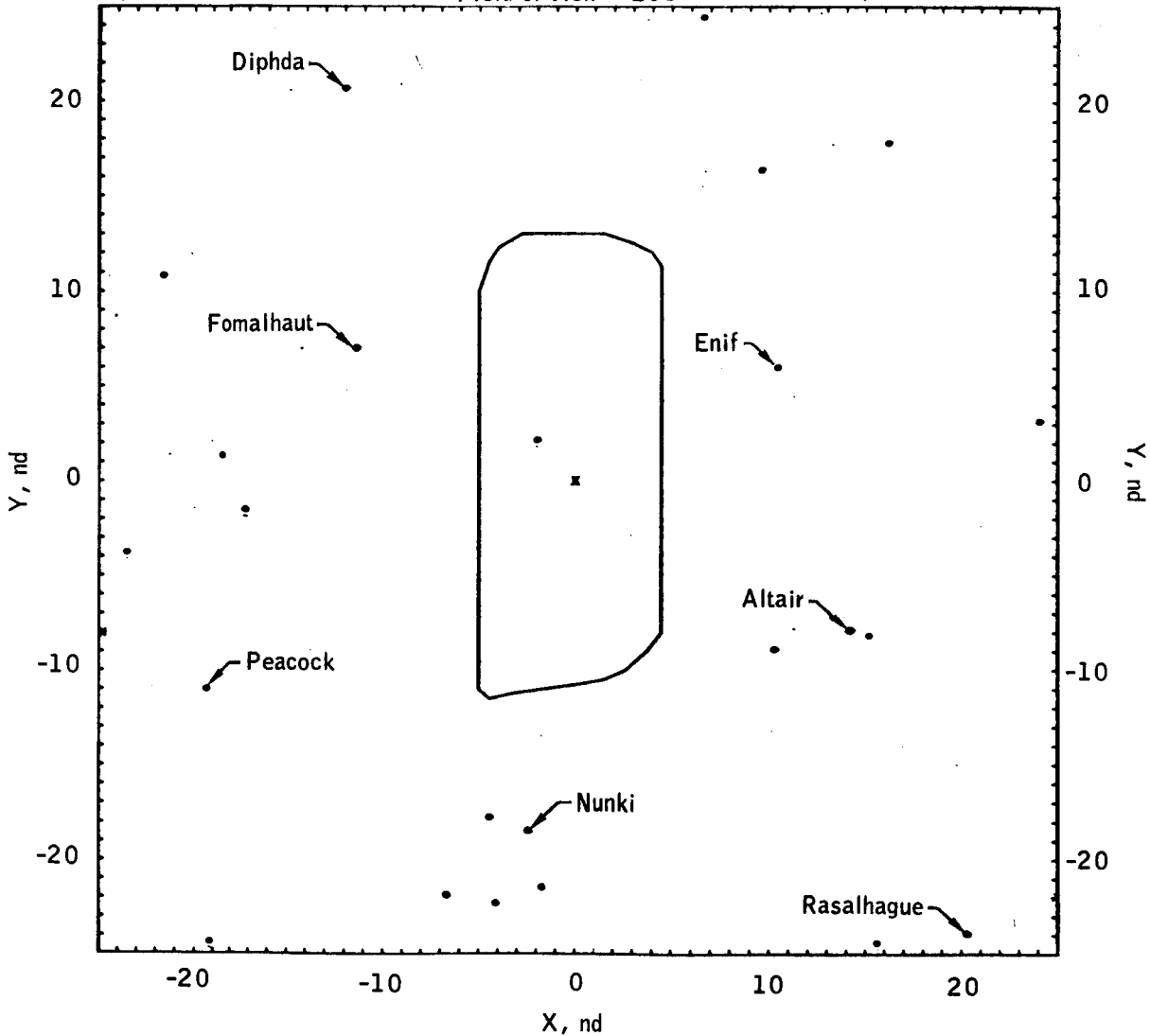
$R_M = 981$  n. mi.

$h_M = 49$  stat. mi.

$V_i = 5390$  fps

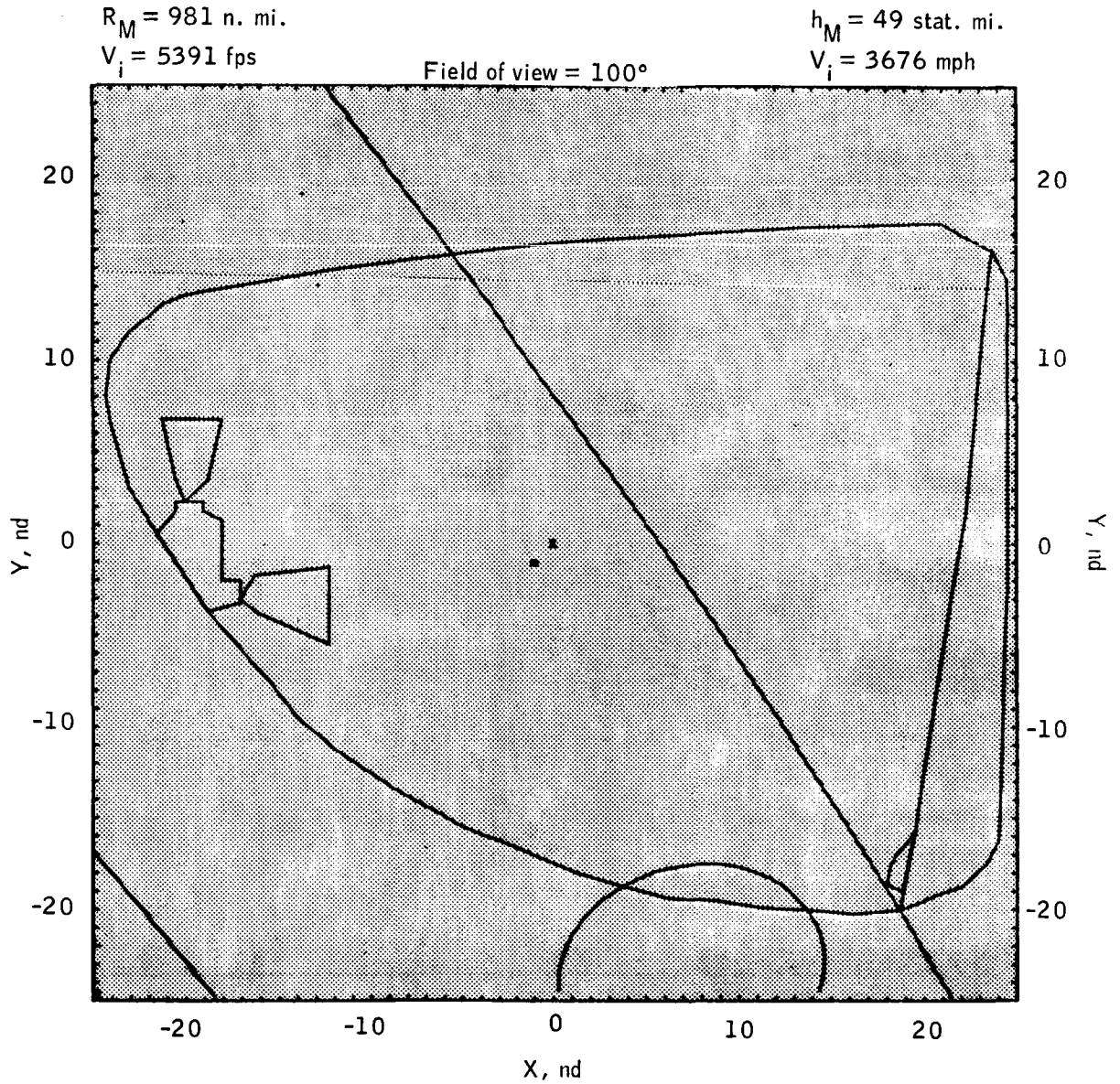
$V_i = 3675$  mph

Field of view =  $100^\circ$



(u) End of CDH burn - docking window (g.e.t. = 104:31:45).

Figure 12.- Continued.



(v) Begin TPI burn - front window (g.e.t. = 105:08:57).

Figure 12.- Continued.

SEQ	377	440	473	480	507	515	535	540	545	551	566	569
X	-21	-10	0	4	23	7	6	24	-24	-7	-9	-22
Y	-11	-5	-4	-4	-7	1	6	-3	18	15	10	21
SEQ	570	580	582	589	593	595	610	624	651	1001		
X	1	20	8	-14	0	-7	15	17	22	1		
Y	15	6	15	24	22	24	18	20	20	0		

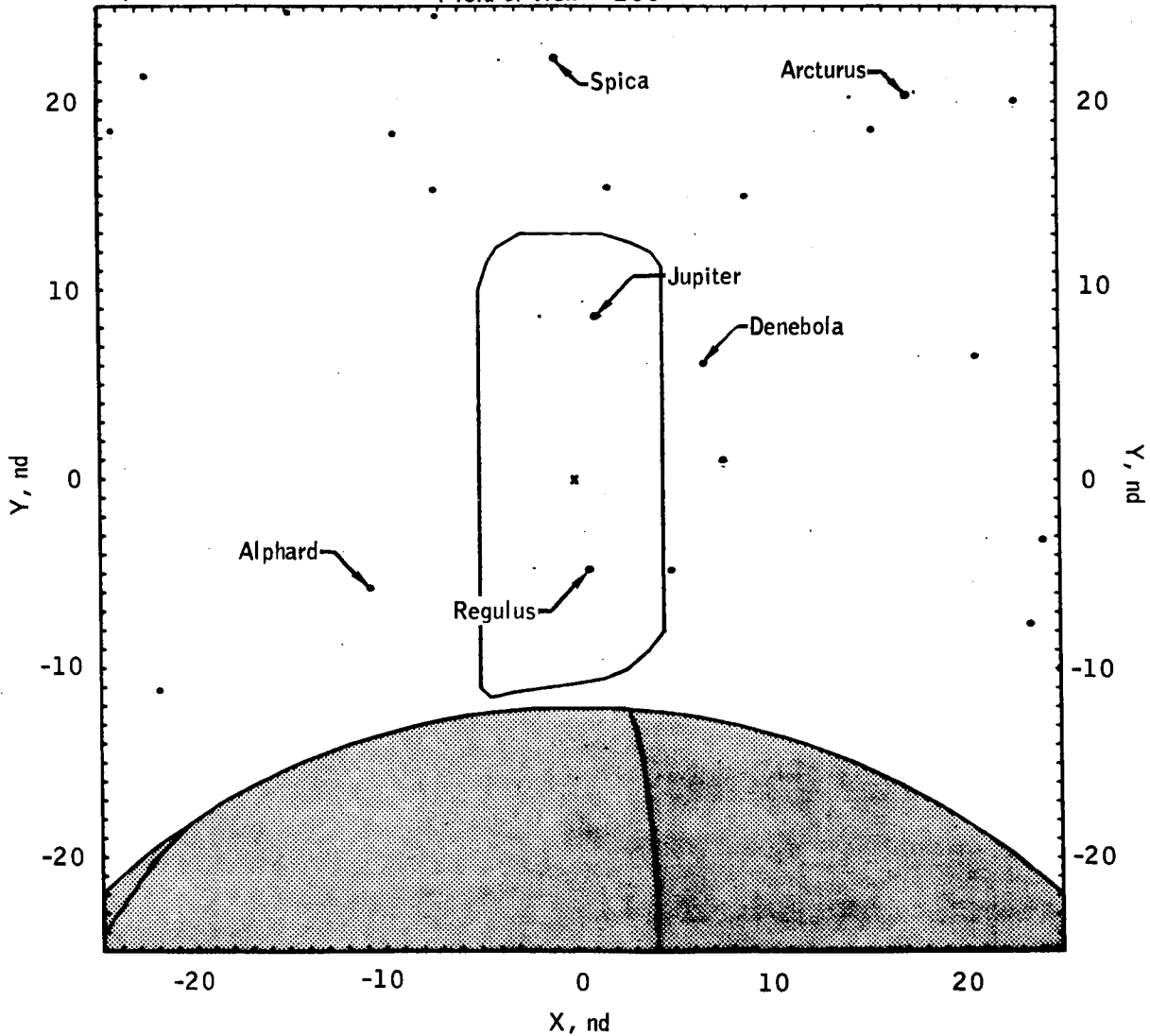
$R_M = 981$  n. mi.

$h_M = 49$  stat. mi.

$V_i = 5391$  fps

$V_i = 3676$  mph

Field of view = 100°



(w) Begin TPI burn - docking window (g.e.t. = 105:08:57).

Figure 12.- Continued.

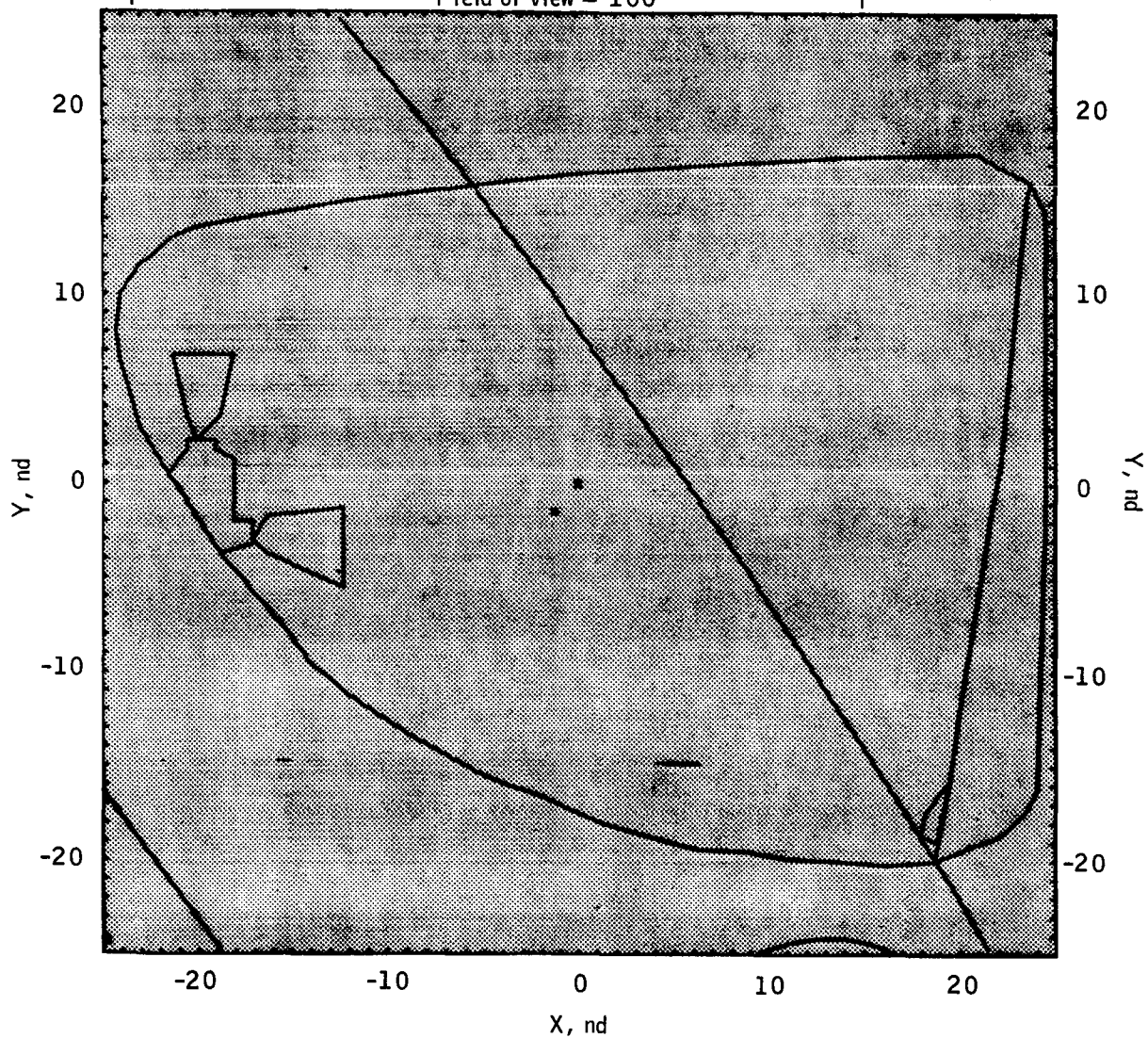
$R_M = 9809$  n. mi.

$V_i = 5413$  fps

$h_M = 49$  stat. mi.

$V_i = 3676$  mph

Field of view =  $100^\circ$

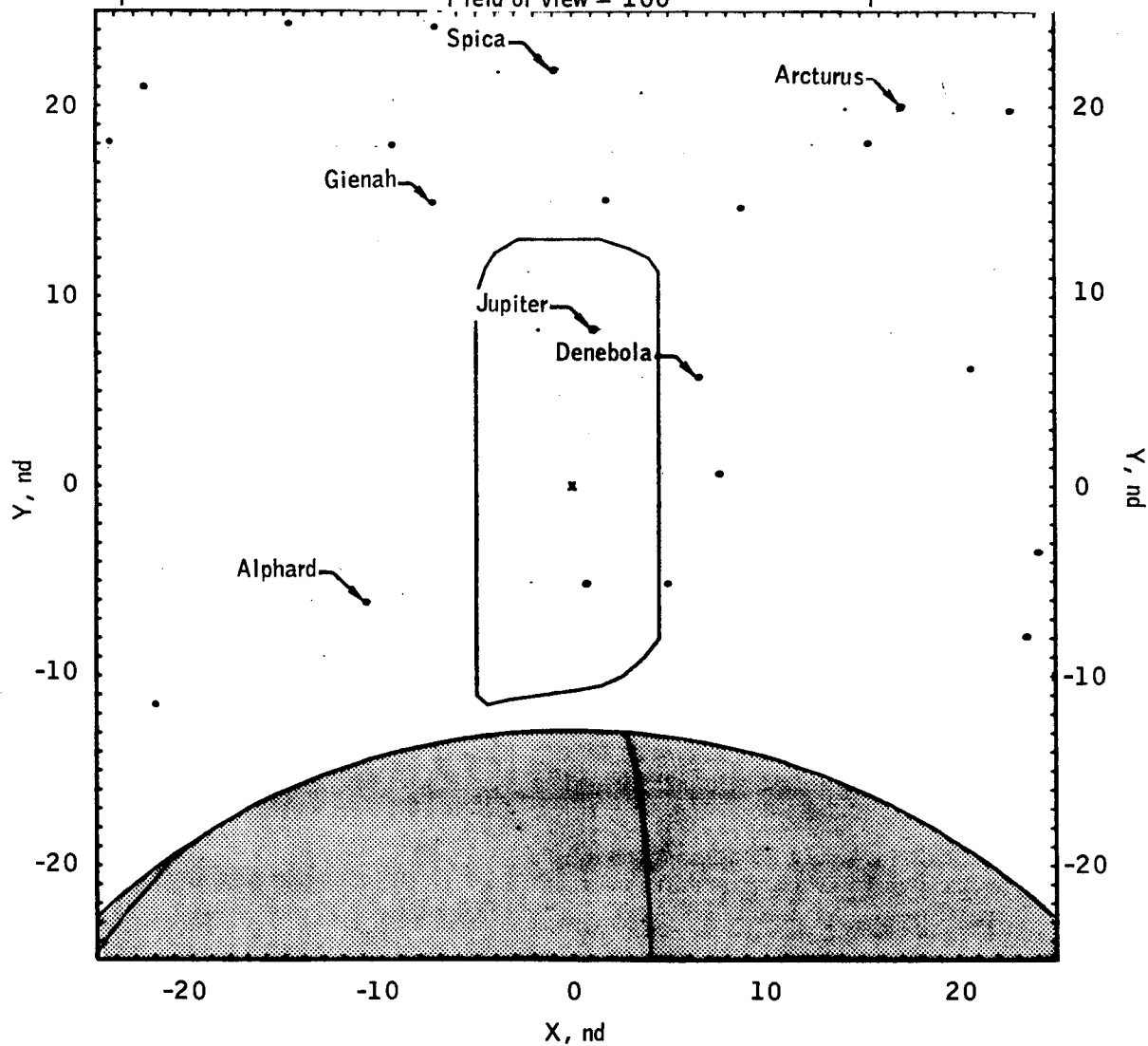


(x) End TPI burn - front window (g.e.t. = 105:09:13).

Figure 12.- Continued.

SEQ	377	440	473	480	507	515	535	540	545	551	566	569
X	-21	-10	0	4	23	7	6	24	-24	-7	-9	-22
Y	-11	-5	-4	-4	-7	0	5	-3	18	15	18	21

SEQ	570	580	582	589	593	595	610	624	651	1001
X	1	20	8	-14	0	-7	15	17	22	1
Y	15	6	14	24	22	24	18	20	19	8

 $R_M = 9809$  n. mi. $h_M = 49$  stat. mi. $V_i = 5431$  fps $V_i = 3676$  mphField of view =  $100^\circ$ 

(y) End of TPI burn - docking window (g.e.t. = 105:09:13).

Figure 12.- Concluded.

TRANSEARTH INJECTION  
BURN



SEQ	22	31	41	47	63	73	75	80	100	111	112	120	144	150	151	186
X	-23	-24	-12	-23	-4	-13	-4	8	6	-10	-11	-15	-2	-6	-10	2
Y	0	-2	2	-4	0	-3	-1	1	-4	-9	-9	-11	-12	-13	-14	-17

SEQ	205	207	215	221	222	230	231	233	237	239	245	246	248	252	256
X	-6	-11	14	16	-13	8	-3	23	12	22	15	13	0	13	18
Y	-20	-20	-18	-18	-21	-22	-23	-17	-22	-19	-21	-22	-24	-23	-22

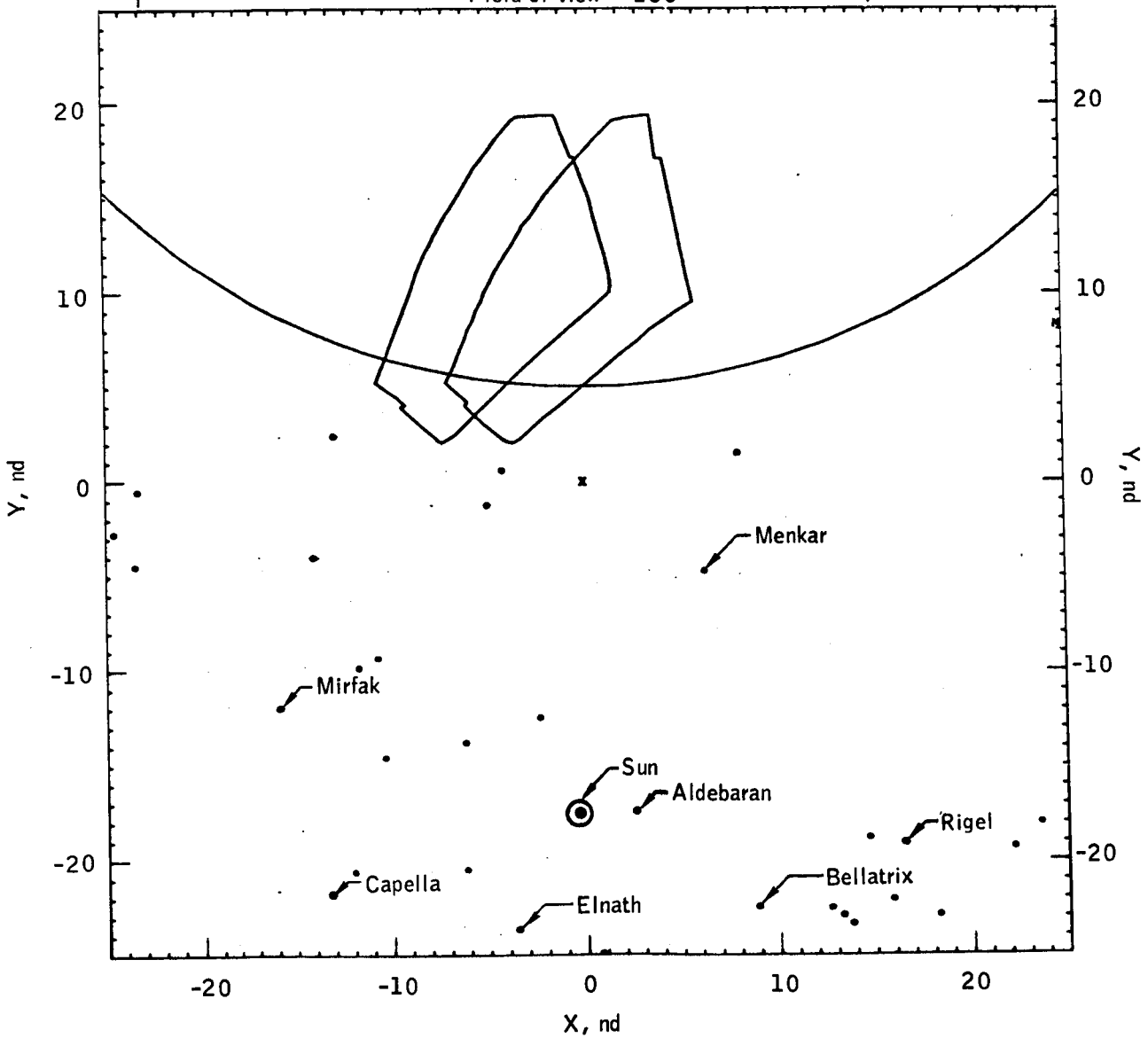
$R_M = 996$  n. mi.

$V_i = 5349$  fps

Field of view =  $100^\circ$

$h_M = 66$  stat. mi.

$V_i = 4758$  mph



(a) Begin TEI burn (g.e.t. = 137:20:22.4).

Figure 13.- Transearth injection burn.

SEG	41	63	73	75	80	108	111	112	120	144	150	151	186	205
X	-15	-8	-16	-7	5	10	13	14	18	-4	-8	-12	0	-8
Y	2	0	-4	-1	1	-4	-9	-10	-12	-12	-14	-14	-17	-20
SEG	207	215	221	222	230	231	233	237	239	245	246	252	256	
X	-14	12	14	-15	6	-5	21	10	19	13	11	11	16	
Y	-20	-18	-19	-22	-22	-23	-17	-22	-19	-21	-22	-23	-22	

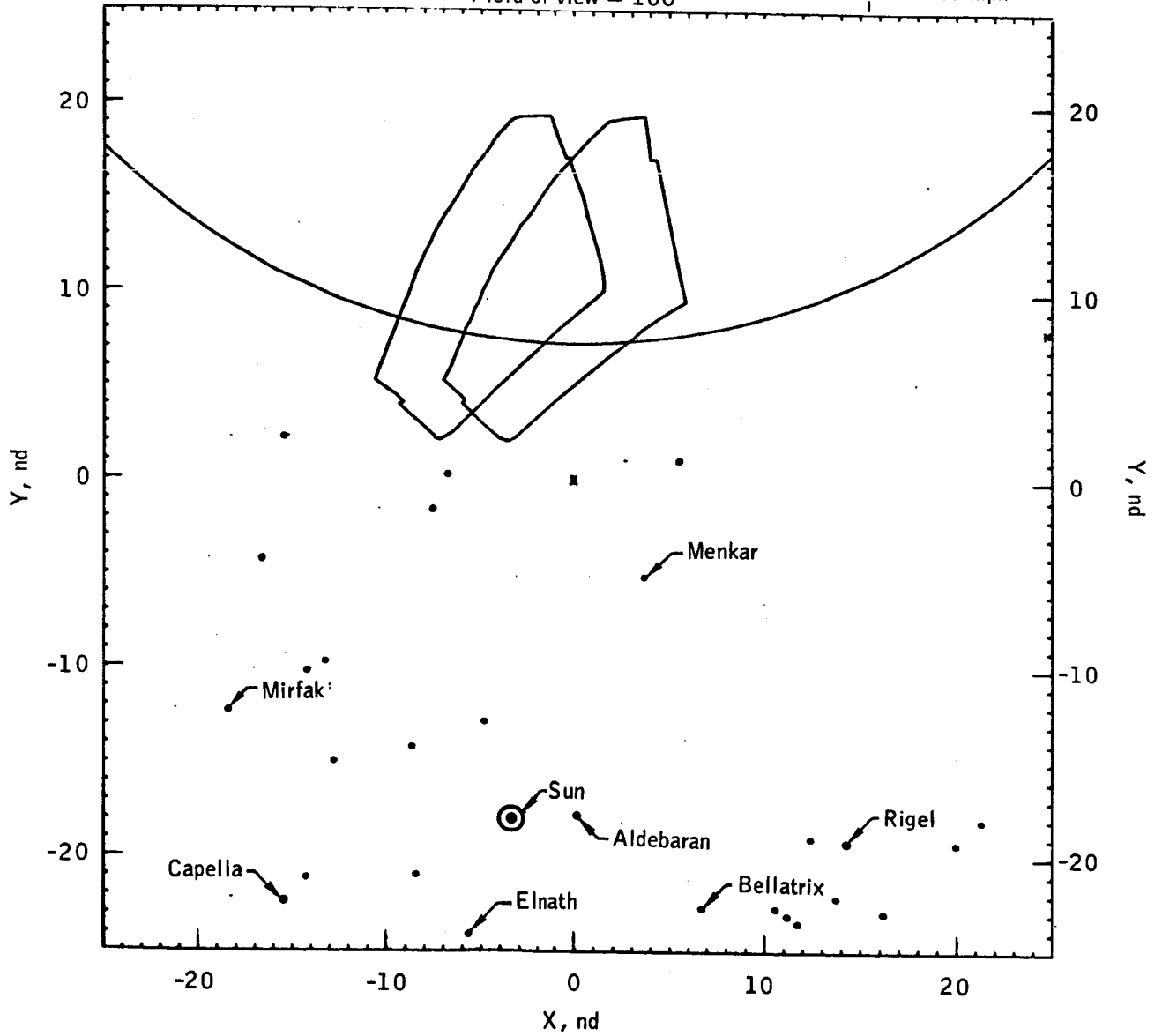
$R_M = 995$  n. mi.

$V_i = 6978$  fps

$h_M = 67$  stat. mi.

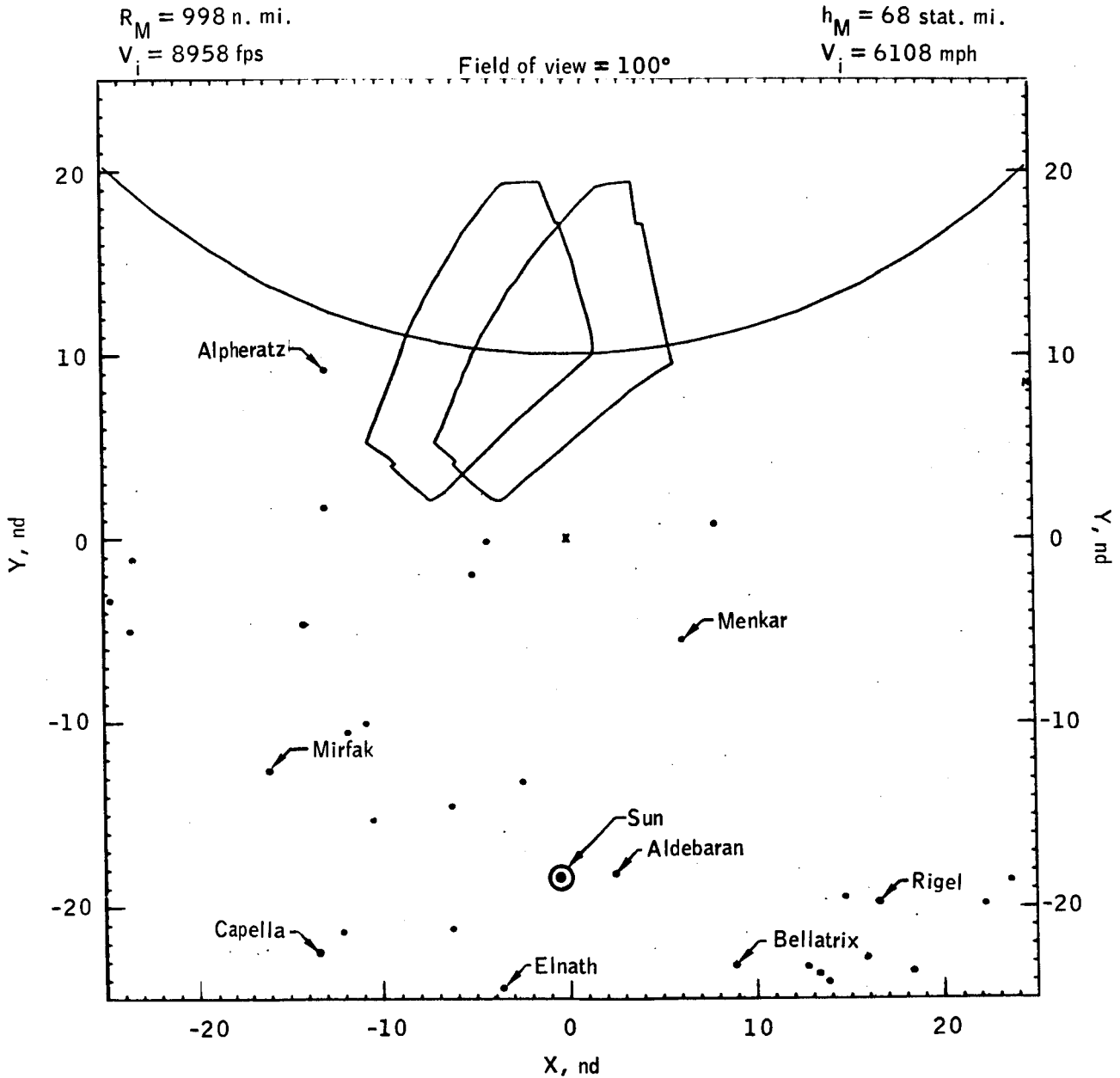
$V_i = 3647$  mph

Field of view = 100°



(b) Middle of TEI burn (g.e.t. = 137:21:52.4).

SEQ	4	22	31	41	47	63	73	75	80	108	111	112	120	144	150	151
X	-12	-23	-24	-12	-23	-4	-14	-5	7	6	-10	-11	-15	-2	-6	-10
Y	9	0	-3	1	-4	0	-4	-1	0	-5	-9	-10	-12	-13	-14	-15
SEQ	186	205	207	215	221	222	230	231	233	237	239	245	246	252	256	
X	2	-6	-12	14	16	-13	6	-3	23	12	22	15	13	13	10	
Y	-18	-21	-21	-19	-19	-22	-23	-24	-18	-93	-19	-22	-23	-23	-23	



(c) End of TEI burn (g.e.t. = 137:23:11.3).

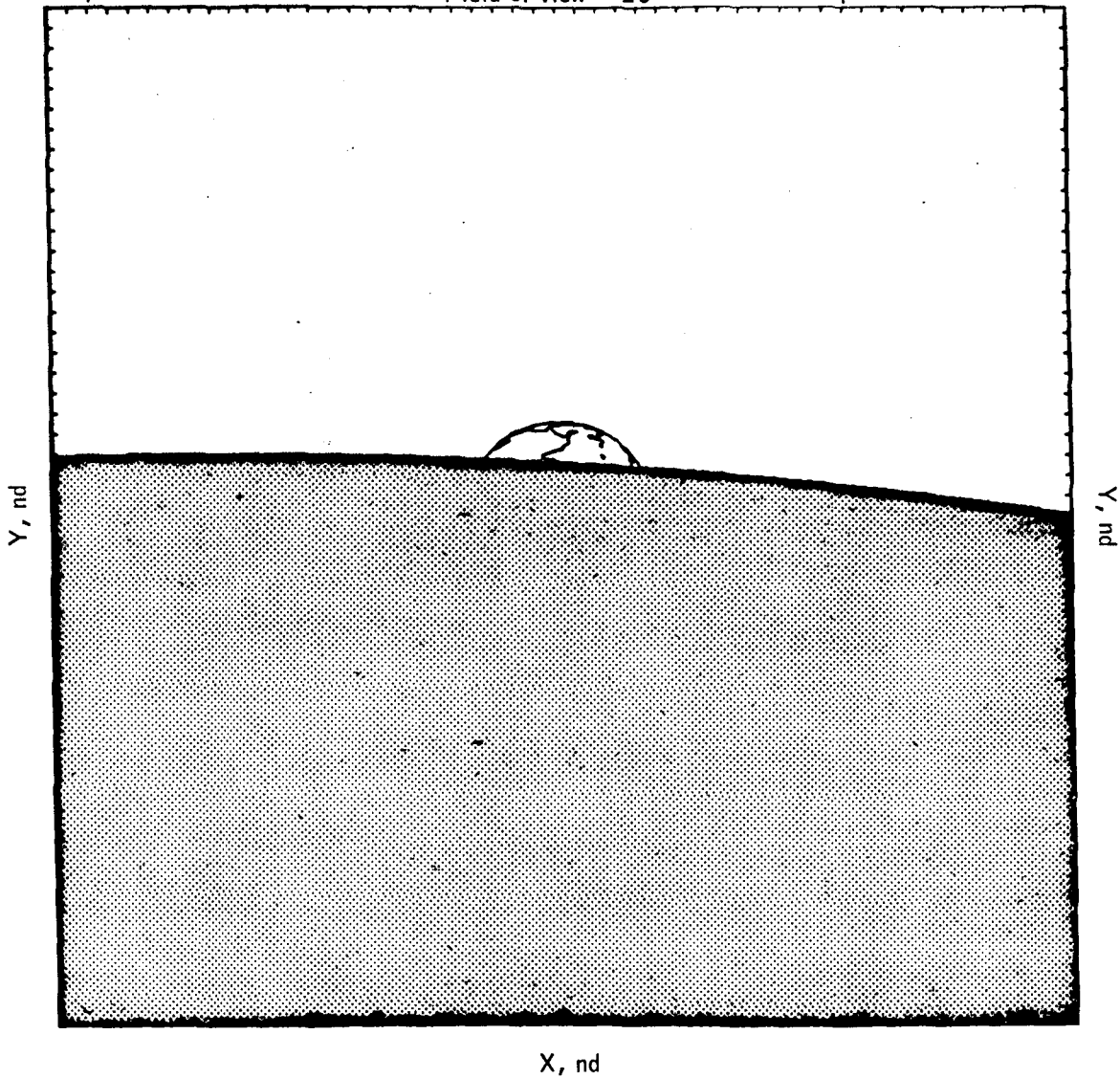
TRANSEARTH COAST

POST TEI

$R_M = 1109$  n. mi.  
 $V_i = 8632$  fps

$h_M = 198$  stat, mi.  
 $V_i = 5885$  mph

Field of view =  $10^\circ$



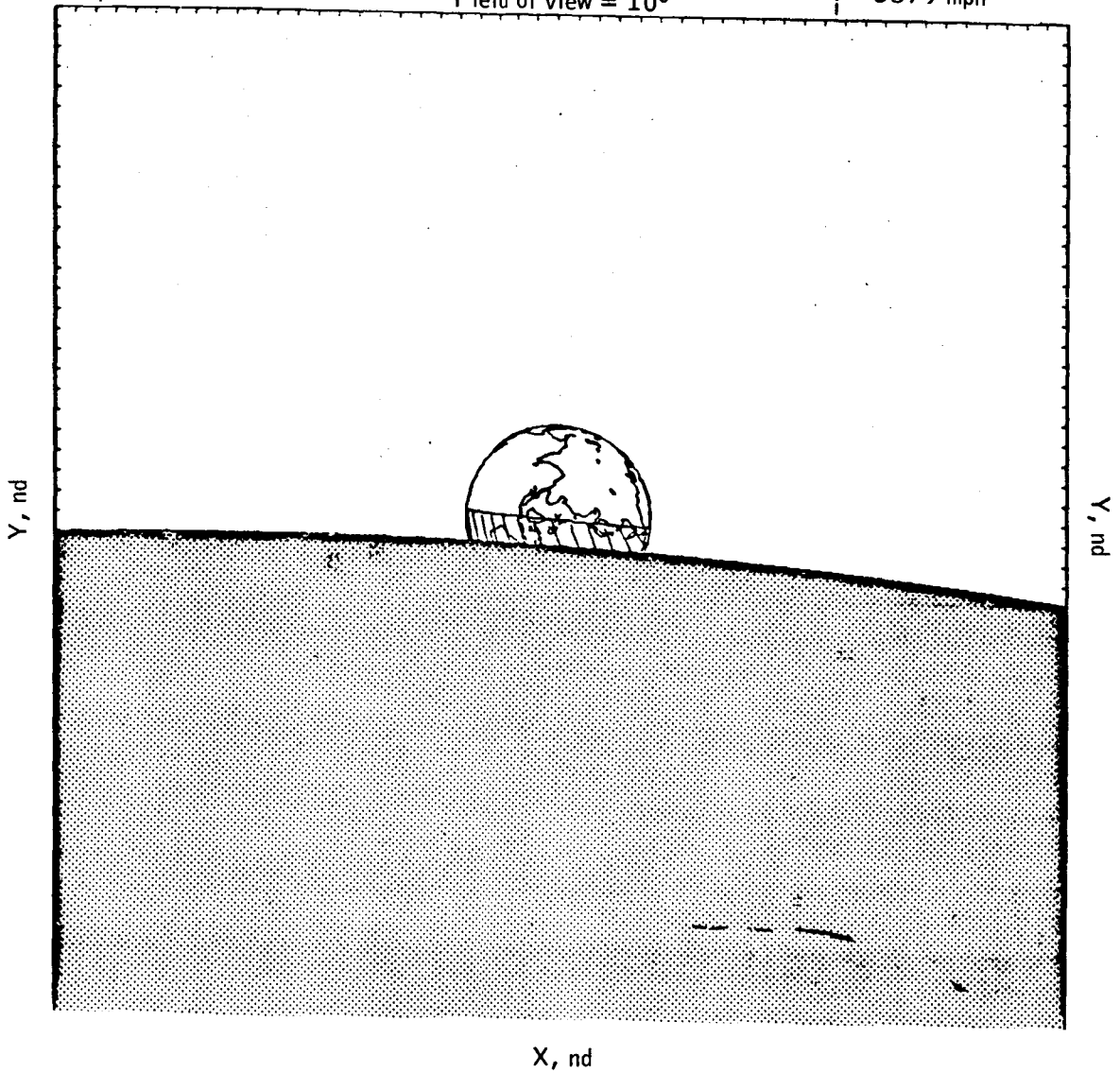
(a) G. e. t. = 137:29:11.3.

Figure 14. - Post TEI.

$R_M = 1113 \text{ n. mi.}$   
 $V_i = 8622 \text{ fps}$

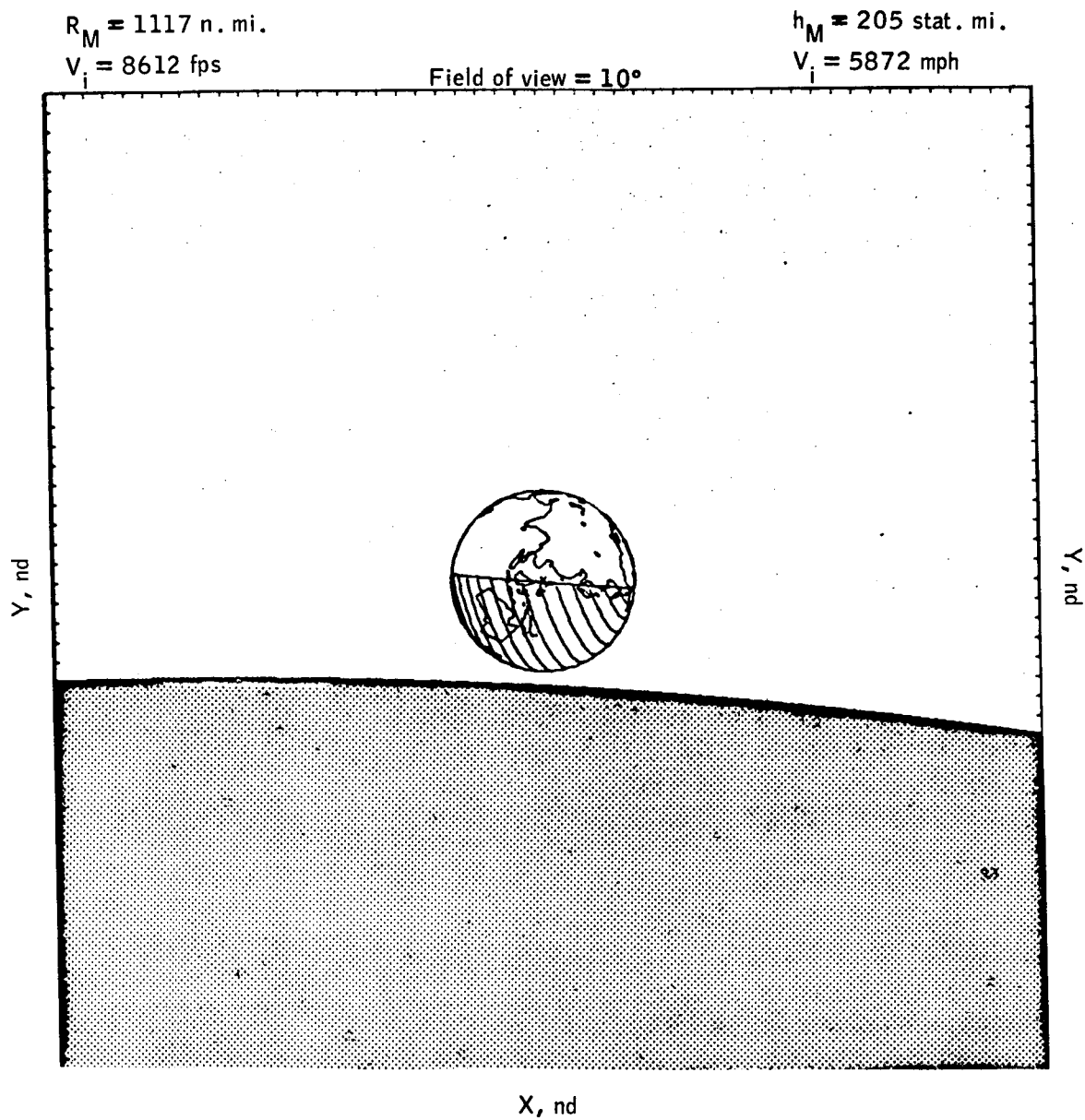
$h_M = 200 \text{ stat. mi.}$   
 $V_i = 5879 \text{ mph}$

Field of view =  $10^\circ$



(b) G.e.t. = 137:29:18.5.

Figure 14.- Continued.



(c) G.e.t. = 137:29:25.7.

Figure 14.- Continued.



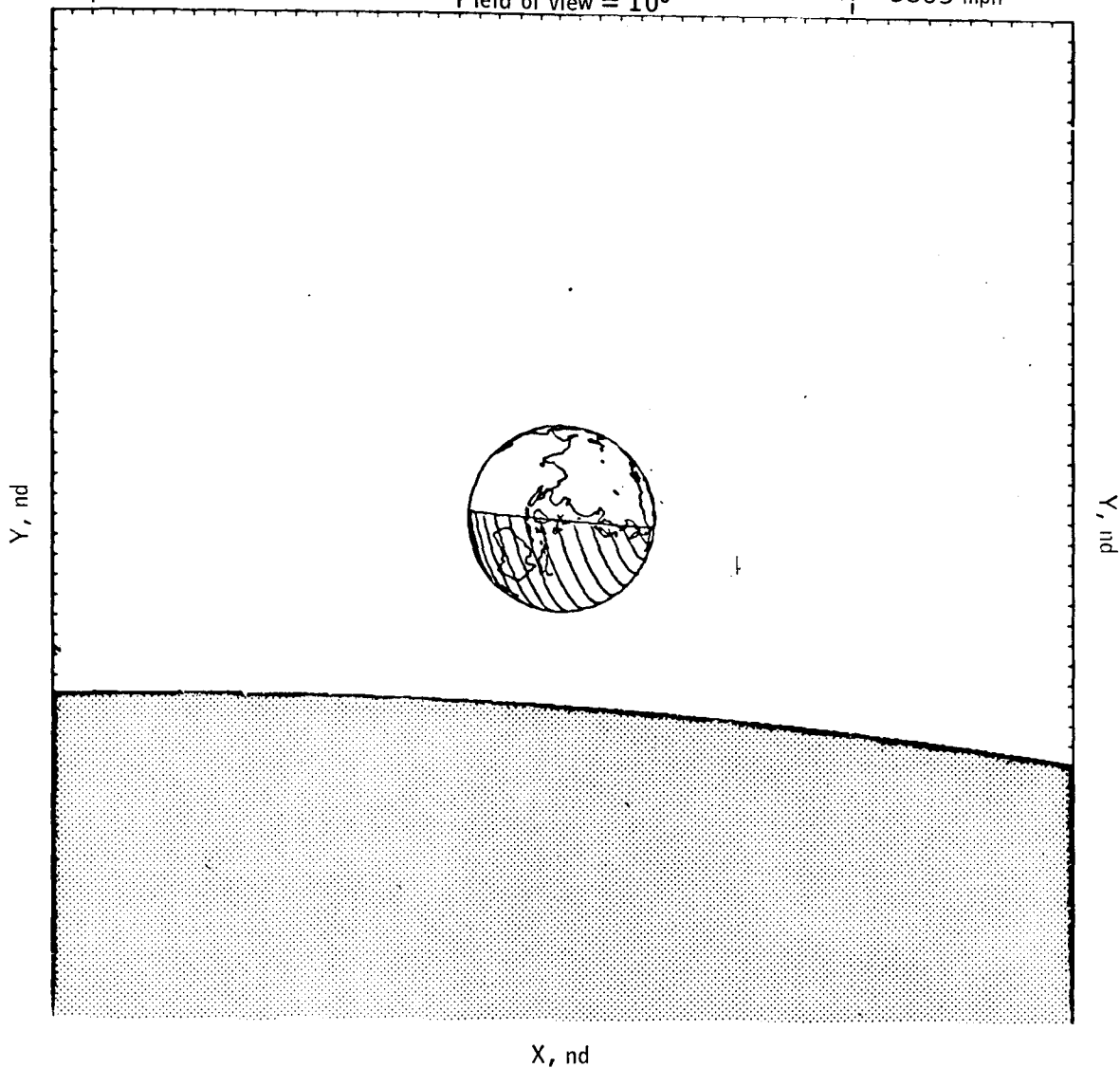
$R_M = 1121$  n. mi.

$V_i = 8602$  fps

$h_M = 209$  stat. mi.

$V_i = 5865$  mph

Field of view =  $10^\circ$



(d) G.e.t. = 137:29:32.9.

Figure 14.- Concluded.

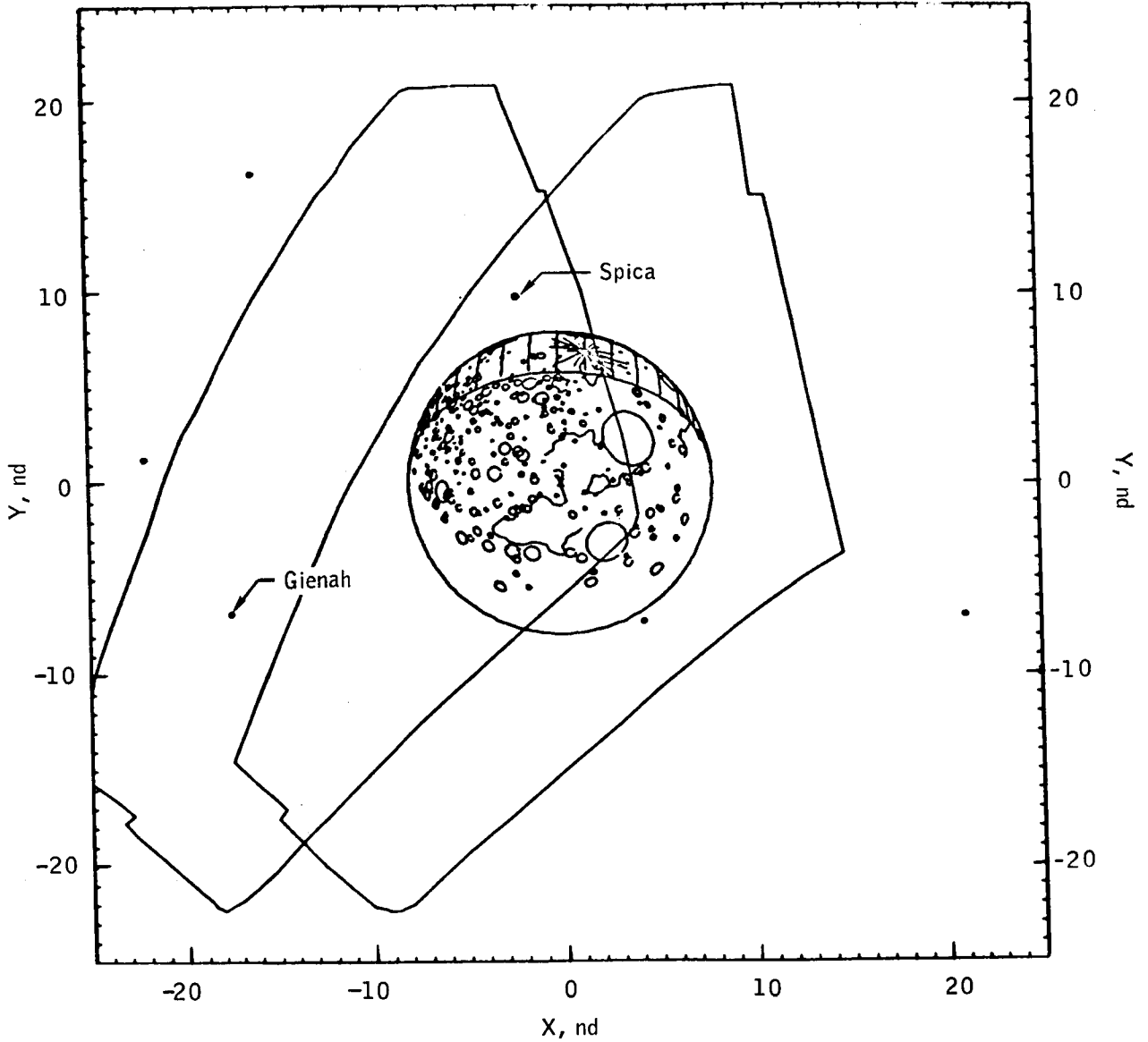
MOON VIEWS

SEQ	551	566	570	582	593	595
X	-17	-21	4	21	-2	-15
Y	-6	1	-7	-6	9	16

$R_M = 8528$  n. mi.  
 $V_i = 5462$  fps

$h_M = 8724$  stat. mi.  
 $V_i = 3724$  mph

Field of view =  $40^\circ$



(a) G.e.t. = 140 hours.

Figure 15.- Transearth coast-constant field of view (moon).

SEG	535	551	566	570	582	593
X	18	-17	-23	3	20	4
Y	-16	2	10	4	6	21

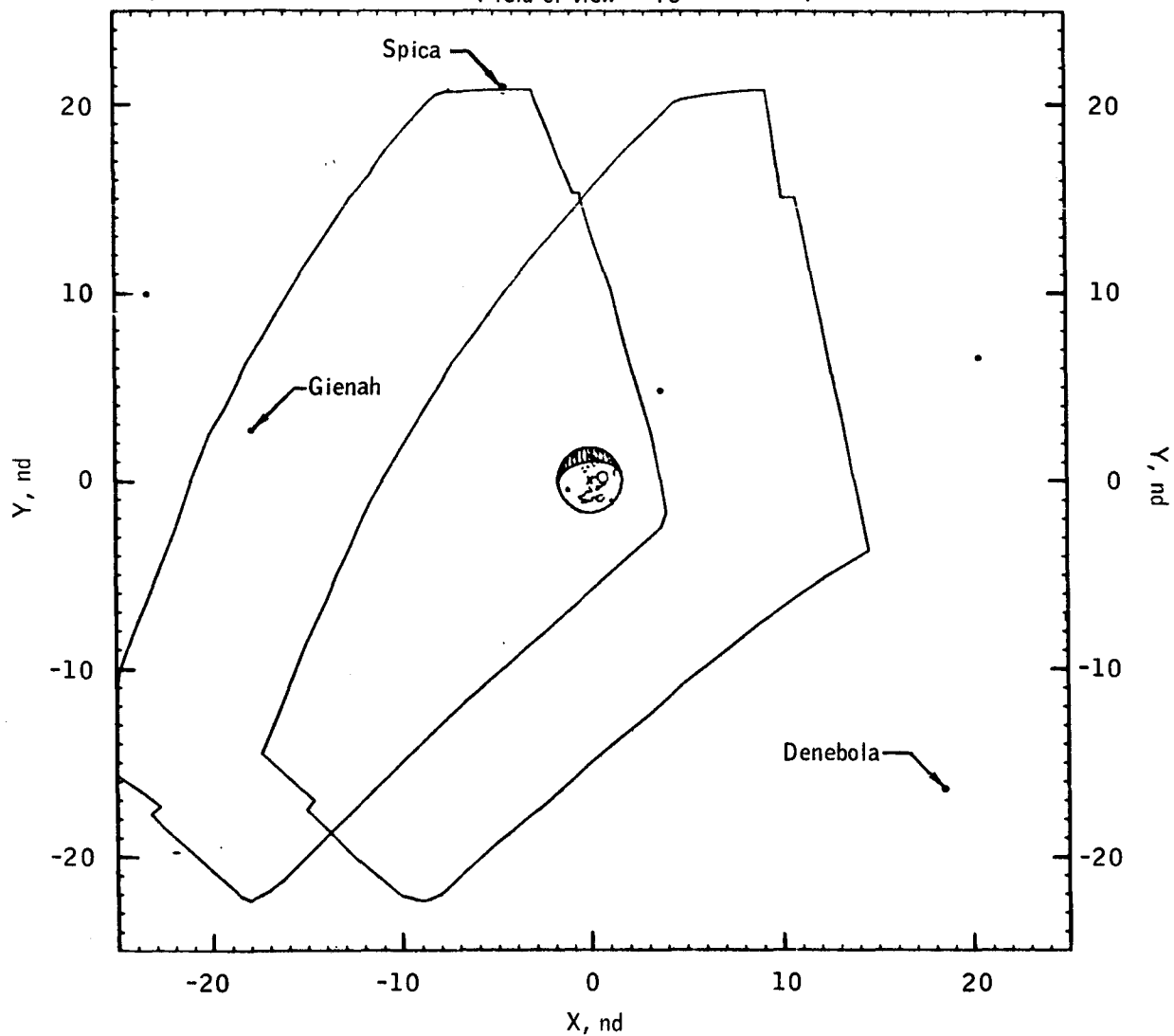
$R_E = 179\,288$  n. mi.

$V_i = 4876$  fps

$h_E = 202\,358$  stat. mi.

$V_i = 3324$  mph

Field of view =  $40^\circ$



(b) G.e.t. = 150 hours.

Figure 15.- Continued.

SEG	535	551	566	570	582	593
X	16	-17	-22	4	20	-2
Y	-15	6	14	6	6	23

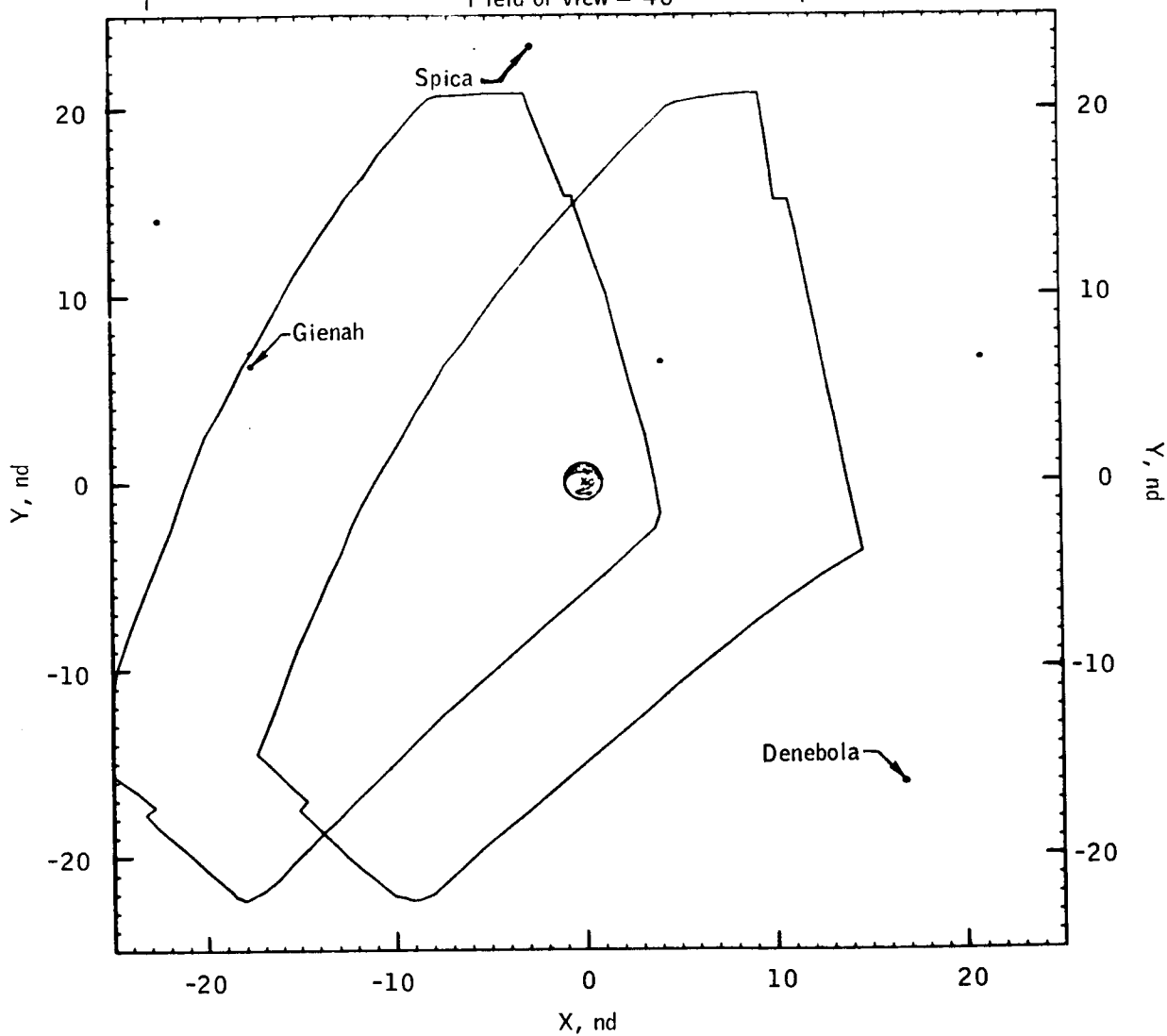
$R_E = 149\,473$  n. mi.

$h_E = 168\,046$  stat. mi.

$V_i = 5338$  fps

Field of view =  $40^\circ$

$V_i = 3640$  mph



(c) G.e.t. = 160 hours.

Figure 15.- Continued.

SEQ	535	551	566	570	582
X	15	-17	-21	4	21
Y	-15	9	17	7	7

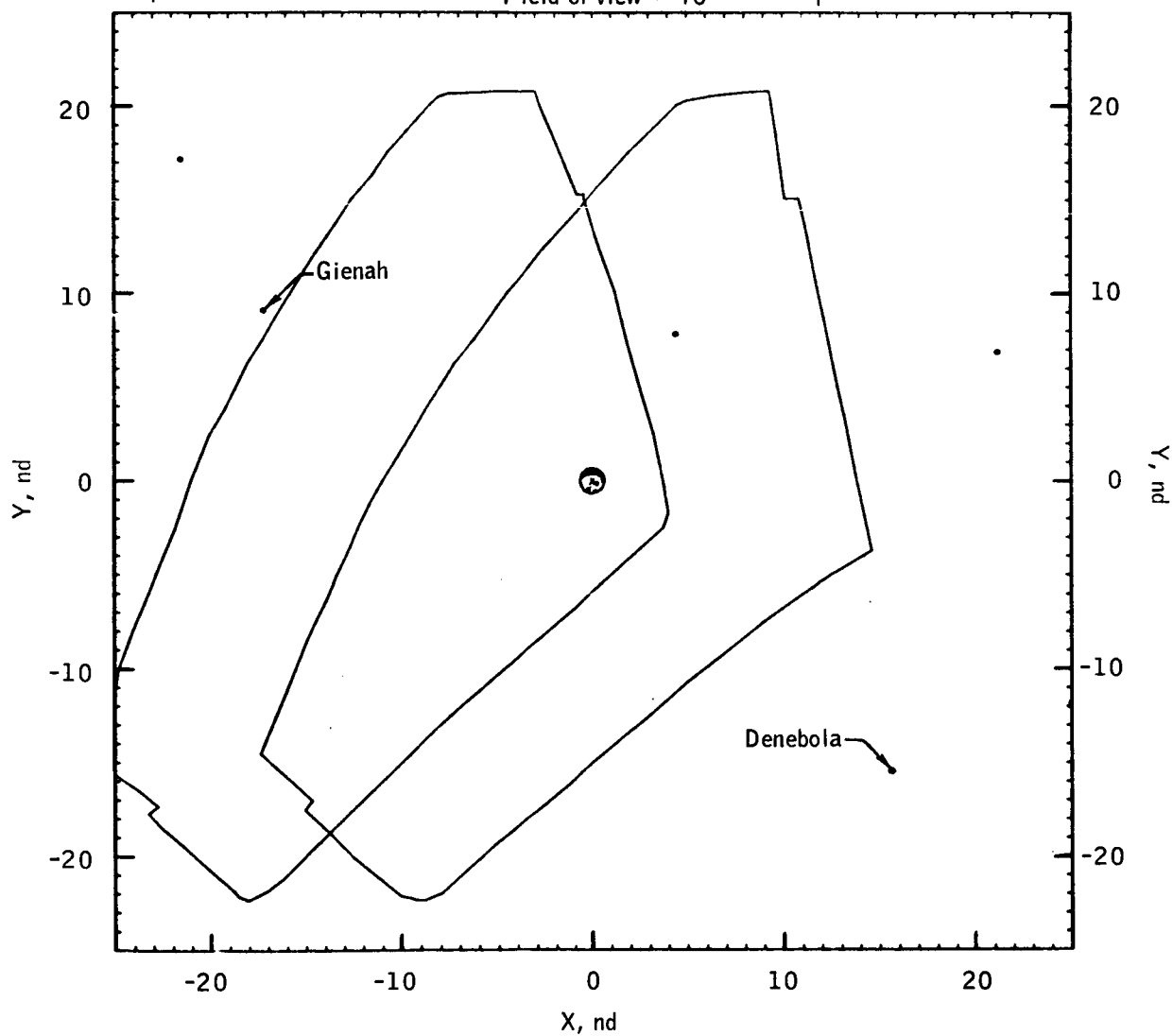
$R_E = 116\,265$  n. mi.

$h_E = 129\,832$  stat. mi.

$V_i = 6097$  fps

$V_i = 4157$  mph

Field of view =  $40^\circ$



(d) G.e.t. = 170 hours.

Figure 15.- Continued.

SEC	535	551	566	570	582
X	14	-16	-20	4	21
Y	-13	12	20	9	8

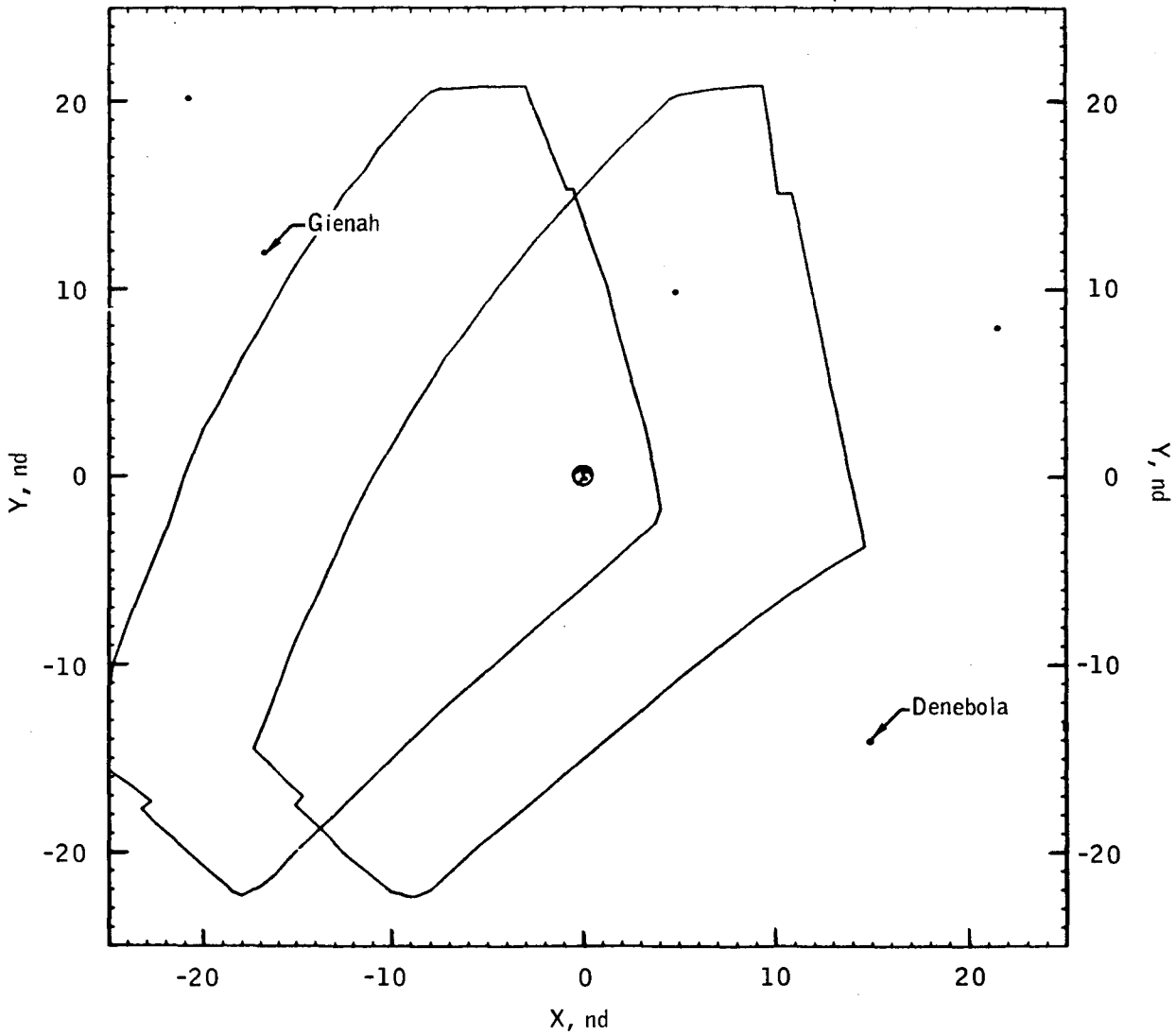
$R_E = 77\,138$  n. mi.

$h_E = 84\,807$  stat. mi.

$V_i = 7571$  fps

$V_i = 5162$  mph

Field of view =  $40^\circ$



(e) G.e.t. = 180 hours.

Figure 15.- Continued.

SEG	515	535	551	566	570	5A2
X	15	14	-16	-20	5	21
Y	-24	-11	15	23	12	10

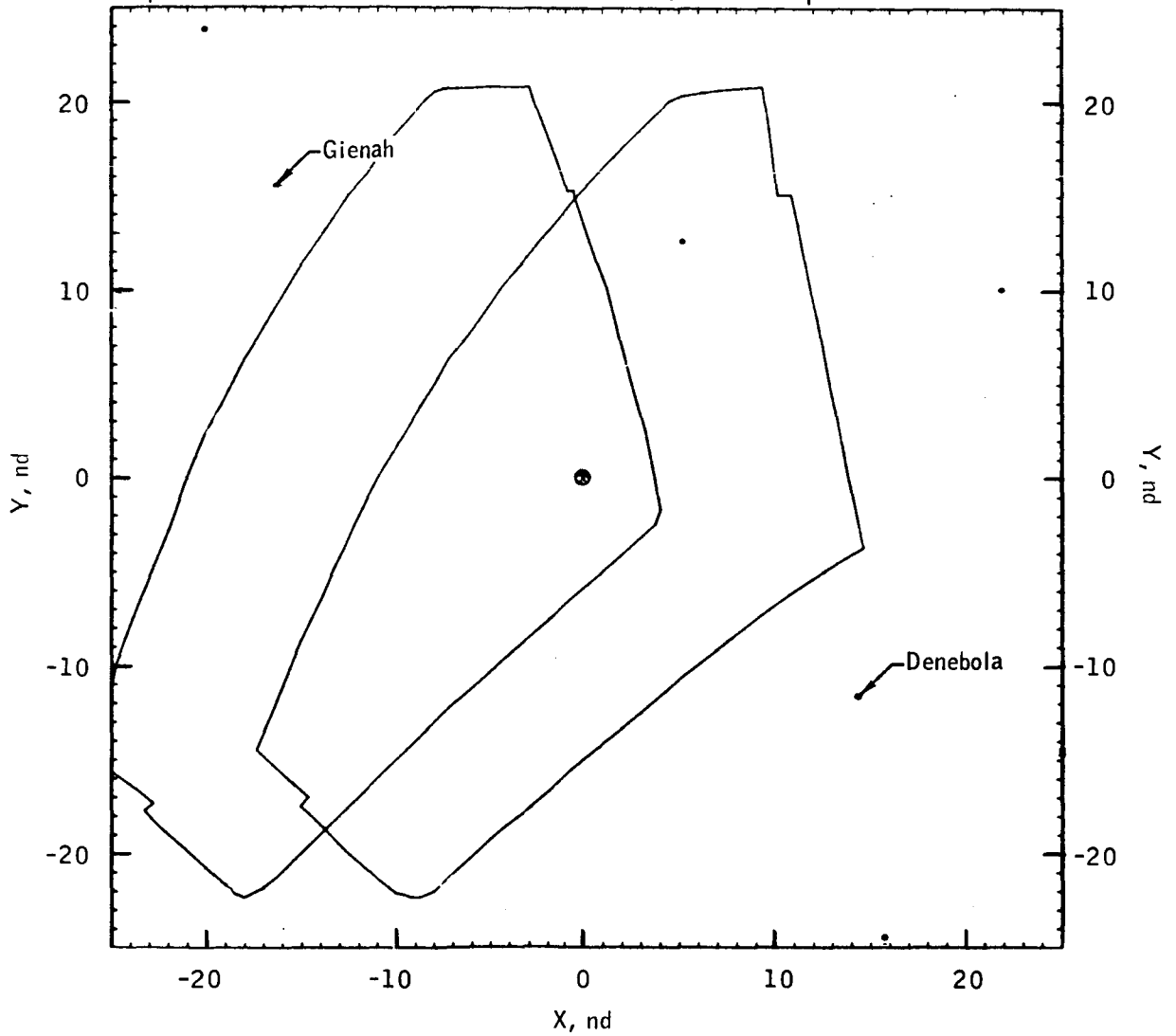
$R_E = 22\,296$  n. mi.

$h_M = 25\,658$  stat. mi.

$V_i = 14\,318$  fps

Field of view =  $40^\circ$

$V_i = 9762$  mph



(f) G.e.t. = 190 hours.

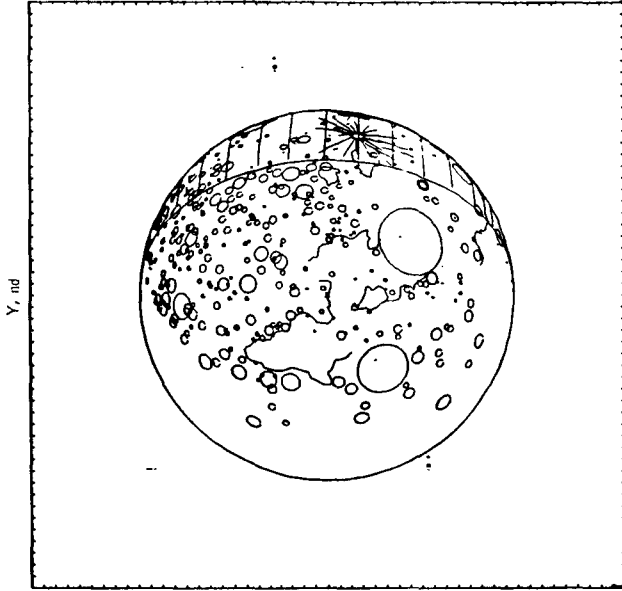
Figure 15.- Concluded.



$R_M = 8528$  n. mi.  
 $V_i = 5462$  fps

$h_M = 8734$  stat. mi.  
 $V_i = 3724$  mph

Field of view =  $20^\circ$



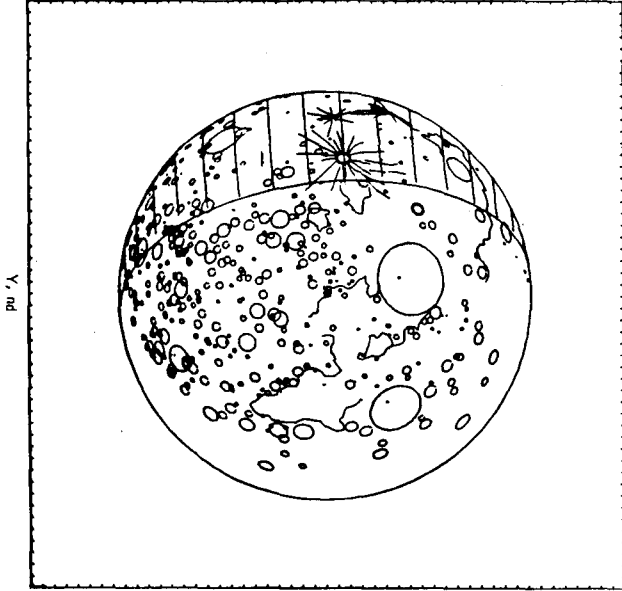
X, nd

(a) G.e.t. = 140 hours.

$R_E = 179\ 288$  n. mi.  
 $V_i = 4876$  fps

$h_E = 202\ 358$  stat. mi.  
 $V_i = 3324$  mph

Field of view =  $4^\circ$



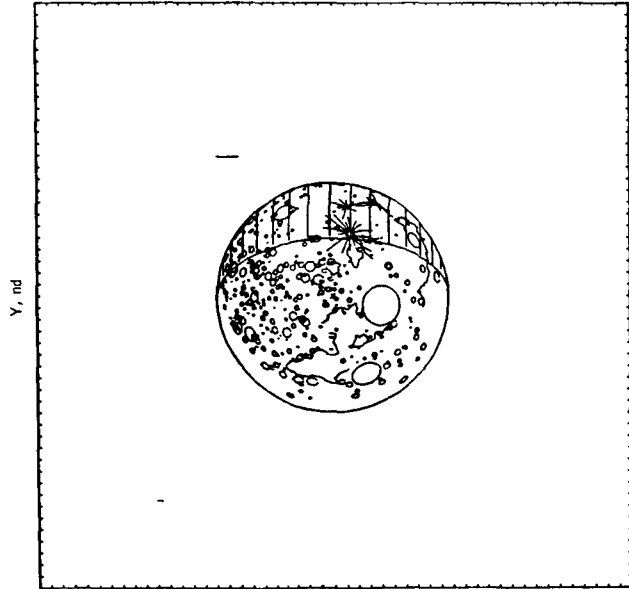
X, nd

(b) G.e.t. = 150 hours.

$R_E = 149\ 473$  n. mi.  
 $V_i = 5338$  fps

$h_E = 168\ 046$  stat. mi.  
 $V_i = 3640$  mph

Field of view =  $4^\circ$



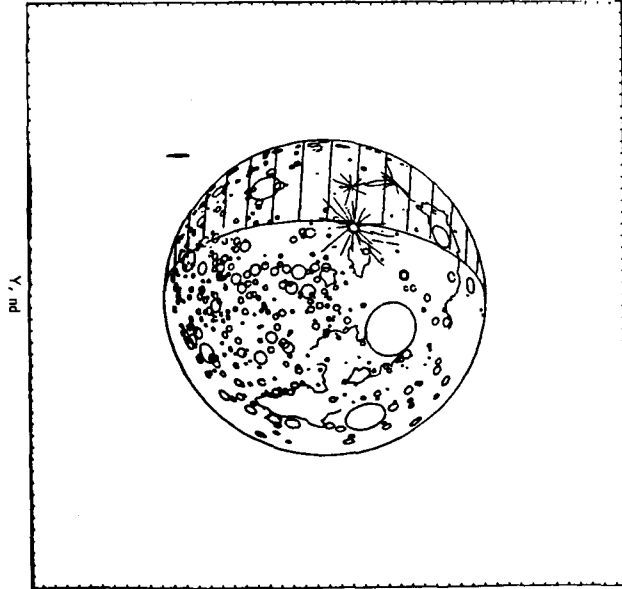
X, nd

(c) G.e.t. = 160 hours.

$R_E = 116\ 265$  n. mi.  
 $V_i = 6097$  fps

$h_E = 129\ 832$  stat. mi.  
 $V_i = 4157$  mph

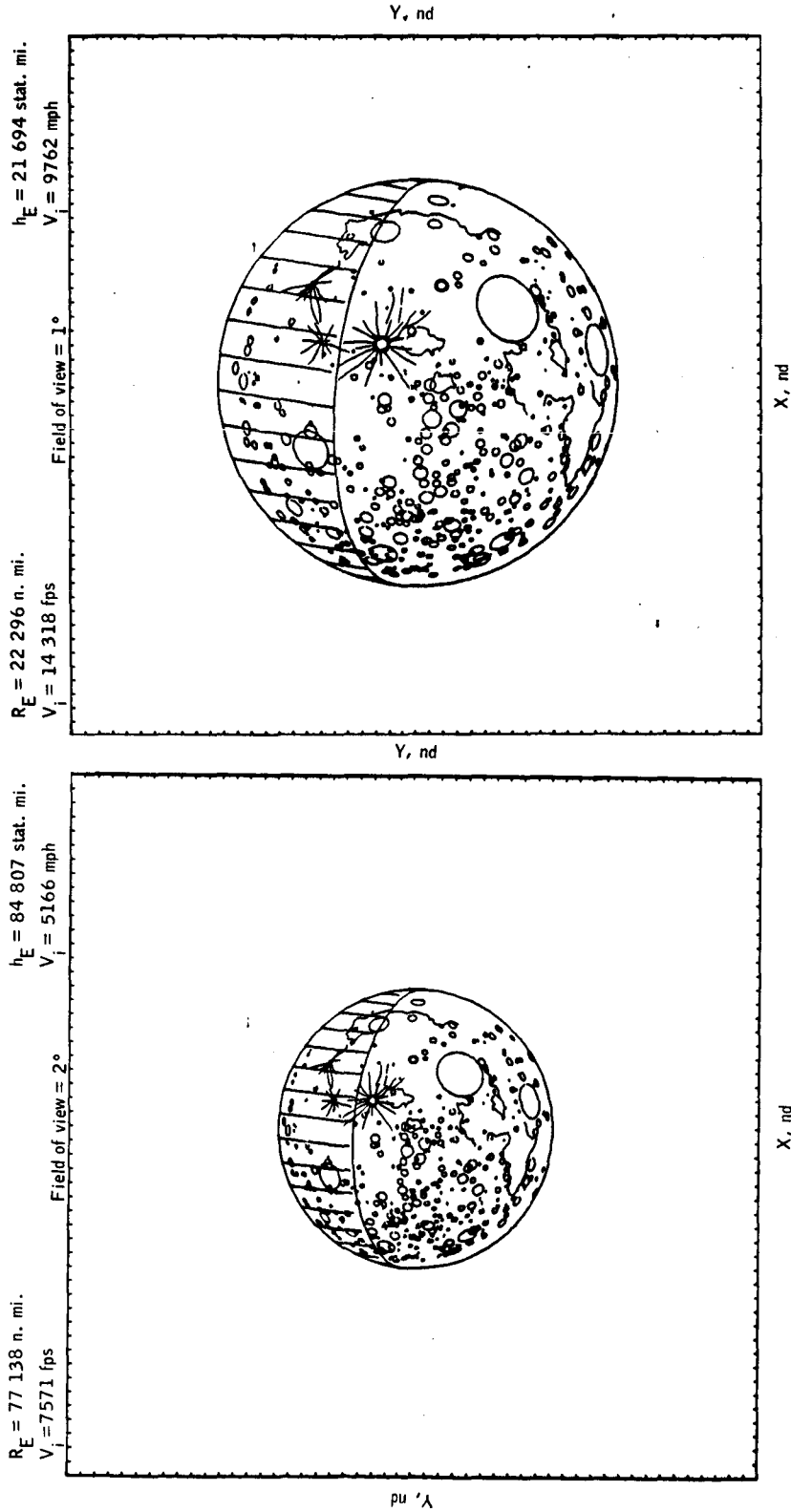
Field of view =  $2^\circ$



X, nd

(d) G.e.t. = 170 hours.

Figure 16. - Transearth coast variable field of view (moon).



(f) G.e.t. = 190 hours.

Figure 16.- Concluded.

(e) G.e.t. = 180 hours.



SLW 990 1041  
 X 0 23  
 Y 12 0

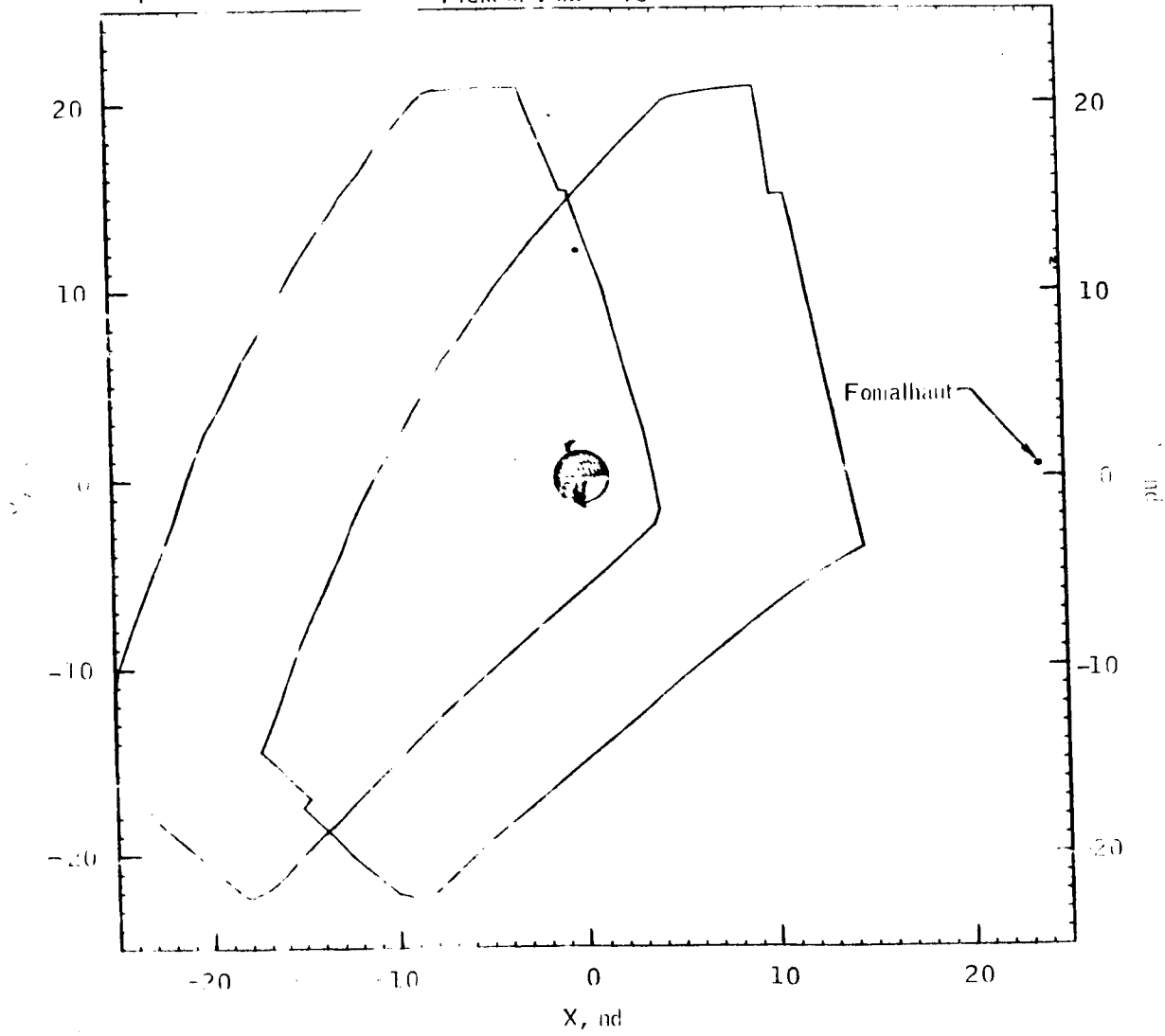
$R_E = 179\,288$  n. mi.

$V_i = 4876$  fps

$h_E = 202\,358$  stat. mi.

$V_i = 3324$  mph

Field of view =  $40^\circ$



) G.e.t. = 150 hours.

Figure 17. Transearth coast-constant field of view (earth).

SEQ 990 1091  
 X 0 23  
 Y 14 2

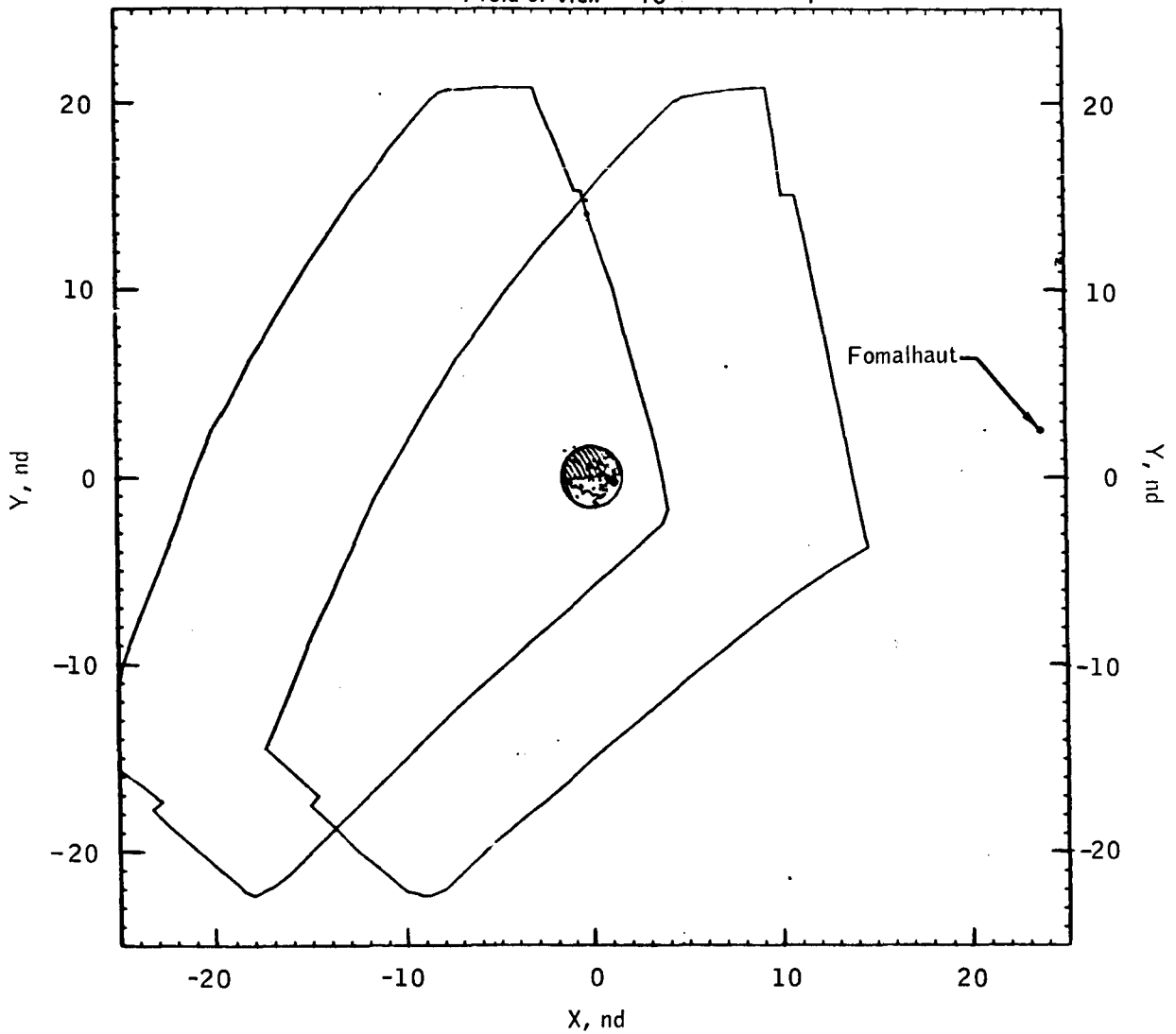
$R_E = 149\,473$  n. mi.

$V_i = 5338$  fps

$h_E = 168\,046$  stat. mi.

$V_i = 3640$  mph

Field of view =  $40^\circ$



(b) G.e.t. = 160 hours.

Figure 17.- Continued.

SEQ 990 1091  
 X 0 23  
 Y 17 5

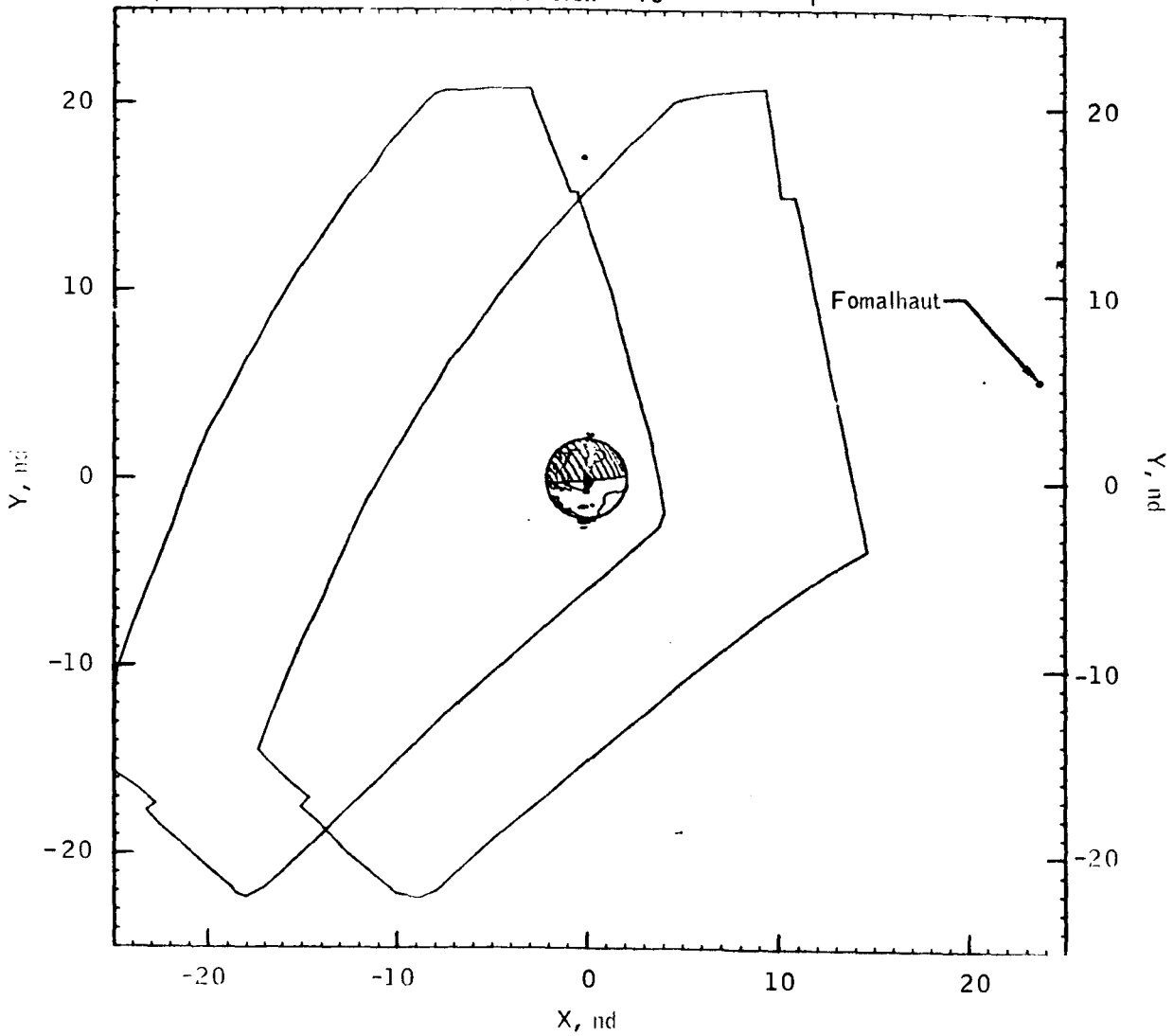
$R_E = 116\,265$  n. mi.

$V_i = 6097$  fps

$h_E = 129\,832$  stat. mi.

$V_i = 4157$  mph

Field of view =  $40^\circ$



(c) G.e.t. = 170 hours.

Figure 17.- Continued.

SEQ 990 1041  
 X U 23  
 Y 23 11

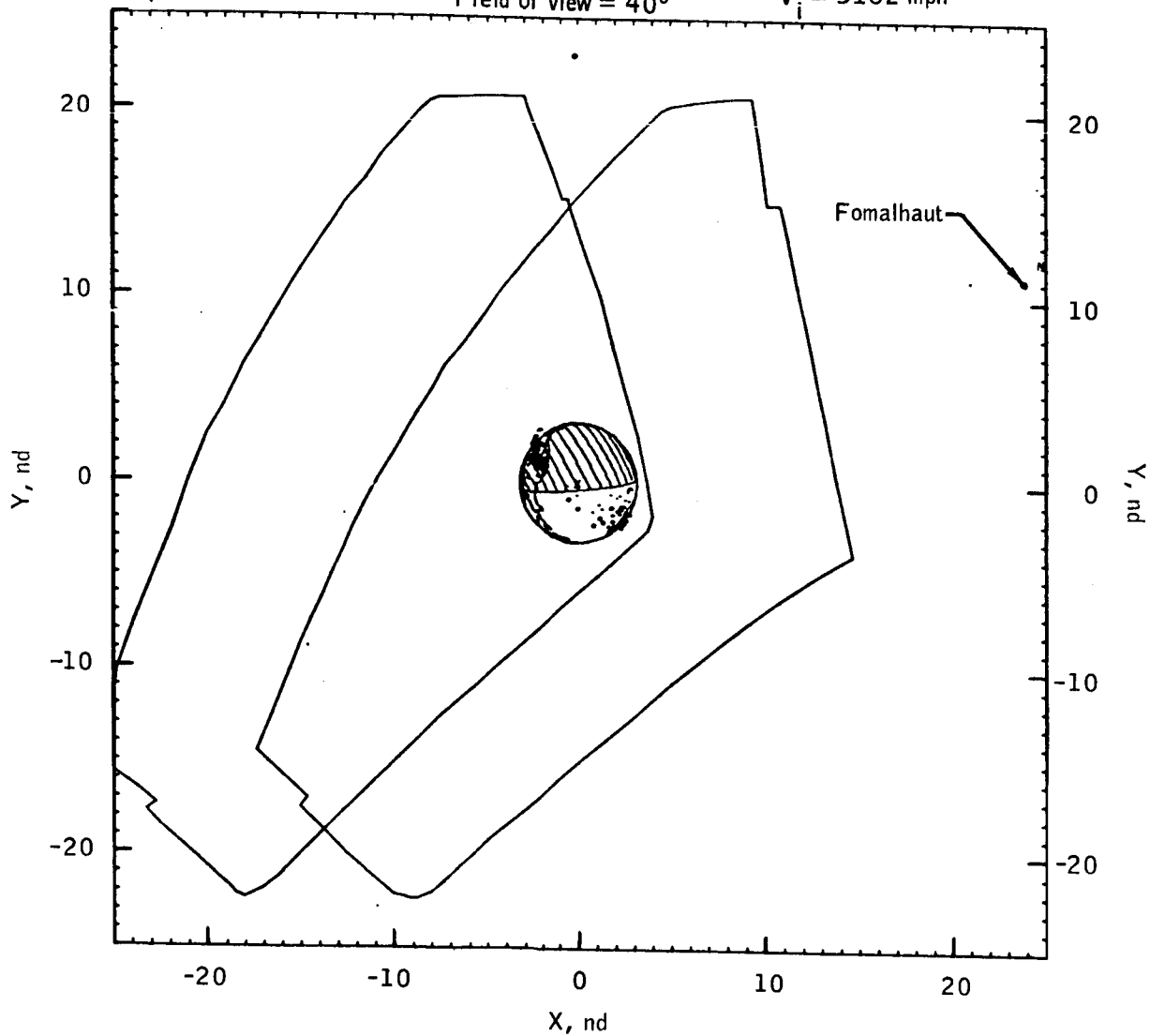
$R_E = 77\,138$  n. mi.

$V_i = 7571$  fps

$h_E = 84\,807$  stat. mi.

$V_i = 5162$  mph

Field of view =  $40^\circ$



(d) G.e.t. = 180 hours.

Figure 17.- Continued.

Seq 7 117  
 X -15 2  
 Y -7 -18

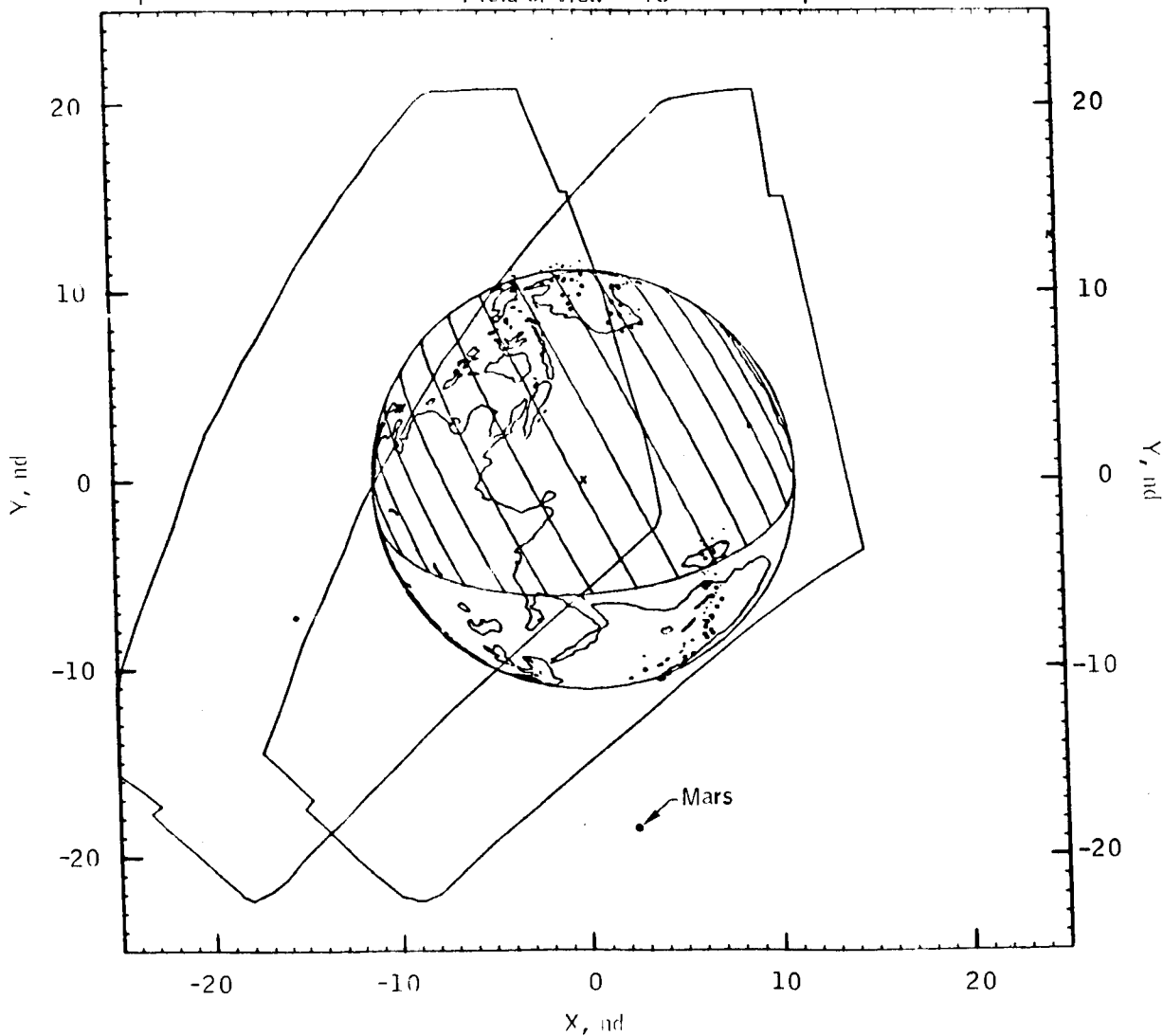
$R_E = 22\,296$  n. mi.

$h_E = 25\,658$  stat. mi.

$V_i = 14\,318$  fps

$V_i = 9762$  mph

Field of view =  $40^\circ$



(e) G.c.t. = 190 hours.

Figure 17.- Concluded.



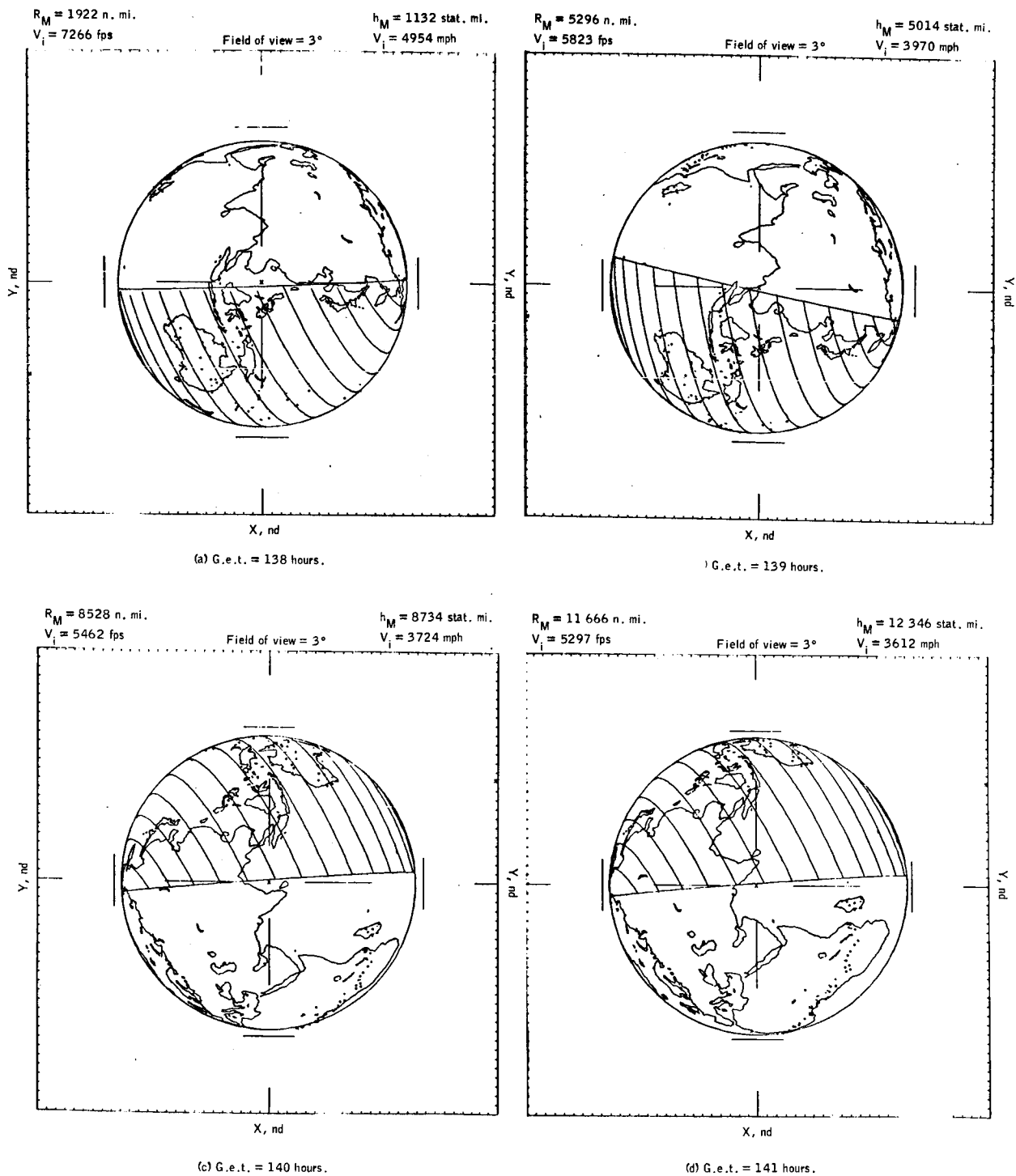


Figure 18. - Transearth coast - variable field of view (earth).

$R_M = 14\ 747$  n. mi.  
 $V_i = 5202$  fps

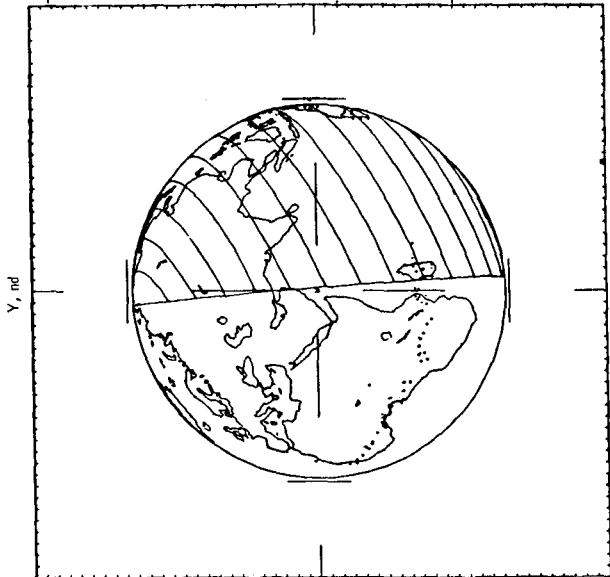
Field of view =  $3^\circ$

$h_M = 15\ 891$  stat. mi.  
 $V_i = 3547$  mph

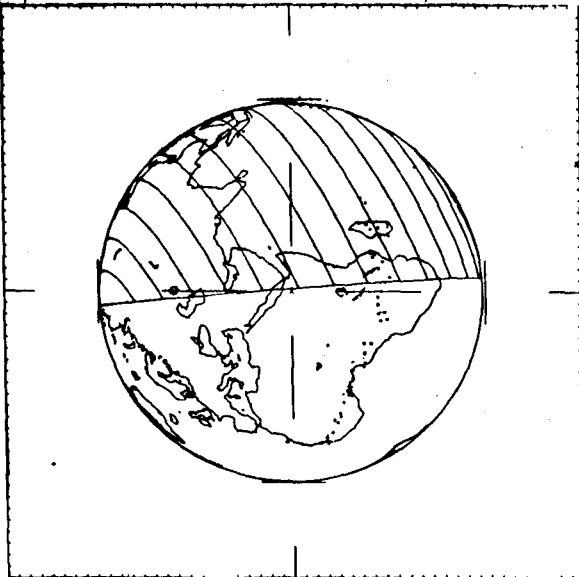
$R_M = 17\ 792$  n. mi.  
 $V_i = 5140$  fps

Field of view =  $3^\circ$

$h_M = 19\ 394$  stat. mi.  
 $V_i = 3505$  mph



(e) G.e.t. = 142 hours.



(f) G.e.t. = 143 hours.

$R_M = 20\ 812$  n. mi.  
 $V_i = 5098$  fps

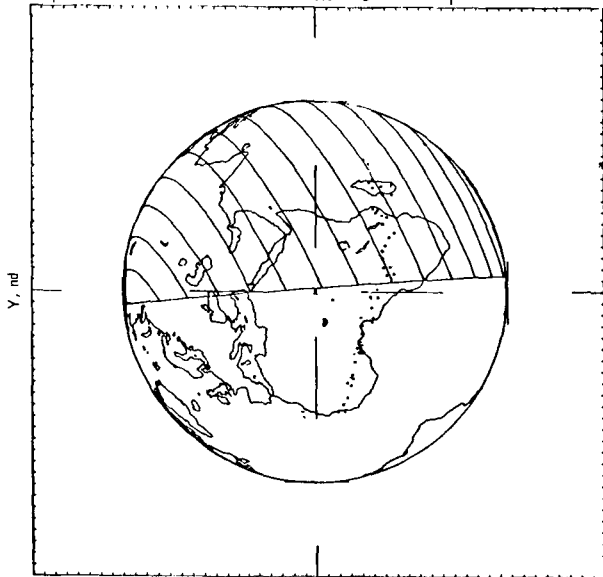
Field of view =  $3^\circ$

$h_M = 22\ 869$  stat. mi.  
 $V_i = 3476$  mph

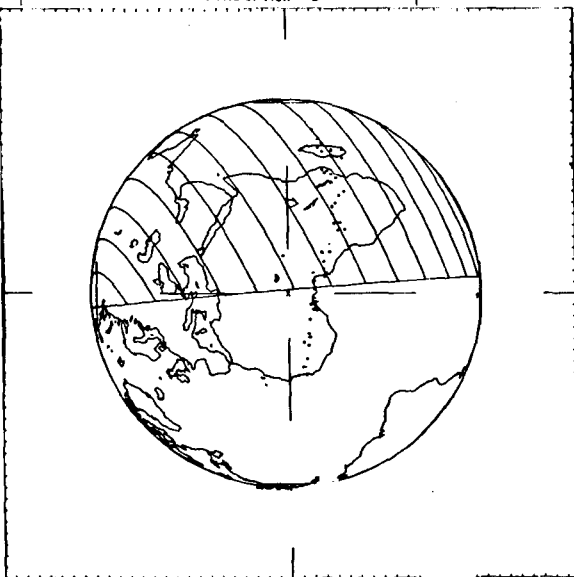
$R_M = 23\ 813$  n. mi.  
 $V_i = 5068$  fps

Field of view =  $3^\circ$

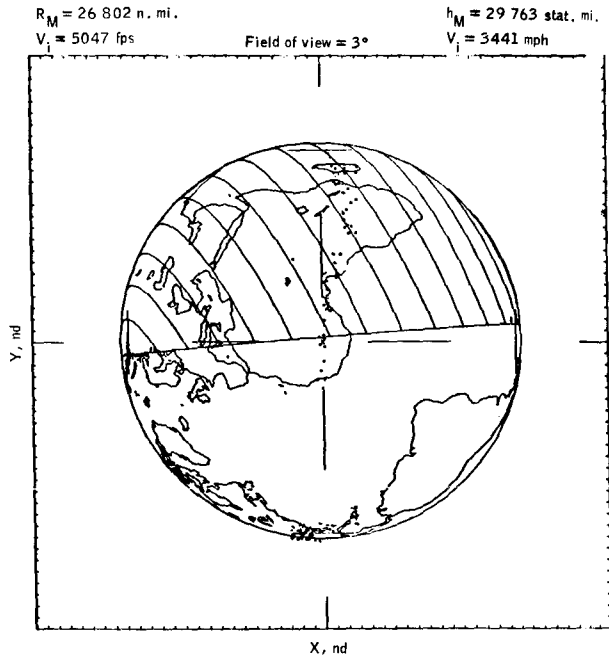
$h_M = 26\ 324$  stat. mi.  
 $V_i = 3455$  mph



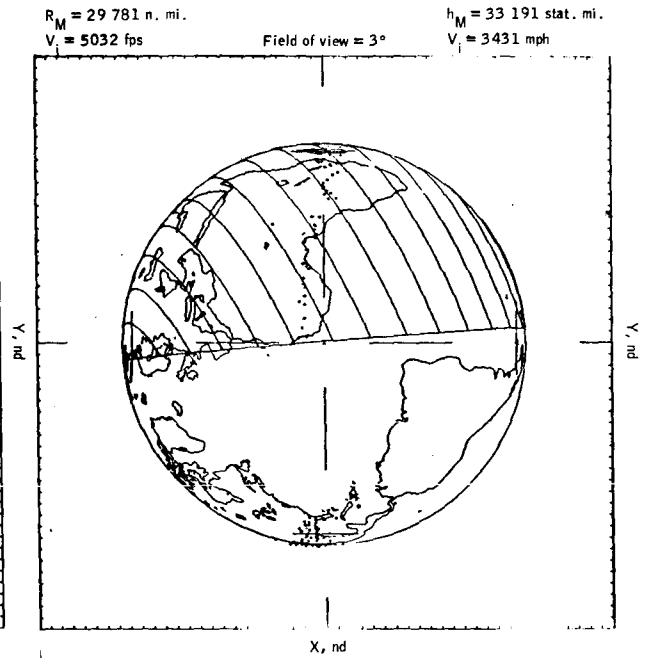
(g) G.e.t. = 144 hours.



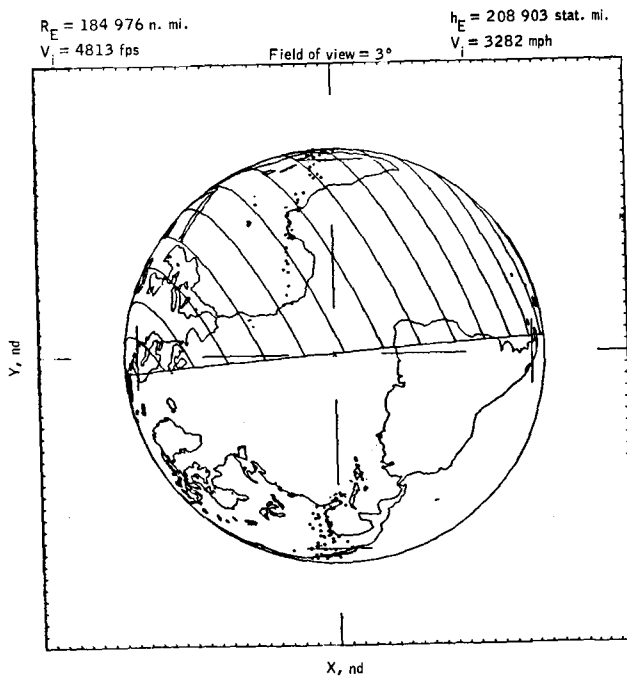
(h) G.e.t. = 145 hours.



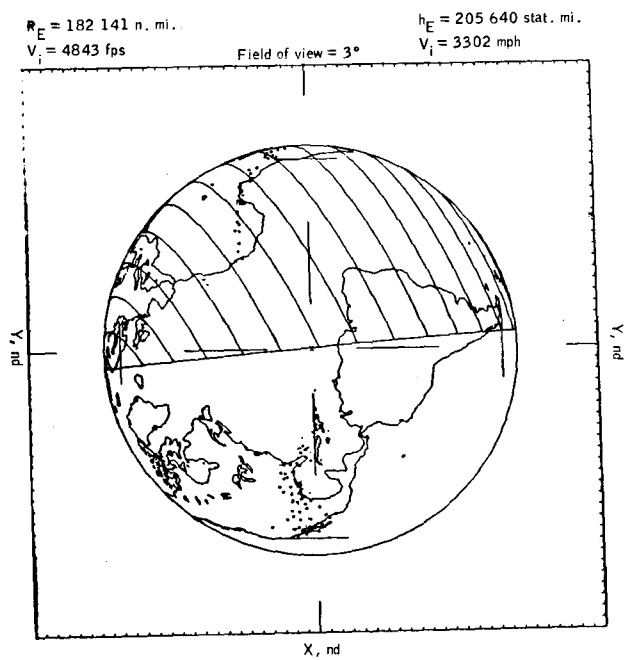
(i) G.e.t. = 146 hours.



(j) G.e.t. = 147 hours.



(k) G.e.t. = 148 hours.

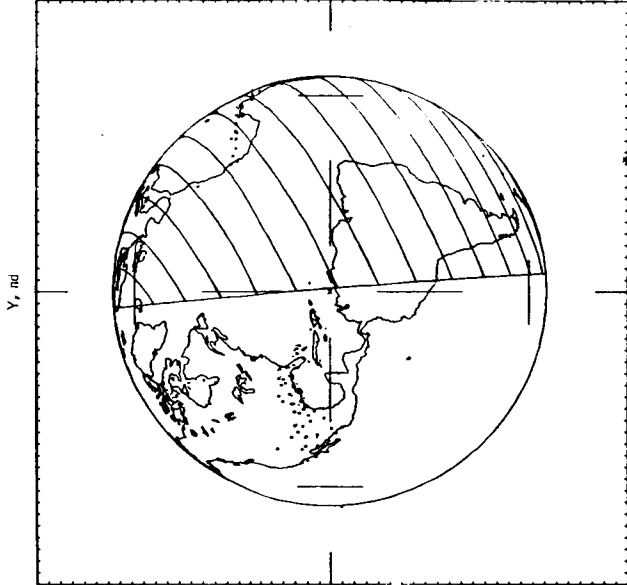


(l) G.e.t. = 149 hours.

Figure 18.- Continued.

$R_E = 179\ 288$  n. mi.  $h_E = 202\ 358$  stat. mi.  
 $V_i = 4876$  fps  $V_i = 3\ 724$  mph

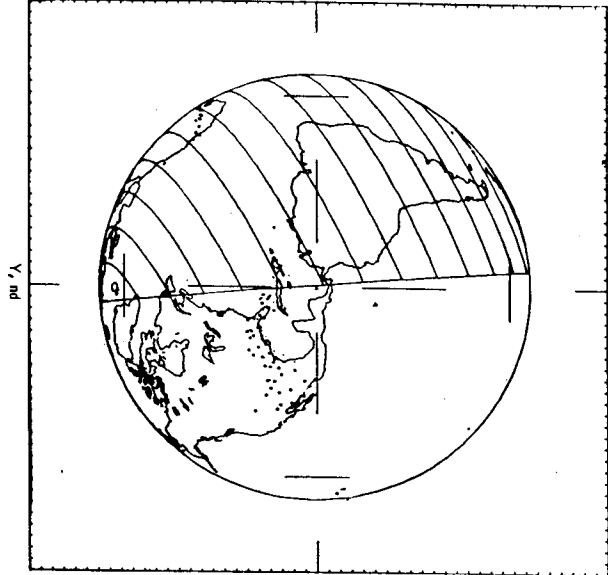
Field of view =  $3^\circ$



(m) G.e.t. = 150 hours.

$R_E = 176\ 416$  n. mi.  $h_E = 199\ 053$  stat. mi.  
 $V_i = 4911$  fps  $V_i = 3\ 348$  mph

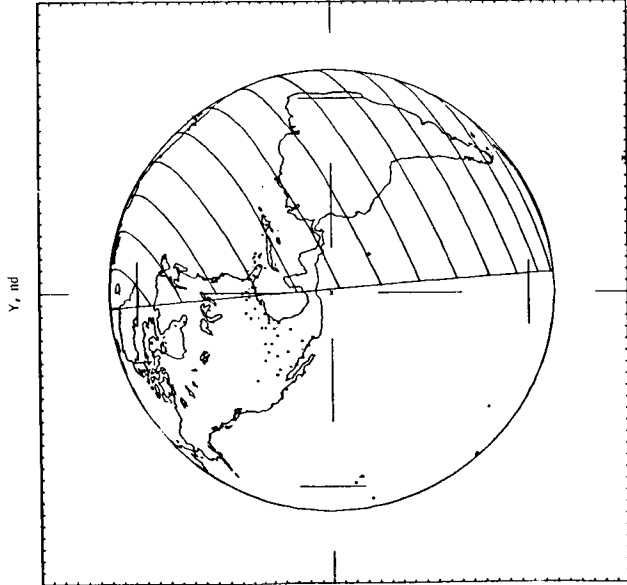
Field of view =  $3^\circ$



(n) G.e.t. = 151 hours.

$R_E = 173\ 523$  n. mi.  $h_E = 195\ 724$  stat. mi.  
 $V_i = 4949$  fps  $V_i = 3\ 374$  mph

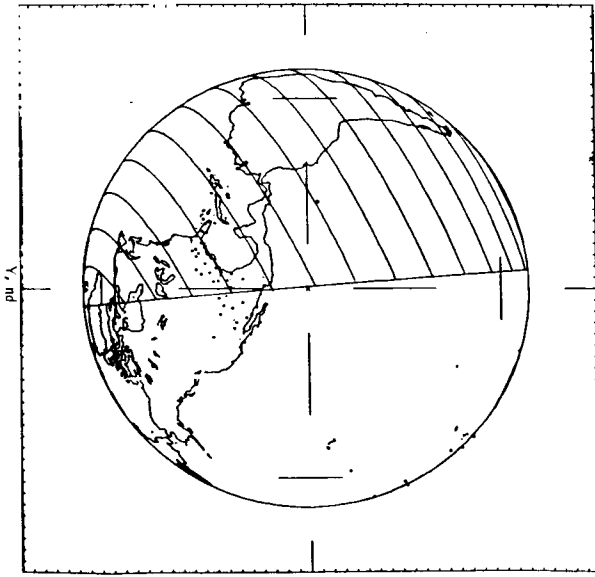
Field of view =  $3^\circ$



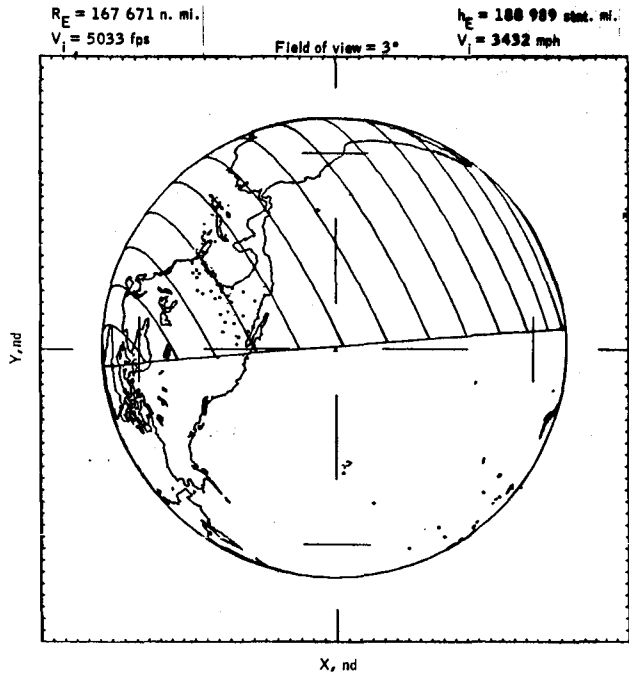
(o) G.e.t. = 152 hours.

$R_E = 170\ 609$  n. mi.  $h_E = 192\ 370$  stat. mi.  
 $V_i = 4990$  fps  $V_i = 3\ 402$  mph

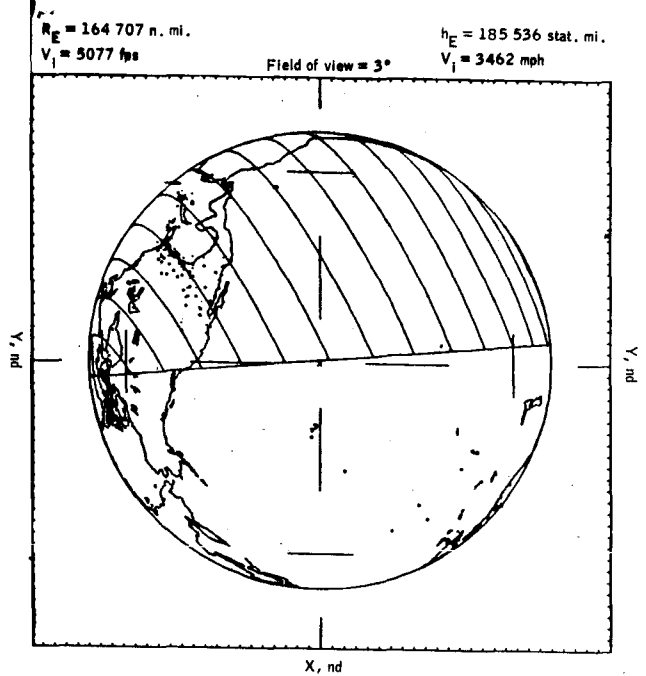
Field of view =  $3^\circ$



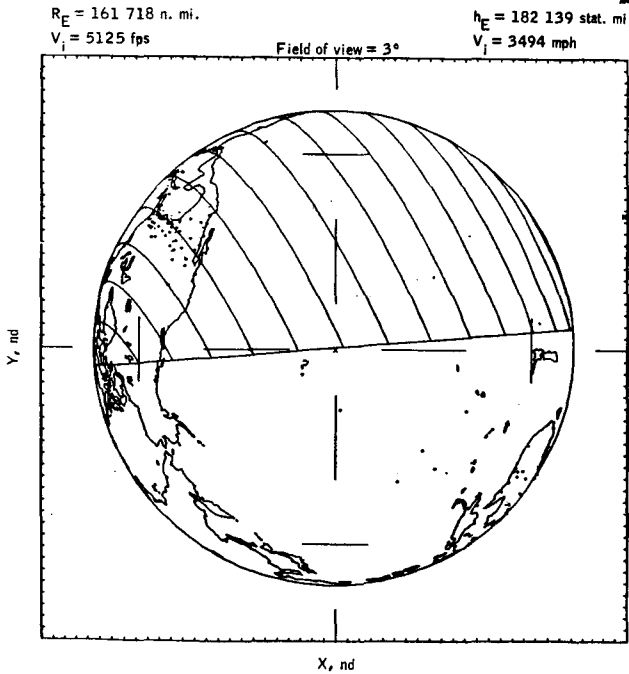
(p) G.e.t. = 153 hours.



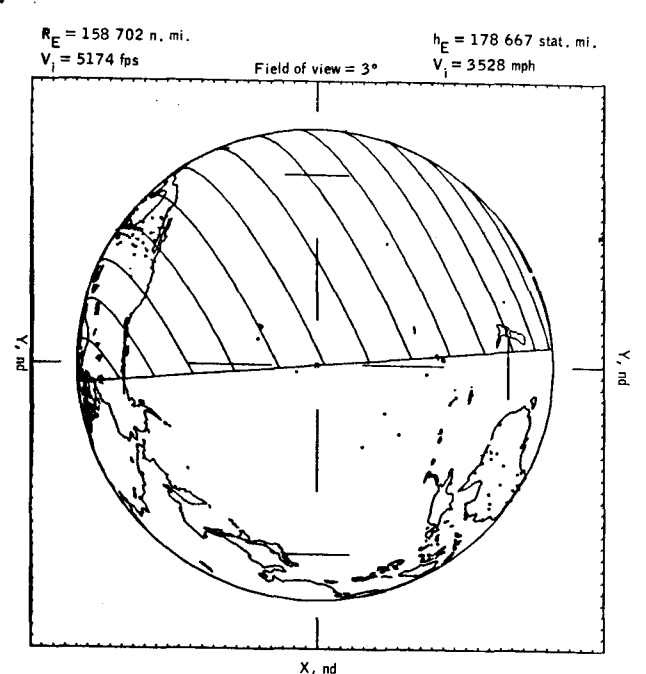
(q) G.e.t. = 154 hours.



(r) G.e.t. = 155 hours.



(s) G.e.t. = 156 hours.

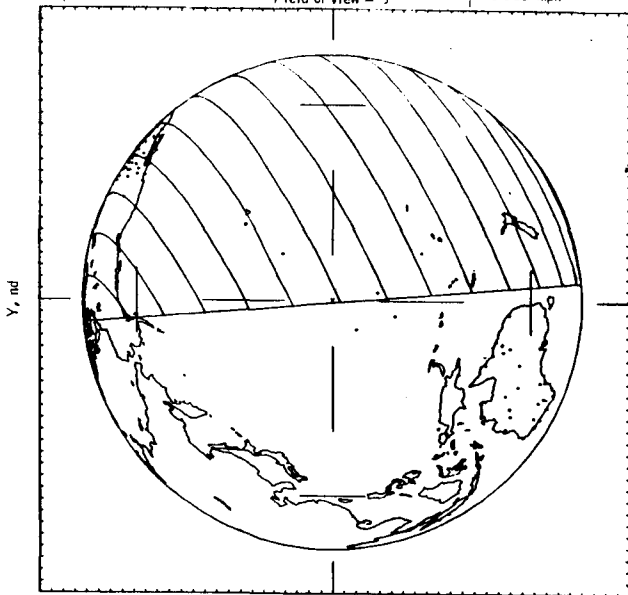


(t) G.e.t. = 157 hours.

Figure 18.- Continued.

$R_E = 155\ 656$  n. mi.  $h_E = 175\ 163$  stat. mi.,  
 $V_i = 5226$  fps  $V_i = 3563$  mph

Field of view =  $3^\circ$

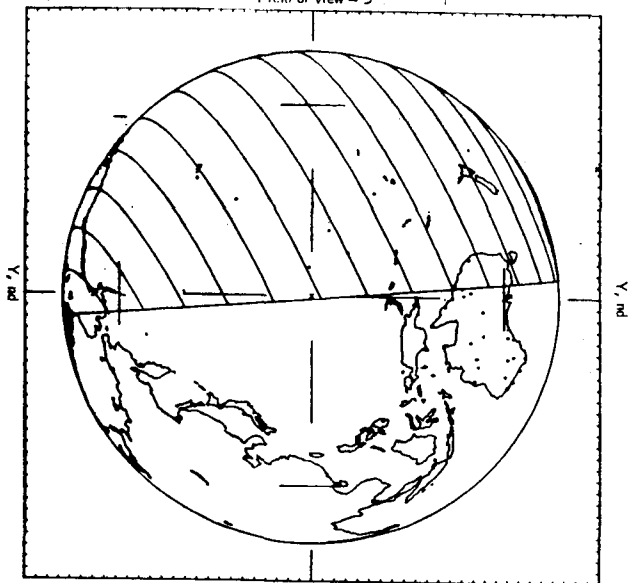


X, nd

(u) G.e.t. = 158 hours.

$R_E = 152\ 580$  n. mi.  $h_E = 175\ 163$  stat. mi.,  
 $V_i = 5280$  fps  $V_i = 3600$  mph

Field of view =  $3^\circ$

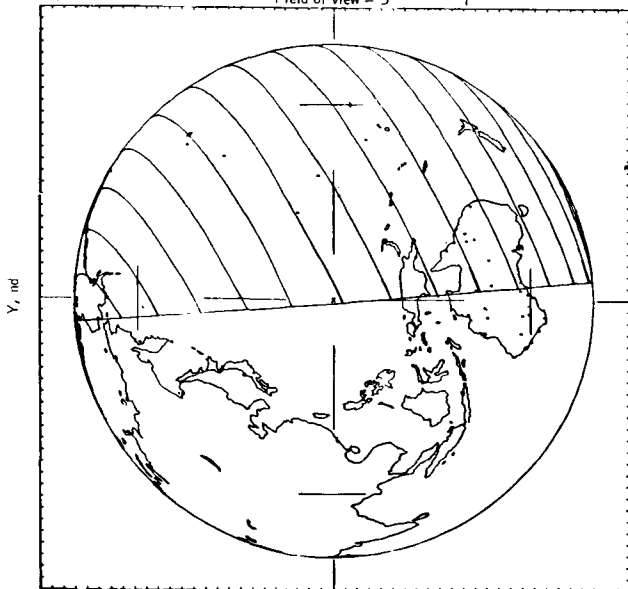


X, nd

(v) G.e.t. = 159 hours.

$R_E = 149\ 473$  n. mi.  $h_E = 168\ 046$  stat. mi.,  
 $V_i = 5338$  fps  $V_i = 3640$  mph

Field of view =  $3^\circ$

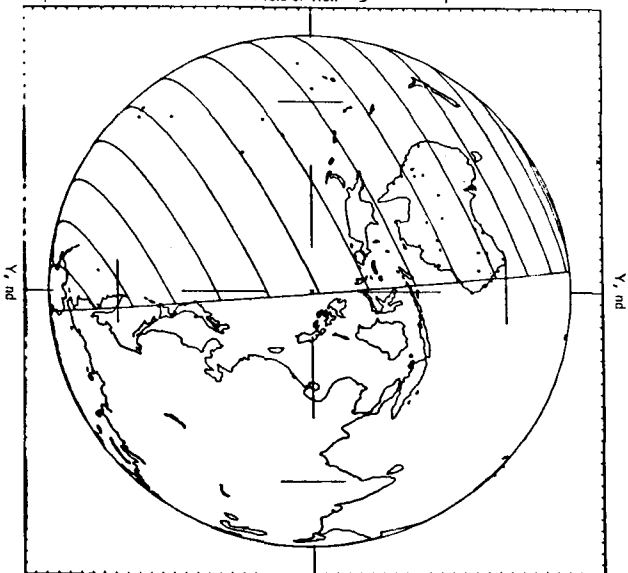


X, nd

(w) G.e.t. = 160 hours.

$R_E = 146\ 332$  n. mi.  $h_E = 164\ 433$  stat. mi.,  
 $V_i = 5398$  fps  $V_i = 3680$  mph

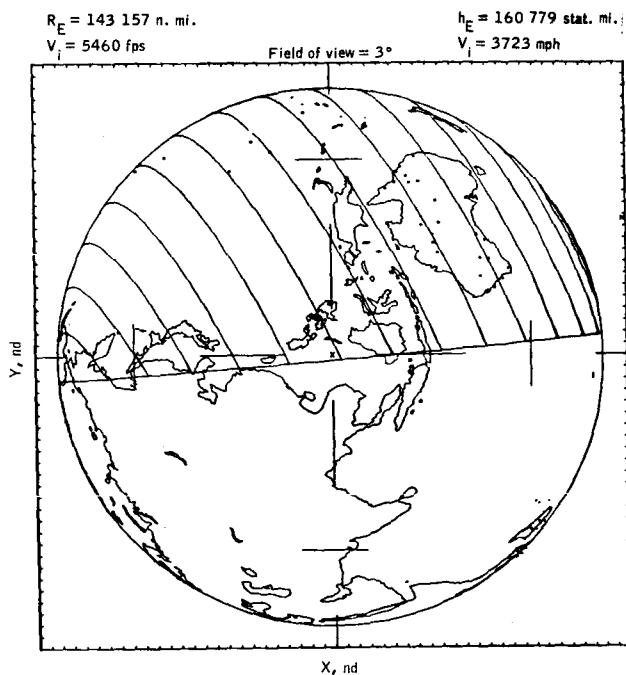
Field of view =  $3^\circ$



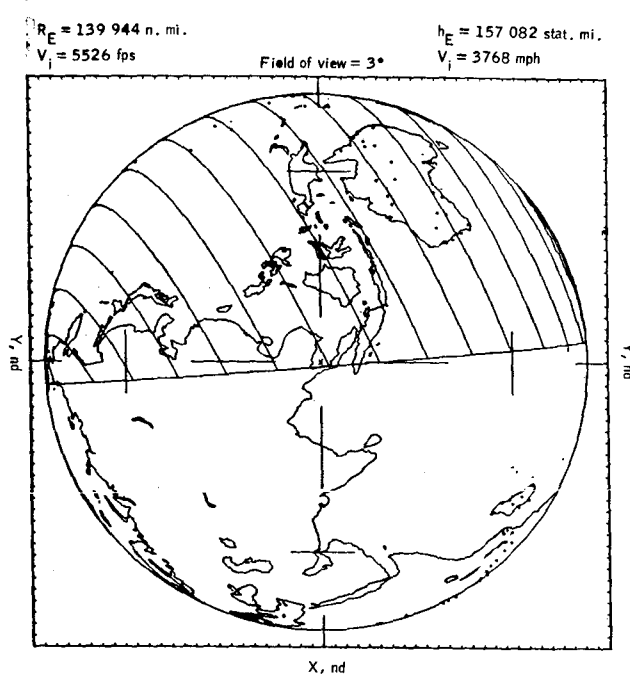
X, nd

(x) G.e.t. = 161 hours.

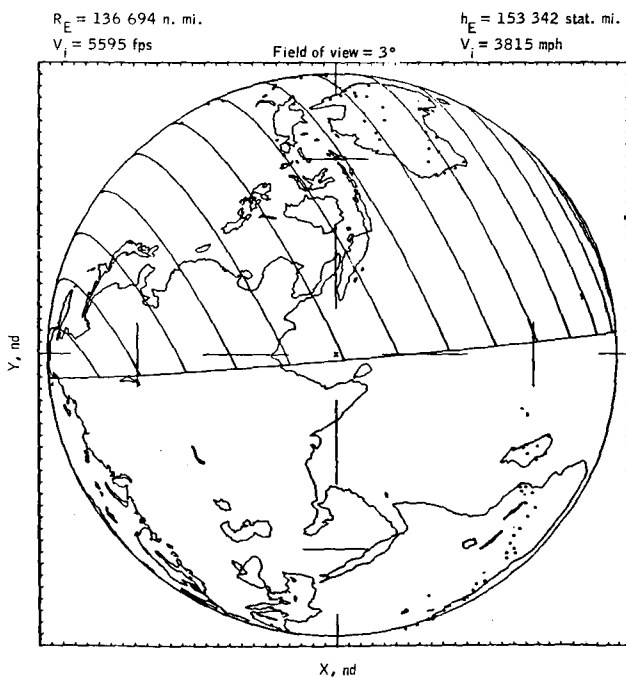
Figure 18.- Continued.



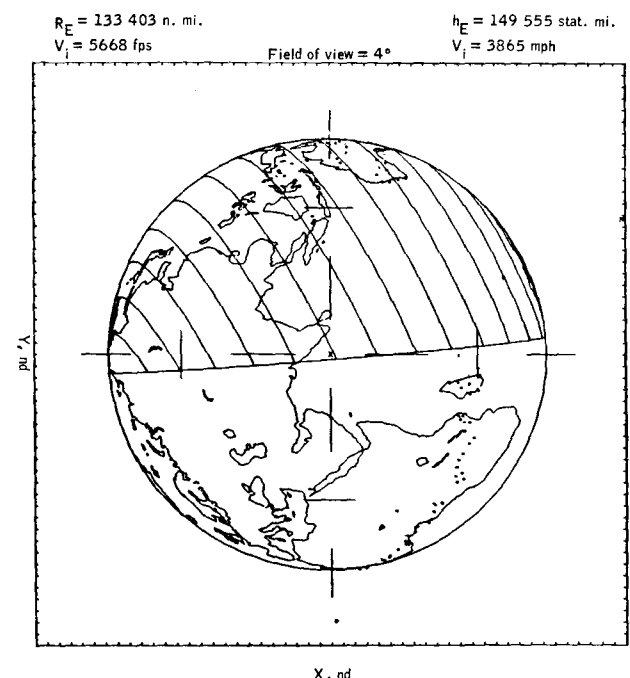
(y) G.e.t. = 162 hours.



(z) G.e.t. = 163 hours.



(aa) G.e.t. = 164 hours.

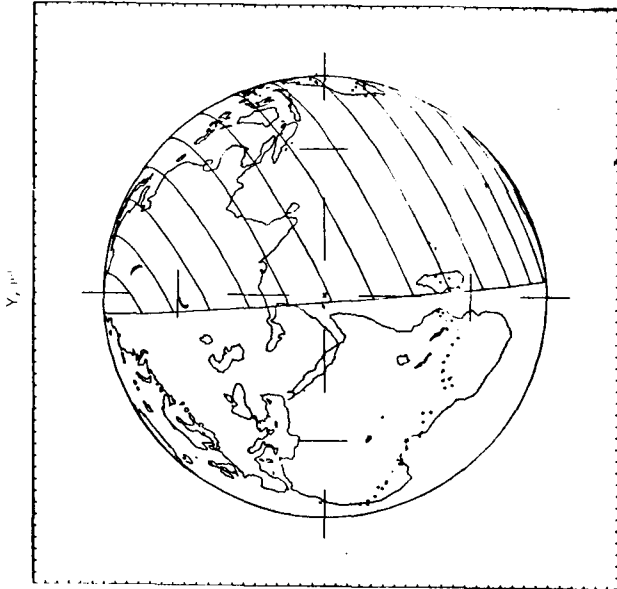


(bb) G.e.t. = 165 hours.

$R_E = 130\ 070$  n. mi.  
 $V_i = 5744$  fps

$h_E = 145\ 719$  stat. mi.  
 $V_i = 3916$  mph

Field of view =  $4^\circ$



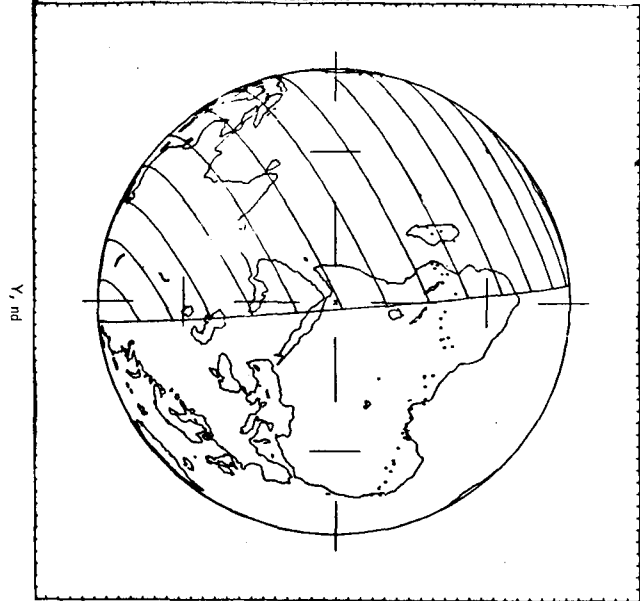
X, nd

(cc) G.e.t. = 166 hours.

$R_E = 126\ 692$  n. mi.  
 $V_i = 5825$  fps

$h_E = 141\ 832$  stat. mi.  
 $V_i = 3972$  mph

Field of view =  $4^\circ$



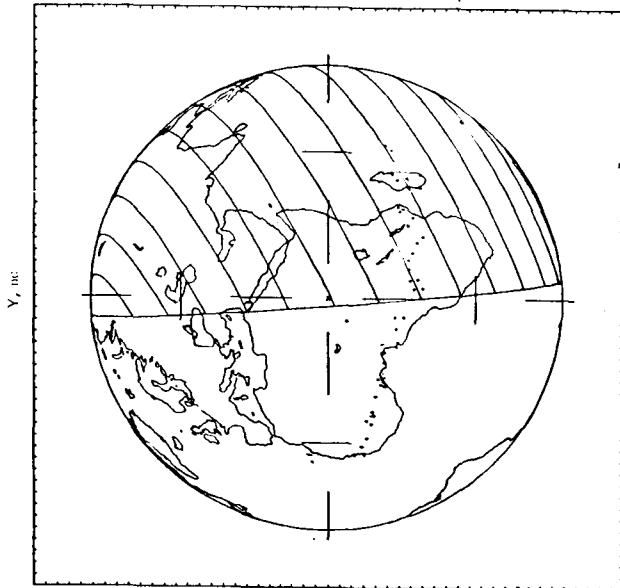
X, nd

(dd) G.e.t. = 167 hours.

$R_E = 123\ 267$  n. mi.  
 $V_i = 5911$  fps

$h_E = 137\ 891$  stat. mi.  
 $V_i = 4030$  mph

Field of view =  $4^\circ$



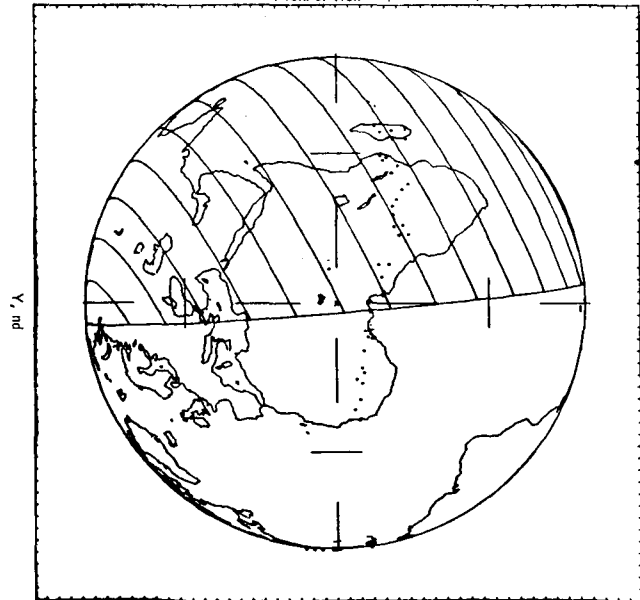
X, nd

(ee) G.e.t. = 168 hours.

$R_E = 119\ 793$  n. mi.  
 $V_i = 6001$  fps

$h_E = 133\ 892$  stat. mi.  
 $V_i = 4092$  mph

Field of view =  $4^\circ$



X, nd

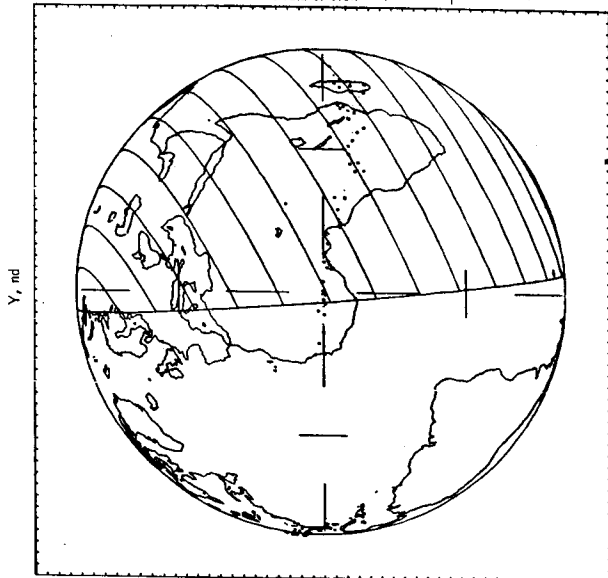
(ff) G.e.t. = 169 hours.

Figure 18.- Continued.



$R_E = 116\ 265$  n. mi.  $h_E = 129\ 832$  stat. mi.  
 $V_i = 6097$  fps  $V_i = 4157$  mph

Field of view =  $4^\circ$

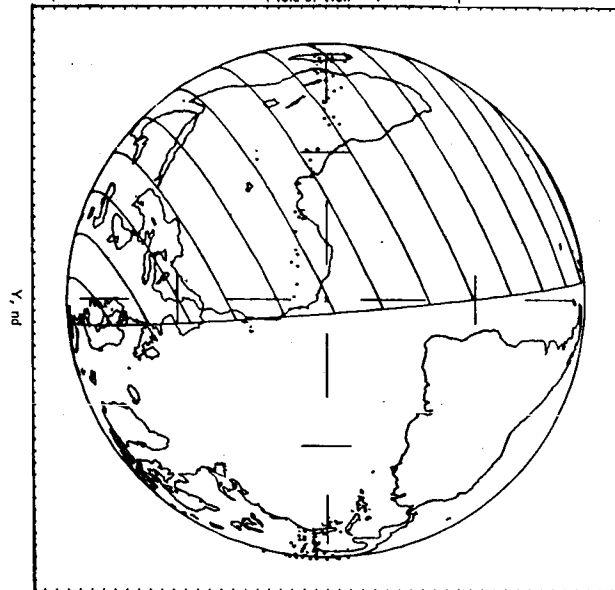


X, nd

(gg) G.e.t. = 170 hours.

$R_E = 112\ 681$  n. mi.  $h_E = 125\ 709$  stat. mi.  
 $V_i = 6199$  fps  $V_i = 4227$  mph

Field of view =  $4^\circ$

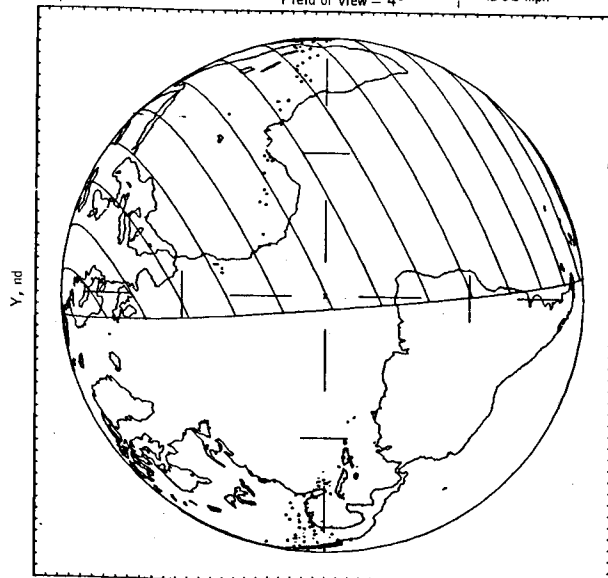


X, nd

(hh) G.e.t. = 171 hours.

$R_E = 109\ 038$  n. mi.  $h_E = 121\ 515$  stat. mi.  
 $V_i = 6308$  fps  $V_i = 4301$  mph

Field of view =  $4^\circ$

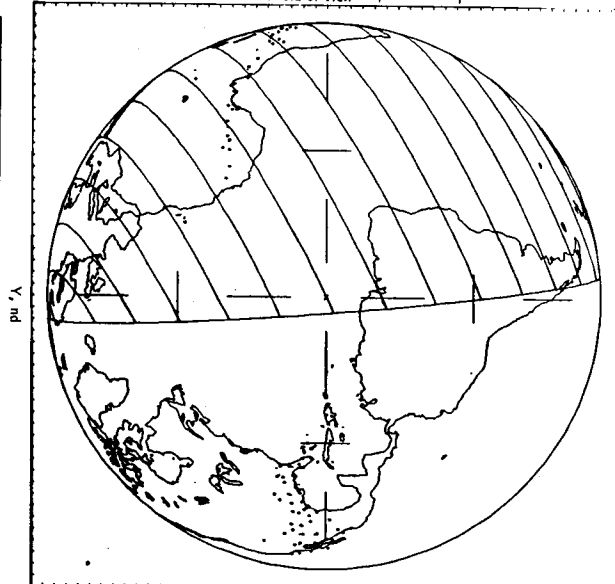


X, nd

(ii) G.e.t. = 172 hours.

$R_E = 105\ 331$  n. mi.  $h_E = 117\ 250$  stat. mi.  
 $V_i = 6425$  fps  $V_i = 4381$  mph

Field of view =  $4^\circ$



X, nd

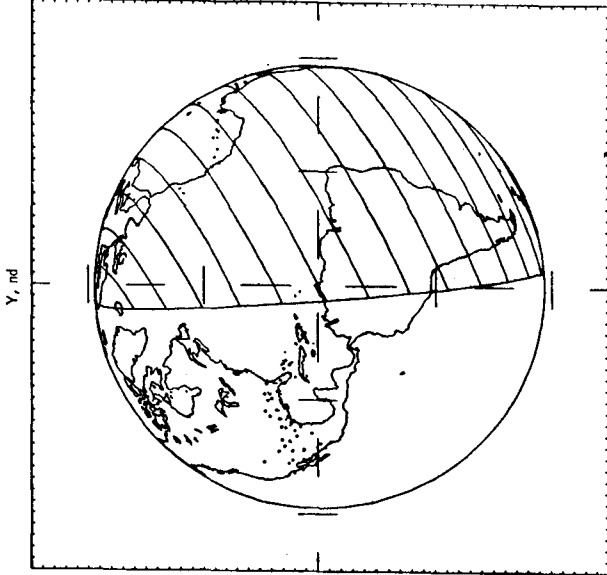
(jj) G.e.t. = 173 hours.

Figure 18.- Continued.

$R_E = 101\ 556$  n. mi.  
 $V_i = 6551$  fps

$h_E = 112\ 906$  stat. mi.  
 $V_i = 4467$  mph

Field of view =  $5^\circ$



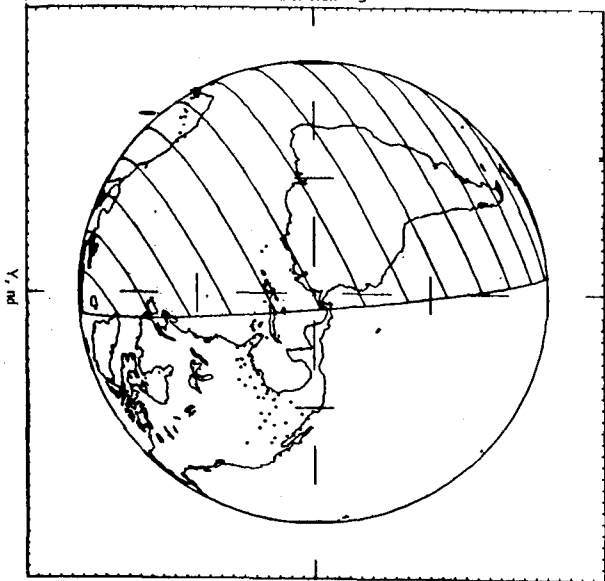
X, nd

(kk) G.e.t. = 174 hours.

$R_E = 97\ 708$  n. mi.  
 $V_i = 6686$  fps

$h_E = 108\ 478$  stat. mi.  
 $V_i = 4559$  mph

Field of view =  $5^\circ$



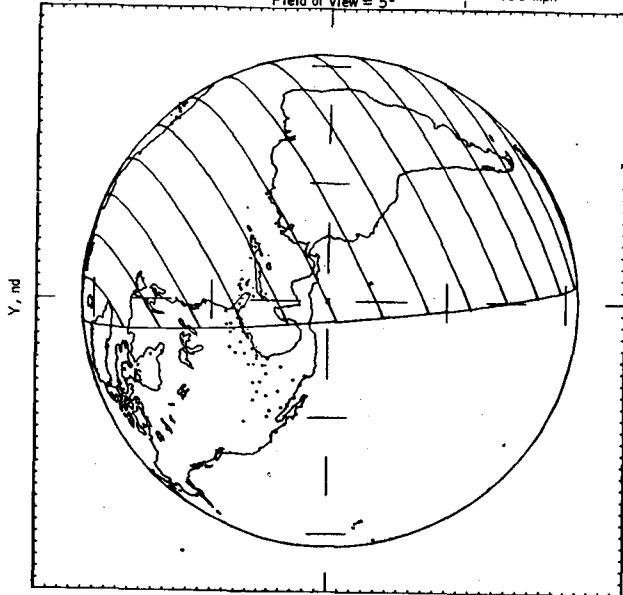
X, nd

(ll) G.e.t. = 175 hours.

$R_E = 93\ 781$  n. mi.  
 $V_i = 6832$  fps

$h_E = 103\ 959$  stat. mi.  
 $V_i = 4658$  mph

Field of view =  $5^\circ$



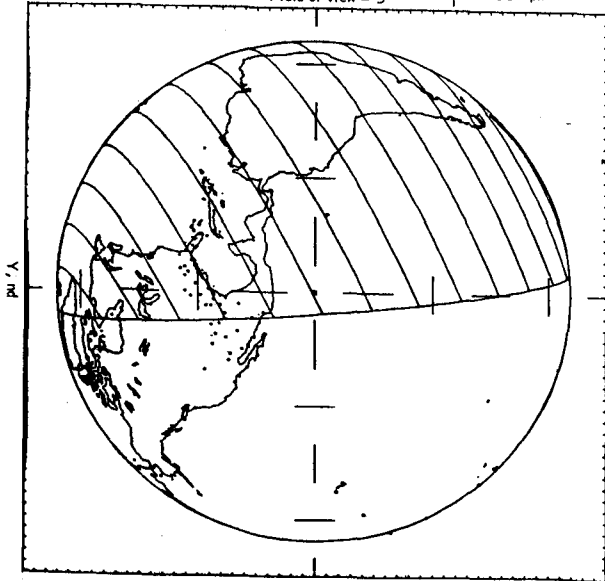
X, nd

(mm) G.e.t. = 176 hours.

$R_E = 89\ 769$  n. mi.  
 $V_i = 6991$  fps

$h_E = 99\ 342$  stat. mi.  
 $V_i = 4658$  mph

Field of view =  $5^\circ$

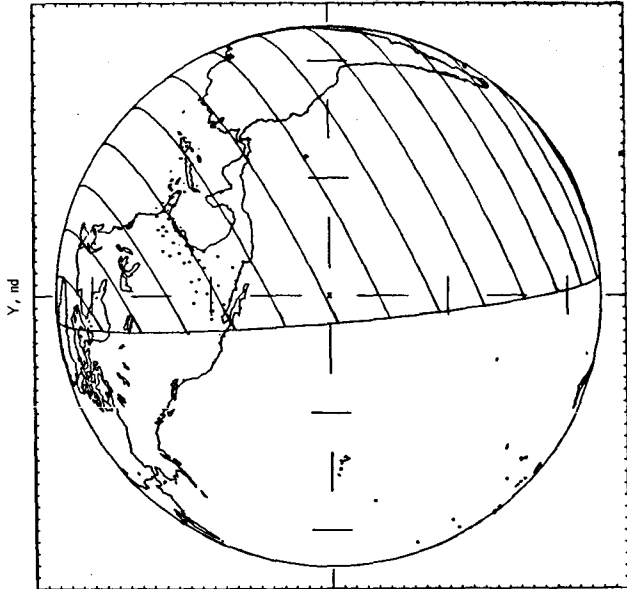


X, nd

(nn) G.e.t. = 177 hours.

$R_E = 85\,664$  n. mi.  $h_E = 94\,618$  stat. mi.  
 $V_i = 7166$  fps  $V_i = 4886$  mph

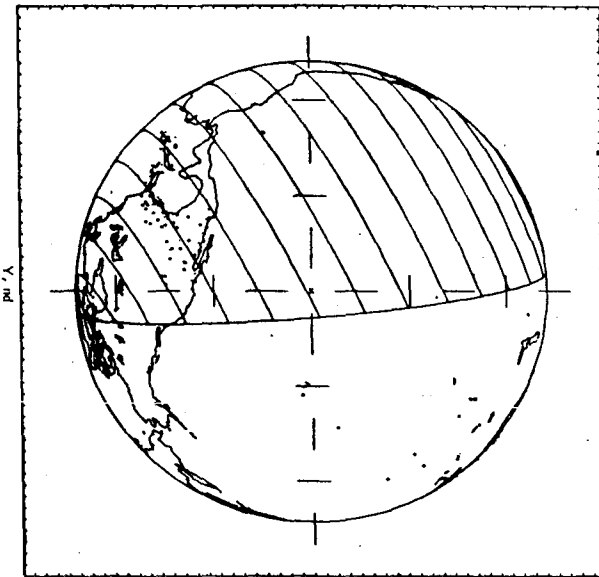
Field of view =  $5^\circ$



(oo) G.e.t. = 178 hours.

$R_E = 81\,457$  n. mi.  $h_E = 89\,776$  stat. mi.  
 $V_i = 7357$  fps  $V_i = 5016$  mph

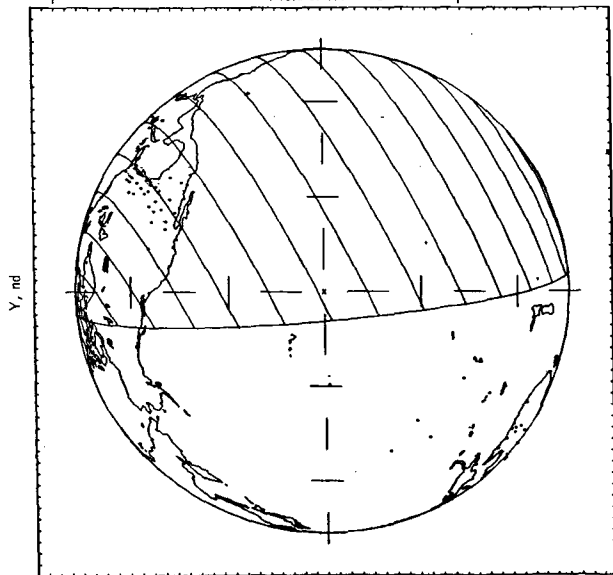
Field of view =  $6^\circ$



(pp) G.e.t. = 179 hours.

$R_E = 77\,138$  n. mi.  $h_E = 84\,807$  stat. mi.  
 $V_i = 7571$  fps  $V_i = 5162$  mph

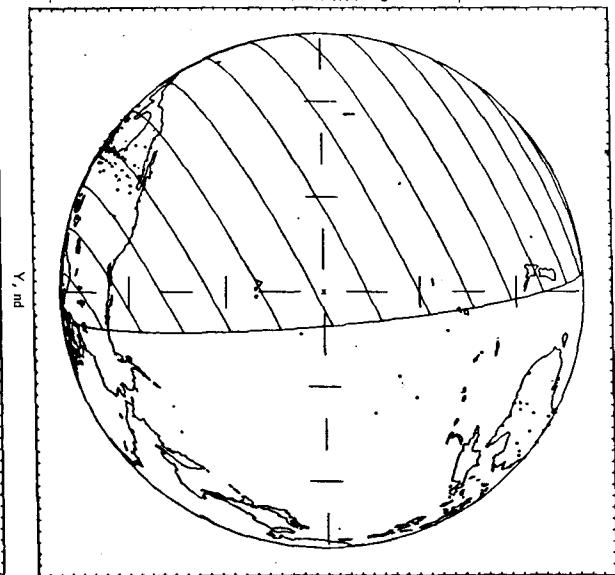
Field of view =  $6^\circ$



(qq) G.e.t. = 180 hours.

$R_E = 72\,695$  n. mi.  $h_E = 79\,692$  stat. mi.  
 $V_i = 7809$  fps  $V_i = 5324$  mph

Field of view =  $6^\circ$



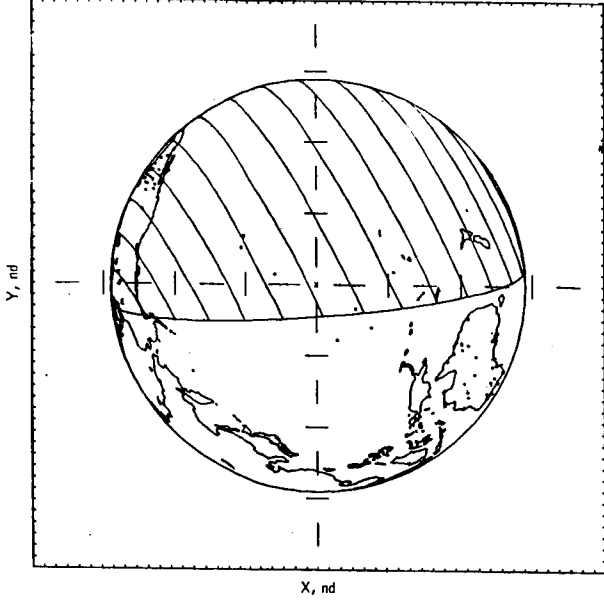
(rr) G.e.t. = 181 hours.

Figure 18.- Continued.

$R_E = 68\ 112$  n. mi.  
 $V_i = 8078$  fps

$h_E = 74\ 420$  stat. mi.  
 $V_i = 5078$  mph

Field of view =  $8^\circ$

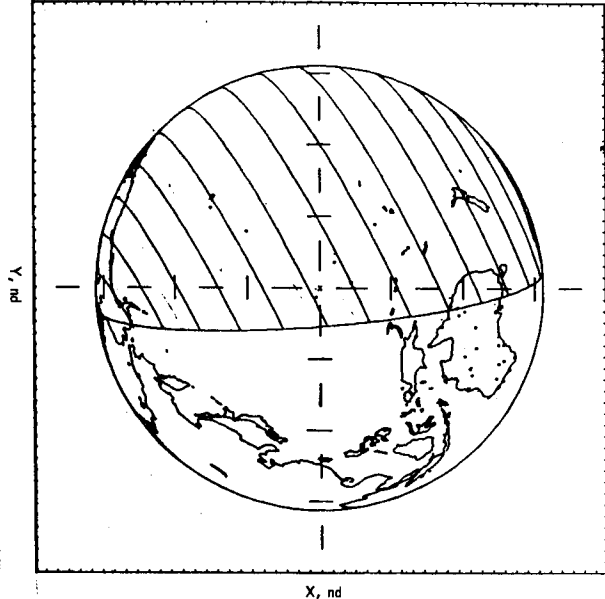


(ss) G.e.t. = 182 hours.

$R_E = 63\ 372$  n. mi.  
 $V_i = 8387$  fps

$h_E = 68\ 964$  stat. mi.  
 $V_i = 5718$  mph

Field of view =  $8^\circ$

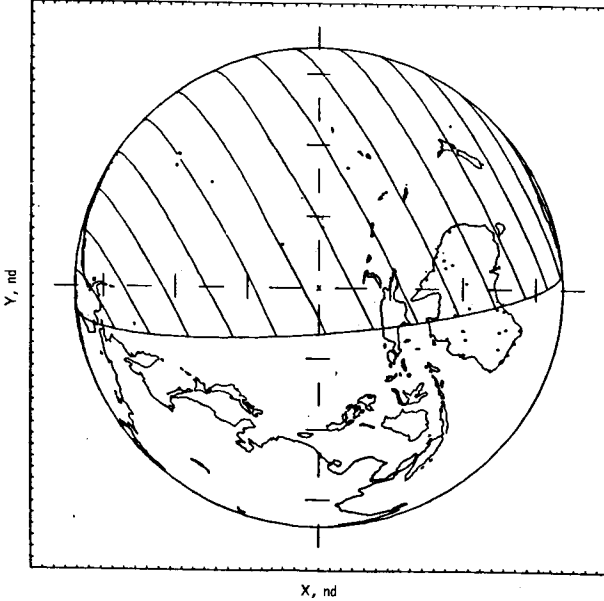


(tt) G.e.t. = 183 hours.

$R_E = 58\ 451$  n. mi.  
 $V_i = 8746$  fps

$h_E = 63\ 302$  stat. mi.  
 $V_i = 5963$  mph

Field of view =  $8^\circ$

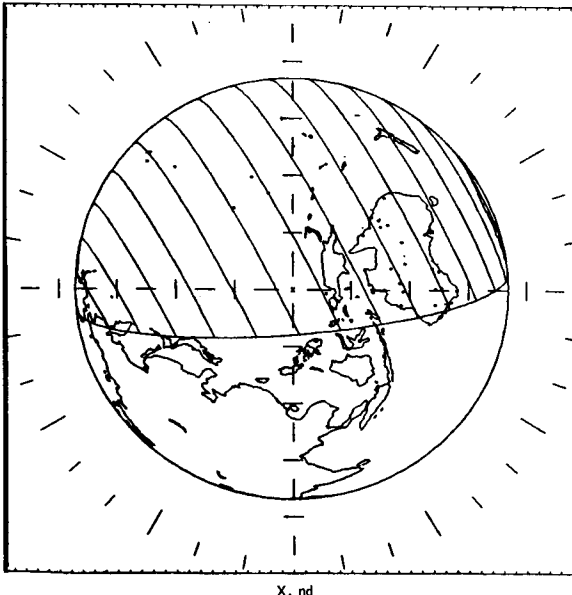


(uu) G.e.t. = 184 hours.

$R_E = 53\ 320$  n. mi.  
 $V_i = 9172$  fps

$h_E = 57\ 396$  stat. mi.  
 $V_i = 6254$  mph

Field of view =  $10^\circ$

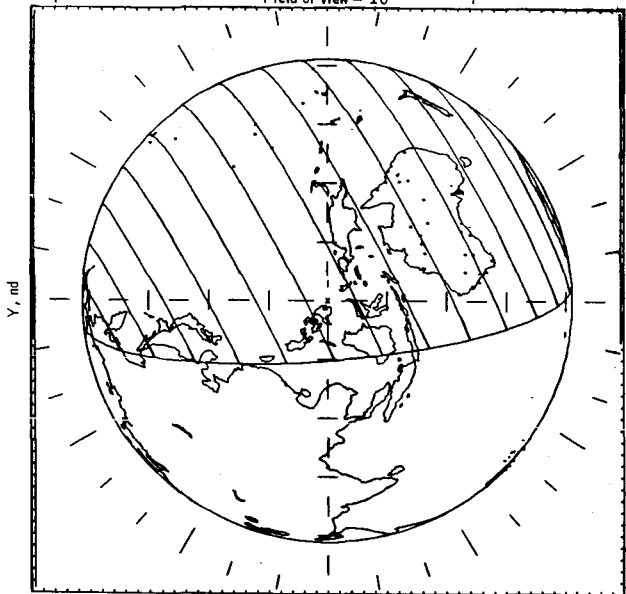


(vv) G.e.t. = 185 hours.

Figure 18. - Continued.

$R_E = 47\,938$  n. mi.  $h_E = 51\,204$  stat. mi.  
 $V_i = 9689$  fps  $V_i = 6606$  mph

Field of view =  $10^\circ$

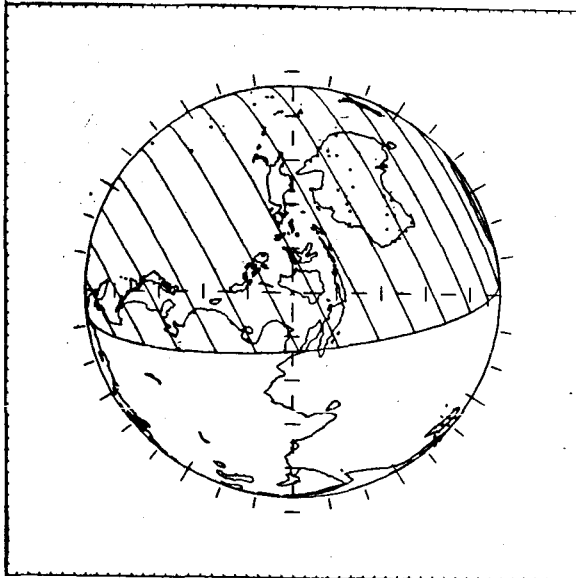


X, nd

(ww) G.e.t. = 186 hours.

$R_E = 42\,252$  n. mi.  $h_E = 44\,661$  stat. mi.  
 $V_i = 10\,338$  fps  $V_i = 7049$  mph

Field of view =  $13^\circ$

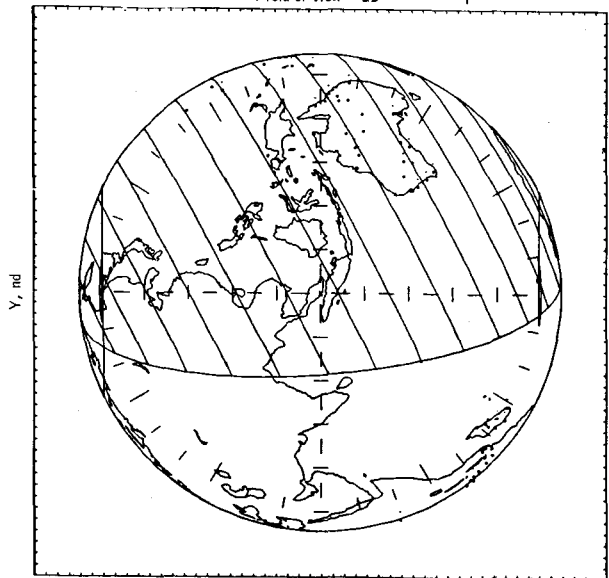


X, nd

(xx) G.e.t. = 187 hours.

$R_E = 36\,182$  n. mi.  $h_E = 37\,674$  stat. mi.  
 $V_i = 11\,192$  fps  $V_i = 7631$  mph

Field of view =  $13^\circ$

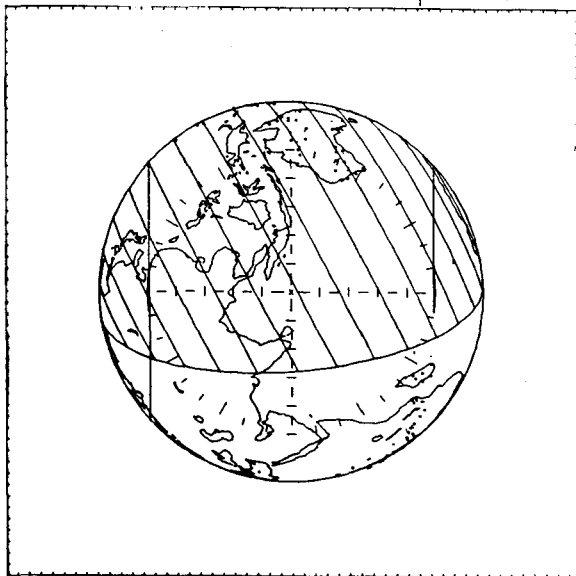


X, nd

(yy) G.e.t. = 188 hours.

$R_E = 29\,603$  n. mi.  $h_E = 30\,103$  stat. mi.  
 $V_i = 12\,399$  fps  $V_i = 9762$  mph

Field of view =  $20^\circ$



X, nd

(zz) G.e.t. = 189 hours.

Figure 18. - Continued.

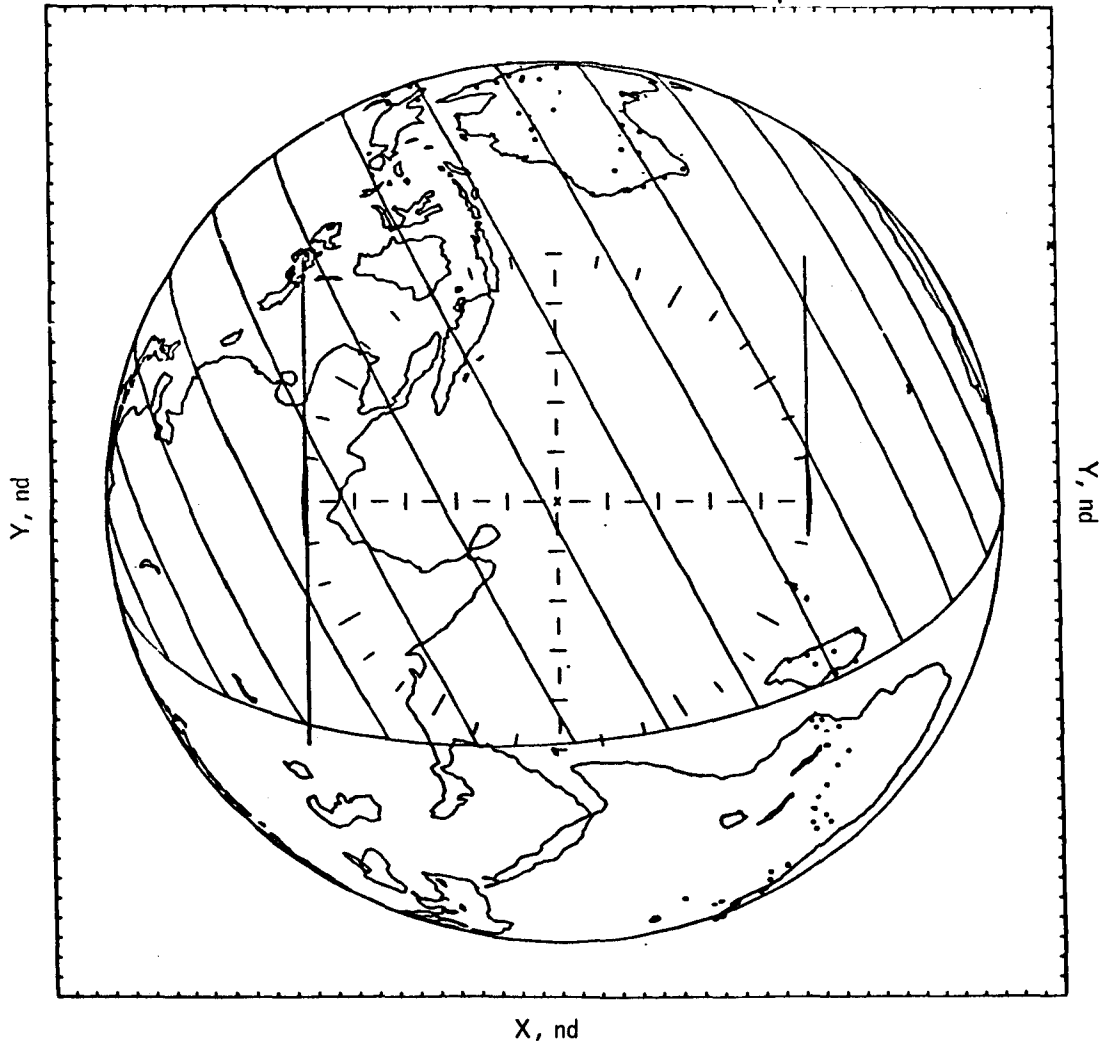
$R_E = 22\,296$  n. mi.

$V_i = 14\,318$  fps

$h_E = 21\,694$  stat. mi.

$V_i = 9762$  mph

Field of view =  $20^\circ$



(aaa) G.e.t. = 190 hours.

Figure 18.- Concluded.



SEQ	286	290	308	349	356	362	377	440	473	480	507	509
X	20	24	22	-3	10	-1	23	12	0	-3	-21	-23
Y	21	15	12	13	9	11	1	-5	-6	-6	0	1

SEQ	515	535	540	580
X	-6	-6	-22	-20
Y	-11	-16	-4	-14

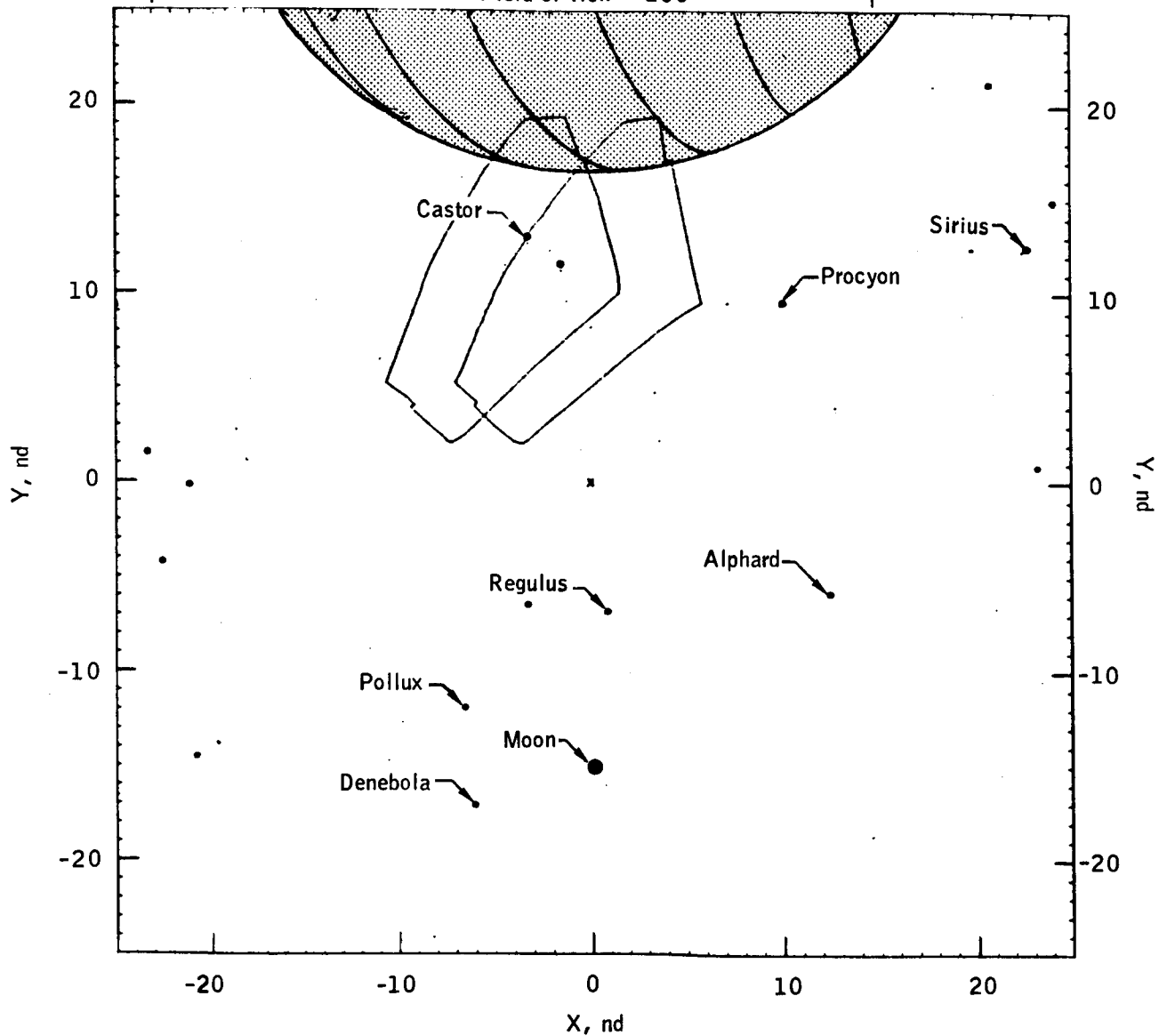
$R_E = 5426$  n. mi.

$V_i = 29\,175$  fps

$h_E = 2283$  stat. mi.

$V_i = 19\,892$  mph

Field of view =  $100^\circ$



(a) 15 min prior to entry (g.e.t. = 191:35:32.2).

Figure 19.- Entry phase.



SEQ	290	308	356	362	377	440	473	480	507	509	515	535	540
X	24	23	10	-1	23	12	0	-3	-21	-23	-6	-5	-22
Y	18	15	13	15	4	-1	-2	-2	3	4	-7	-12	0

SEQ	551	570	580	582	610	651
X	7	-1	-20	-9	-16	-24
Y	-22	-22	-10	-21	-23	-23

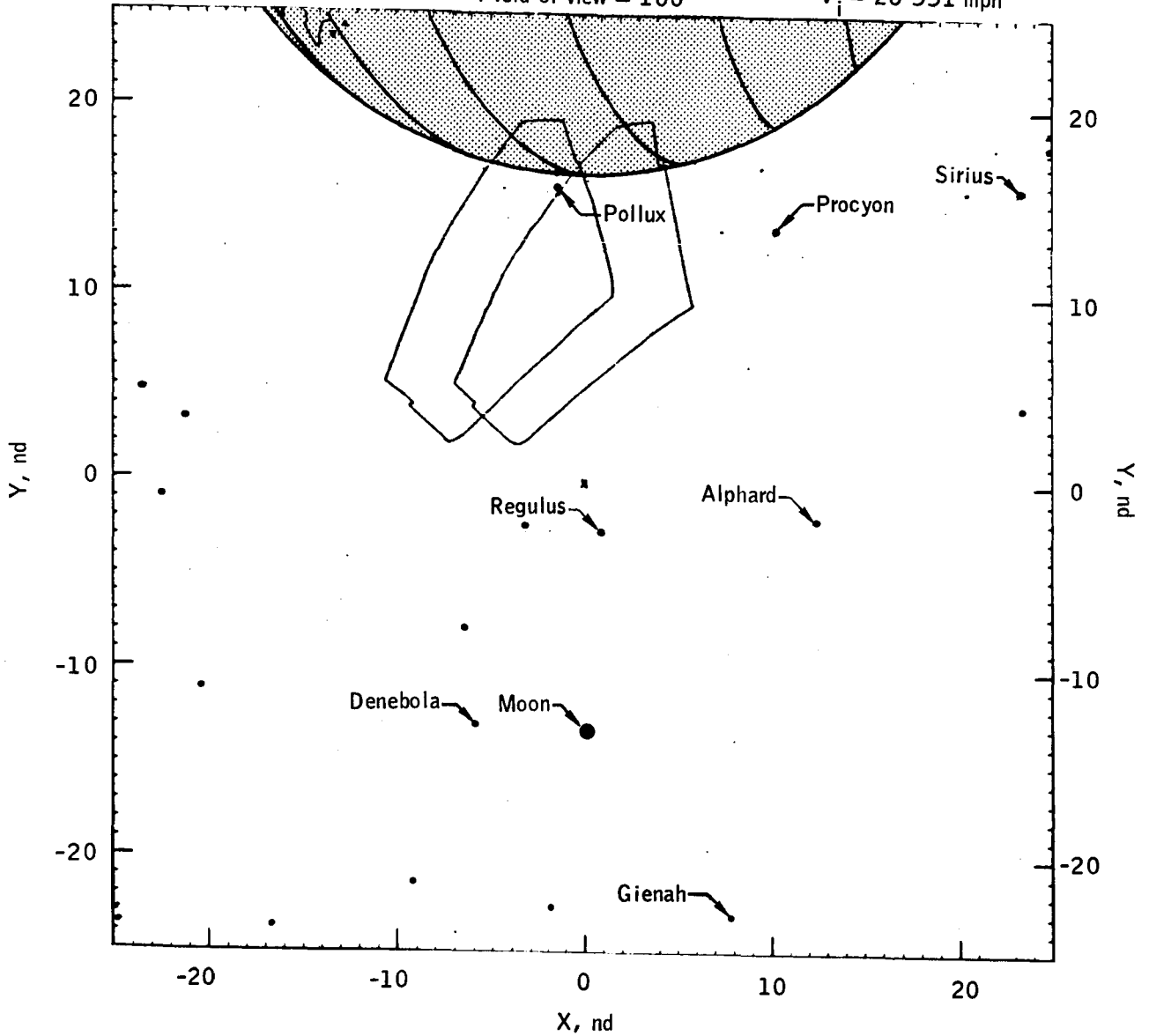
$R_E = 5085$  n. mi.

$V_i = 30\ 141$  fps

$h_E = 1891$  stat. mi.

$V_i = 20\ 551$  mph

Field of view =  $100^\circ$

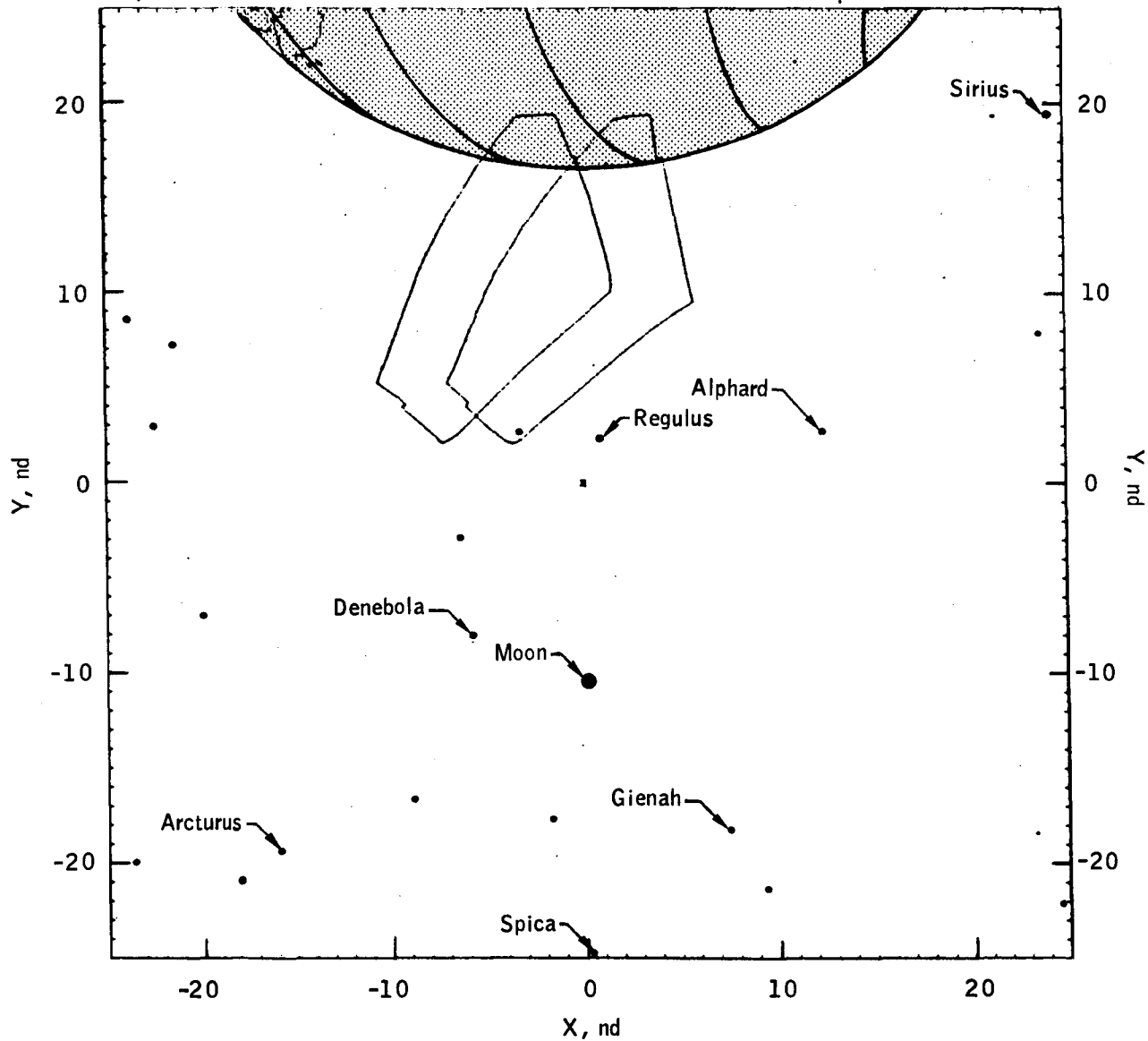


(b) 13 min prior to entry (g.e.t. = 191:39:32.2).

Figure 19. - Continued.

SEQ	378	377	440	473	480	507	509	515	535	540	545	551	566
X	24	23	12	0	-3	-21	-23	-6	-5	-22	24	7	9
Y	19	8	2	2	2	7	-8	-2	-7	3	-21	-18	-21

SEQ	570	580	582	583	610	624	651
X	-1	-19	-8	0	-15	-17	-23
Y	-17	-8	-16	-24	-19	-20	-19

 $R_E = 4756$  n. mi. $h_E = 1512$  stat. mi. $V_i = 31\,168$  fps $V_i = 21\,251$  mphField of view =  $100^\circ$ 

(c) 11 min prior to entry (g.e.t. = 191:39:32.2).

Figure 19.- Continued.

SEQ	377	440	473	480	507	509	515	535	540	545	551	566	569
X	24	12	0	-3	-21	-24	-6	-5	-22	23	7	9	21
Y	12	7	7	8	11	12	2	-2	7	-18	-12	-6	-20

SEQ	570	580	582	589	593	595	610	624	651
X	-1	-19	-8	13	0	6	-15	-17	-22
Y	-12	-2	-11	-23	-19	-22	-14	-16	-15

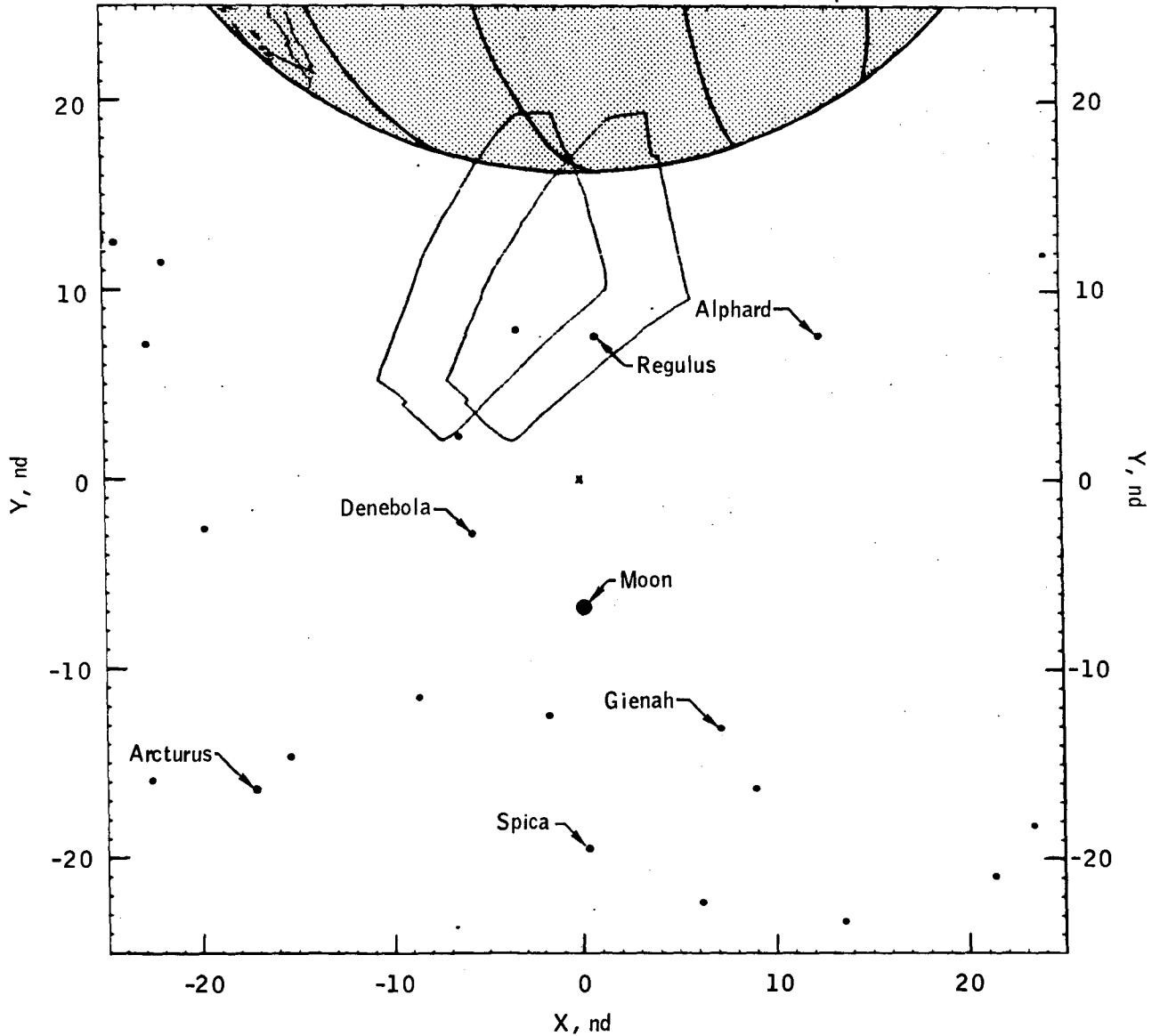
$R_E = 4446$  n. mi.

$h_E = 1247$  stat. mi.

$V_i = 32\,242$  fps

Field of view =  $100^\circ$

$V_i = 21\,983$  mph



(d) 9 min prior to entry (g.e.t. = 191:41:32.2).

Figure 19. - Continued.

SEQ	440	473	480	507	515	535	540	545	551	561	566	569	570
X	12	0	-3	-22	-6	-5	-23	22	7	24	8	20	-1
Y	13	14	14	16	8	3	12	-13	-6	-16	-9	-15	-5

SEQ	580	582	589	593	595	599	610	617	621	624	651	655	700
X	-19	-8	12	0	5	20	-14	23	10	-16	-21	-1	-16
Y	2	-5	-17	-12	-15	-20	-8	-23	-21	-10	-10	-23	-23

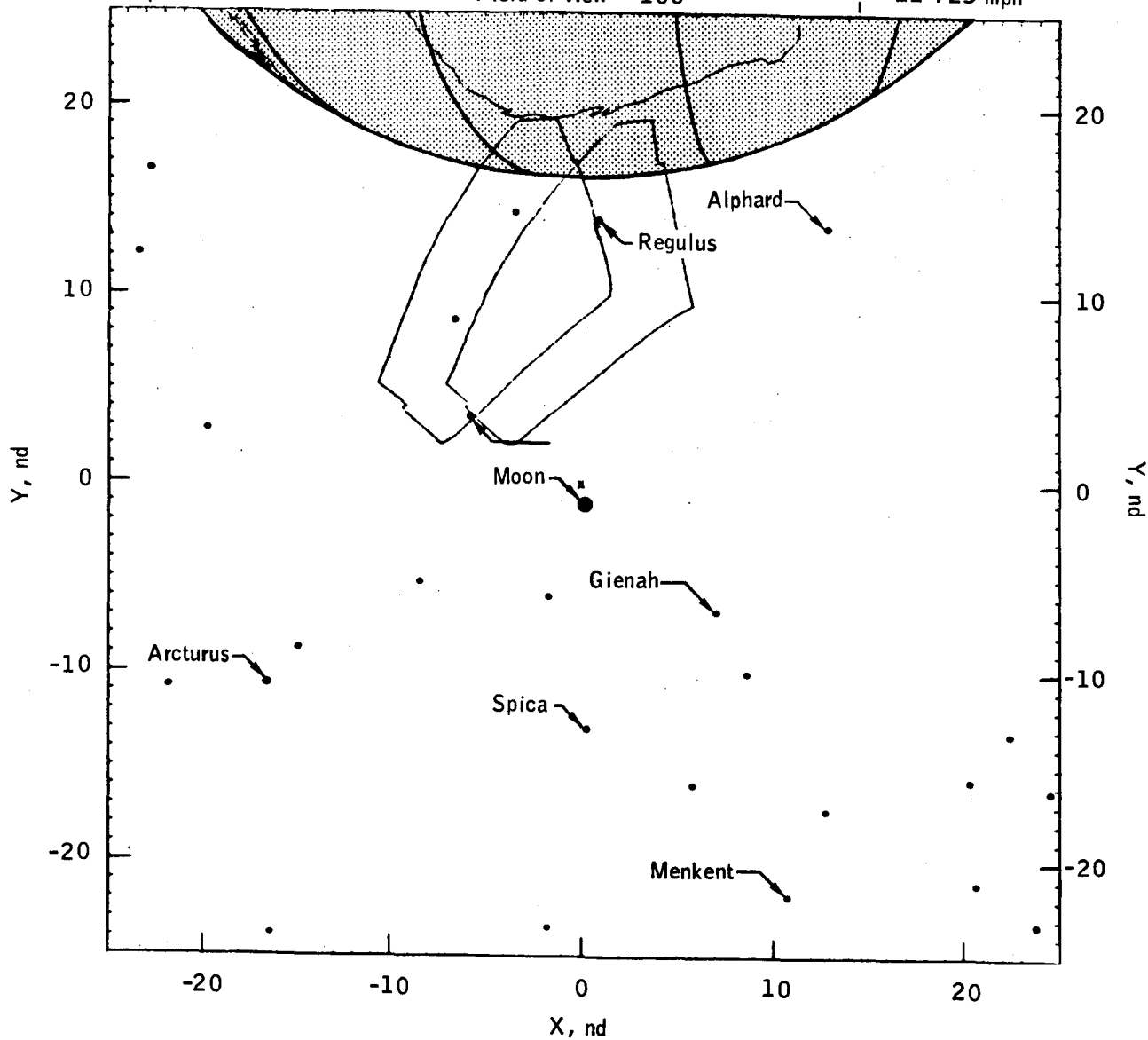
$R_E = 4161$  n. mi.

$h_E = 819$  stat. mi.

$V_i = 33\,330$  fps

$V_i = 22\,725$  mph

Field of view =  $100^\circ$



(e) 7 min prior to entry (g.e.t. = 191:43:32.2).

Figure 19.- Continued.

SEQ	515	535	540	545	551	561	566	569	570	574	580	582	589	593	595
X	-8	-5	-24	21	8	23	8	19	-1	24	-20	-8	12	0	5
Y	15	10	17	-7	0	-10	-2	-9	1	-12	9	1	-10	-5	-8
SEQ	599	610	617	621	624	641	643	645	651	655	660	673	688	690	700
X	19	-14	22	10	-16	12	21	14	-21	-1	12	6	10	-24	15
Y	-14	-1	-17	-14	-4	-18	-20	-19	-4	-16	-20	-17	-23	-9	-17

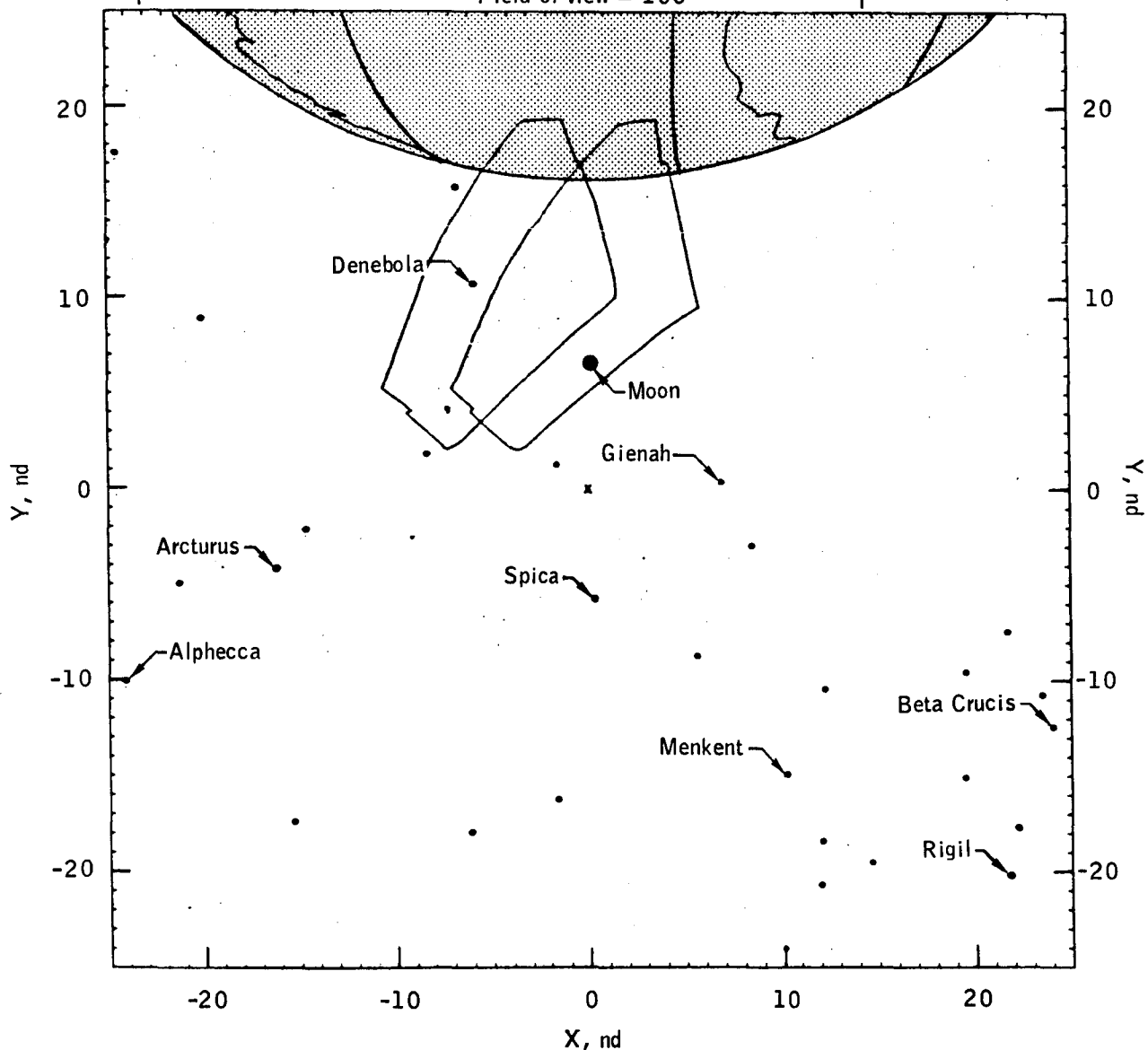
$R_E = 3910$  n. mi.

$V_i = 34\,384$  fps

$h_E = 540$  stat. mi.

$V_i = 23\,444$  mph

Field of view =  $100^\circ$



(f) 5 min prior to entry (g.e.t. = 191:45:32.2).

Figure 19.- Continued.

SEQ	545	551	561	566	569	570	574	580	582	589	593	595	599
X	21	7	22	8	19	-1	23	-20	-8	12	0	5	10
Y	0	8	-4	5	-2	9	-5	16	10	-2	2	0	-7
SEQ	610	617	621	624	641	643	645	651	655	660	673	688	
X	-14	21	9	-16	11	20	13	-21	-1	11	-5	9	
Y	5	-10	-6	3	-10	-13	-11	2	-7	-12	-9	-15	
SEQ	690	700	717	719	724	736	743	745	751	753	757	759	770
X	-23	-14	1	0	-2	0	0	-23	1	-8	23	4	-6
Y	-3	-9	-16	-16	-16	-19	-20	-11	-20	-19	-20	-22	-23
SEQ	795	803											
X	-22	-18											
Y	-21	-24											

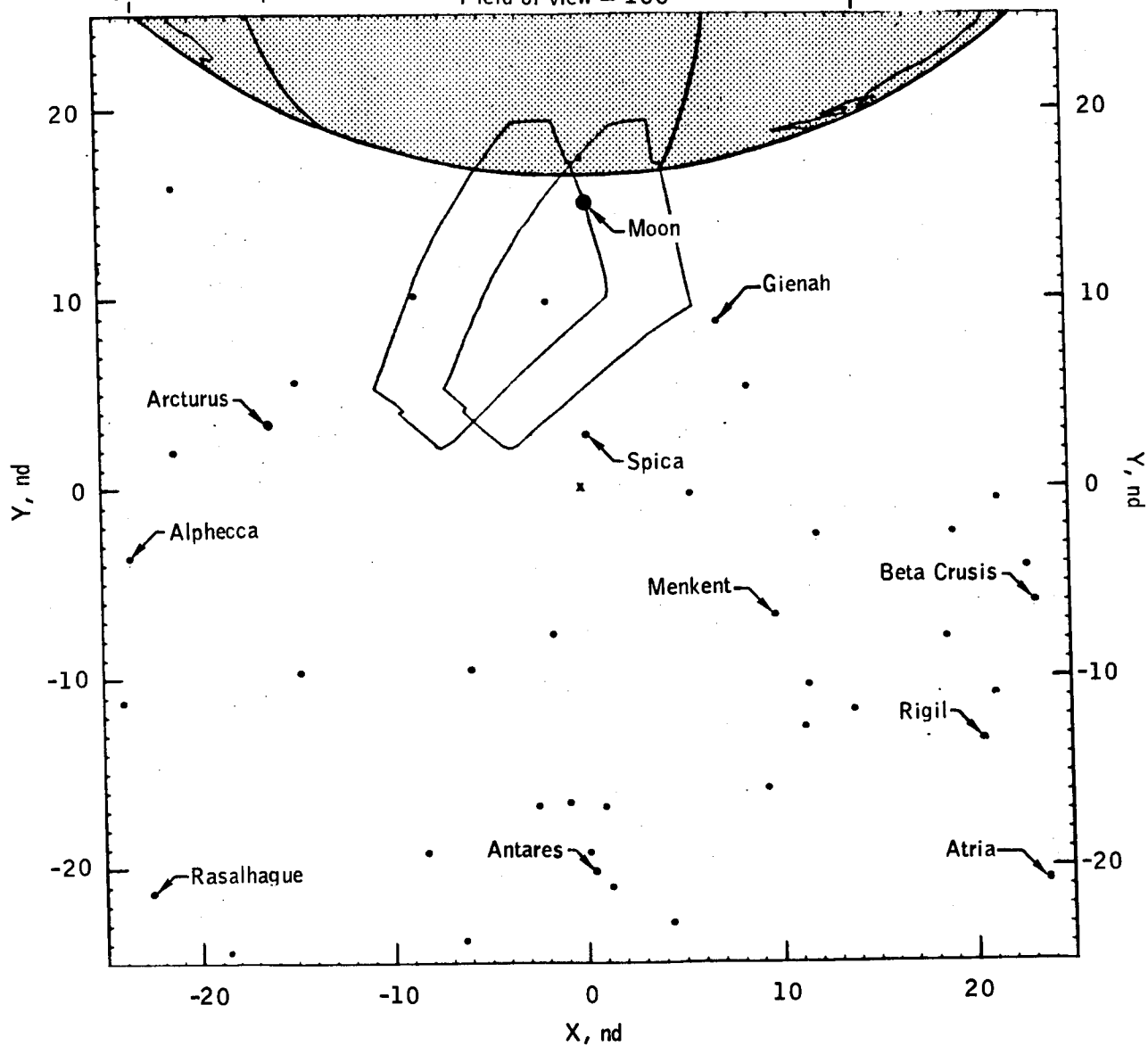
$R_E = 3706$  n. mi.

$V_i = 35\,325$  fps

Field of view =  $100^\circ$

$h_E = 304$  stat. mi.

$V_i = 24\,085$  mph



(g) 3 min prior to entry (g.e.t. = 191:47:32.2).

Figure 19.- Continued.

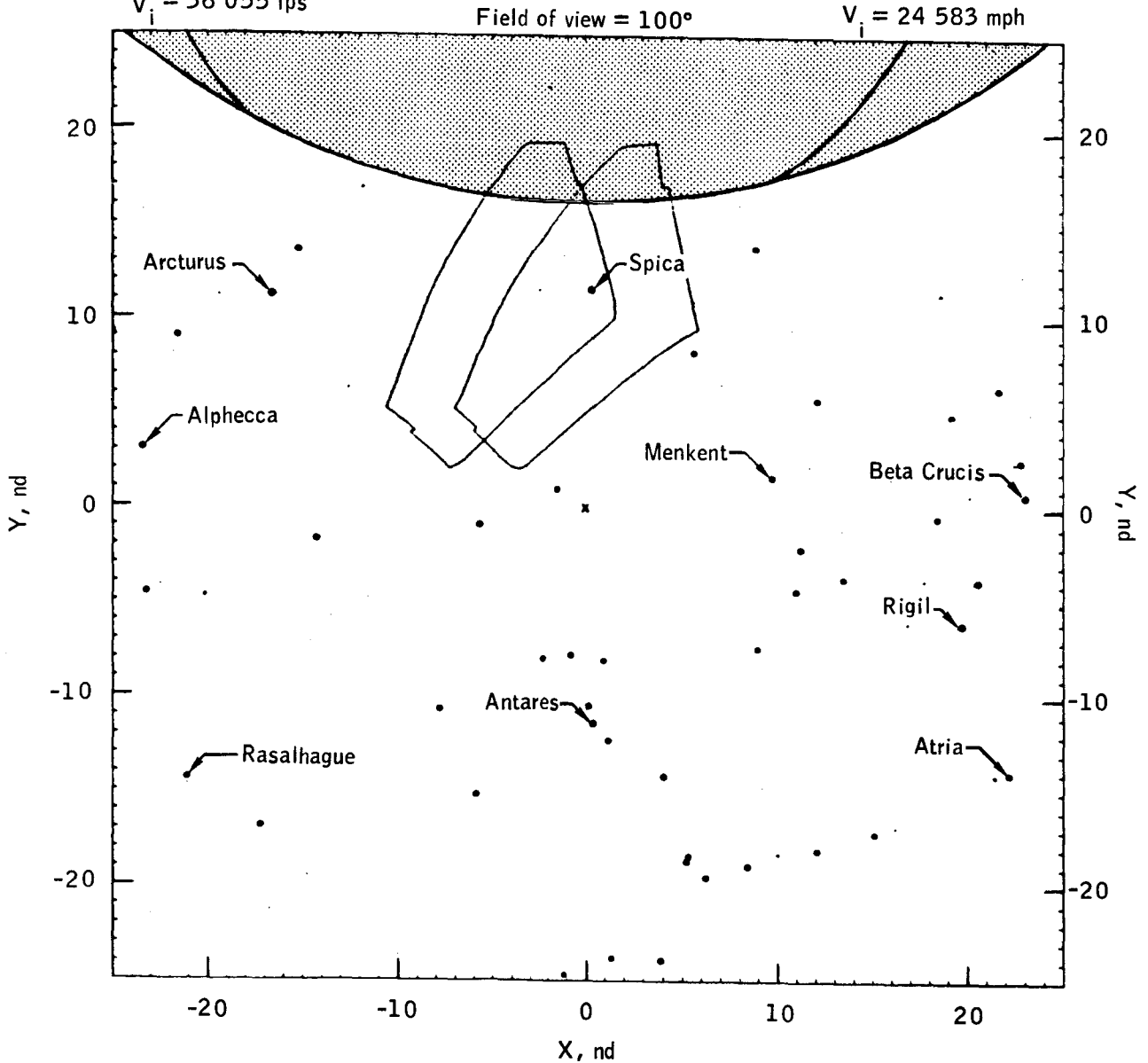
SEQ	545	561	566	569	574	589	593	595	599	610	617	621	629	641	643
X	21	22	8	19	23	12	0	5	18	-15	20	9	-16	11	19
Y	6	2	13	5	0	5	11	8	0	13	-3	1	11	-1	-5
SEQ	645	651	655	660	673	688	690	700	712	719	724	736	743	745	751
X	13	-21	-1	10	-5	8	-23	-14	8	8	-2	0	0	-23	1
Y	-3	9	1	-4	0	-7	3	-1	7	-7	-7	-10	-11	-4	-12
SEQ	753	757	769	770	781	789	790	793	795	797	802	803	836	841	844
X	-7	22	4	-5	15	5	12	5	-21	8	6	-17	1	3	-1
Y	-10	-13	-14	-15	-17	-18	-17	-18	-14	-18	-19	-16	-23	-23	-24

$R_E = 3557$  n. mi.

$V_i = 36\,055$  fps

$h_E = 132$  stat. mi.

$V_i = 24\,583$  mph



(h) 1 min prior to entry (g.e.t. = 191:49:32.2).

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SEQ	545	546	549	574	589	593	595	599	617	621	641	643	645
X	21	22	19	23	12	0	5	18	20	9	11	19	13
Y	10	6	8	4	10	16	12	3	0	6	2	02	0
SEQ	651	655	660	673	688	690	700	717	719	724	736	743	
X	-21	-1	10	-5	8	-23	-14	0	0	-2	0	0	
Y	12	5	0	3	-2	6	2	-3	-3	-3	-5	-6	
SEQ	745	751	753	757	759	770	781	789	790	793	795	797	802
X	-23	1	-7	21	4	-5	14	5	11	5	-20	8	6
Y	0	-7	-6	-10	-9	-10	-12	-13	-13	-14	-10	-64	-14
SEQ	803	836	841	844	861	871	933						
X	-16	1	3	-1	0	1	18						
Y	-12	-19	-19	-19	-22	-23	-24						

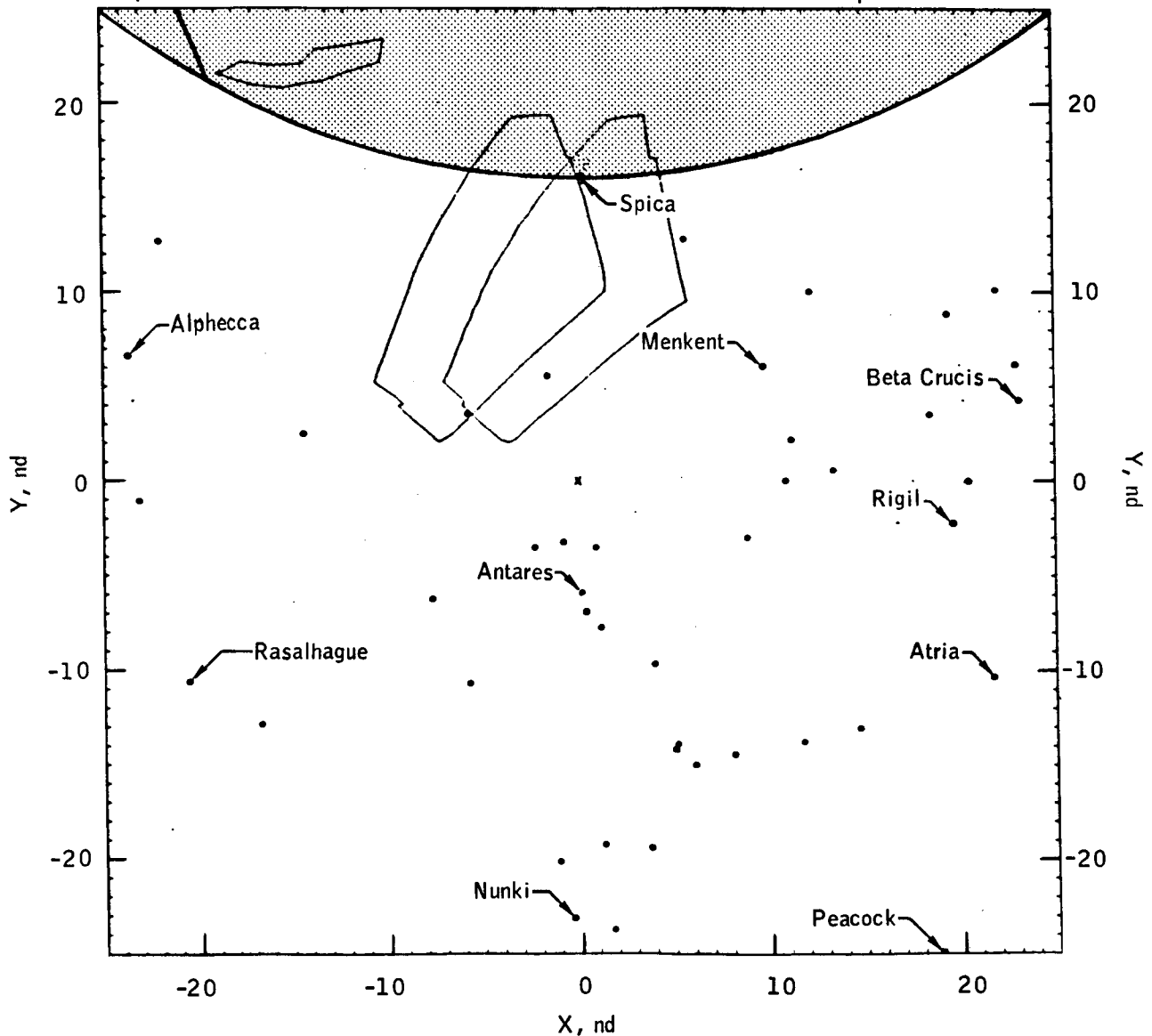
$R_E = 3508$  n. mi.

$V_i = 36\,309$  fps

Field of view =  $100^\circ$

$h_E = 76$  stat. mi.

$V_i = 24\,756$  mph



(i) Entry interface (g.e.t. = 191:50:32.2).

Figure 19.- Concluded.



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3. OMAB; LMAB; and LAB: The Spacecraft Operational Trajectory for Apollo 10 (Mission F), Volume II. MSC IN 69-FM-97,