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NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

MSC INTERNAL NOTE NO. 69-FM-136

May 13, 1969

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APOLLO 10 (MISSION F)  
CREW CHARTS



Mission Planning Support Office

MISSION PLANNING AND ANALYSIS DIVISION

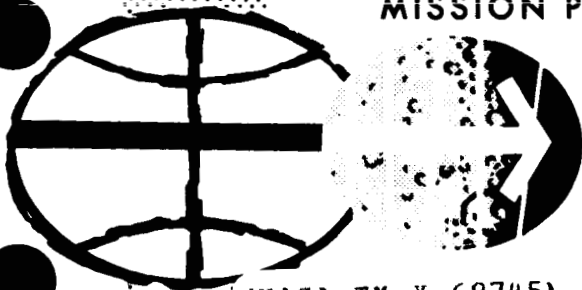
MANNED SPACECRAFT CENTER  
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(NASA-TM-X-69745) APOLLO 10 (MISSION F)  
CREW CHARTS (NASA) 46 p

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*Internal Note No 69-FM-136*



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PROJECT APOLLO

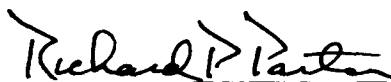
APOLLO 10 (MISSION F) CREW CHARTS


By Data Management Group  
Mission Planning Support Office

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May 13, 1969

MISSION PLANNING AND ANALYSIS DIVISION  
NATIONAL AERONAUTICS AND SPACE ADMINISTRATION  
MANNED SPACECRAFT CENTER  
HOUSTON, TEXAS

Approved:   
Richard P. Parten, Chief  
Mission Planning Support Office

Approved:   
John P. Mayer, Chief  
Mission Planning and Analysis Division

## FOREWORD

The purpose of this document is to present the crew charts for Apollo 10 (Mission F). These charts have been coordinated by the Data Management Group of Mission Planning and Analysis Division with Mr. Bill Anderson of Flight Crew Support Division and Mr. Ray Mitchell of TRW, who supports the Flight Planning Branch FCSD under TRW task 81. The charts are to be included in the onboard data file and are considered to be presented in final form as of May 5, 1969.

Should any changes be made to the crew charts prior to lift-off, the backup crew's copy of the onboard crew charts will reflect the changes and will supersede the original charts. An operational description of the crew charts will not be covered in this document because the charts have already been defined in the mission techniques documents.

The following is a list of the Apollo 10 (Mission F) crew charts, with the originator of each chart and responsible organization.

Chart 1: Launch abort curves - E. M. Henderson, FAB/MPAD

Chart 2: Listing of planned launch trajectory parameters - E. M. Henderson, FAB/MPAD

Chart 3: TLI + 10 minute abort - B. Weber, FAB/MPAD

Chart 4: TLI + 10 minute abort - B. Weber, FAB/MPAD

Chart 5: Nominal LOI 15 minute abort CSM/LM - C. Foggatt, FAB/MPAD

Chart 6: LOI mode I 15 minute and 5 hour abort curves, CSM only - C. Foggatt, FAB/MPAD

Chart 7: LOI mode III abort curves, CSM only - C. Foggatt, FAB/MPAD

Chart 8: LM PDI abort maneuver - J. Bell, OMAB/MPAD

Chart 9:  $\Delta V_0$  versus  $\Delta\theta_{\text{Long}}$ ,  $K = .4$  to  $.04$  - J. Yencharis, LMAB/MPAD

Chart 10:  $\Delta V_0$  versus  $\Delta\theta_{\text{Long}}$ ,  $K = .04$  to  $.004$  - J. Yencharis, LMAB/MPAD

Chart 11: P37 return to earth program - corridor control -  
J. Yencharis, LMAB/MPAD

Loss of communication Navigation Procedures - C. Denham, MPB/MPAD

Chart 12: Detailed sighting schedule for aborts at TLI + 4 hr  
for a May 18, 1969, launch (15.5-hr return) - C. Denham, MPB/MPAD

Chart 13: Detailed sighting schedule for aborts at TLI + 4 hr for  
a May 18, 1969, launch (greater than a 15.5-hr return) - C. Denham, MPB/MPAD

Chart 14: Detailed sighting schedule for aborts from lunar orbit  
after rev 17 for a May 18, 1969, launch (TEI to TEI plus 40 hr) -  
C. Denham, MPB/MPAD

Chart 15: Detailed sighting schedule for aborts from lunar orbit  
after rev 17 for a May 18, 1969, launch (EI minus 40 hr to EI) -  
C. Denham, MPB/MPAD

Chart 16: Planet half-unit vectors - J. Blucker, MPB/MPAD

Chart 17: Entry Corridor - J. Burton, LAB/MPAD

Chart 18: Command module computer constant - drag value - J. Burton,  
LAB/MPAD

Chart 19: Earth orbit BBA versus  $\Delta\Delta V_x$  - J. Burton, LAB/MPAD

Chart 20: SM RCS propellant profile (total) - A. Loyd, GPB/MPAD

Chart 21: Onboard reading of LM RCS propellant remaining, percentage -  
S. Mayfield, GPB/MPAD

Chart 22: SPS tailoff  $\Delta V$  versus spacecraft weight - O. Graf, GPB/MPAD

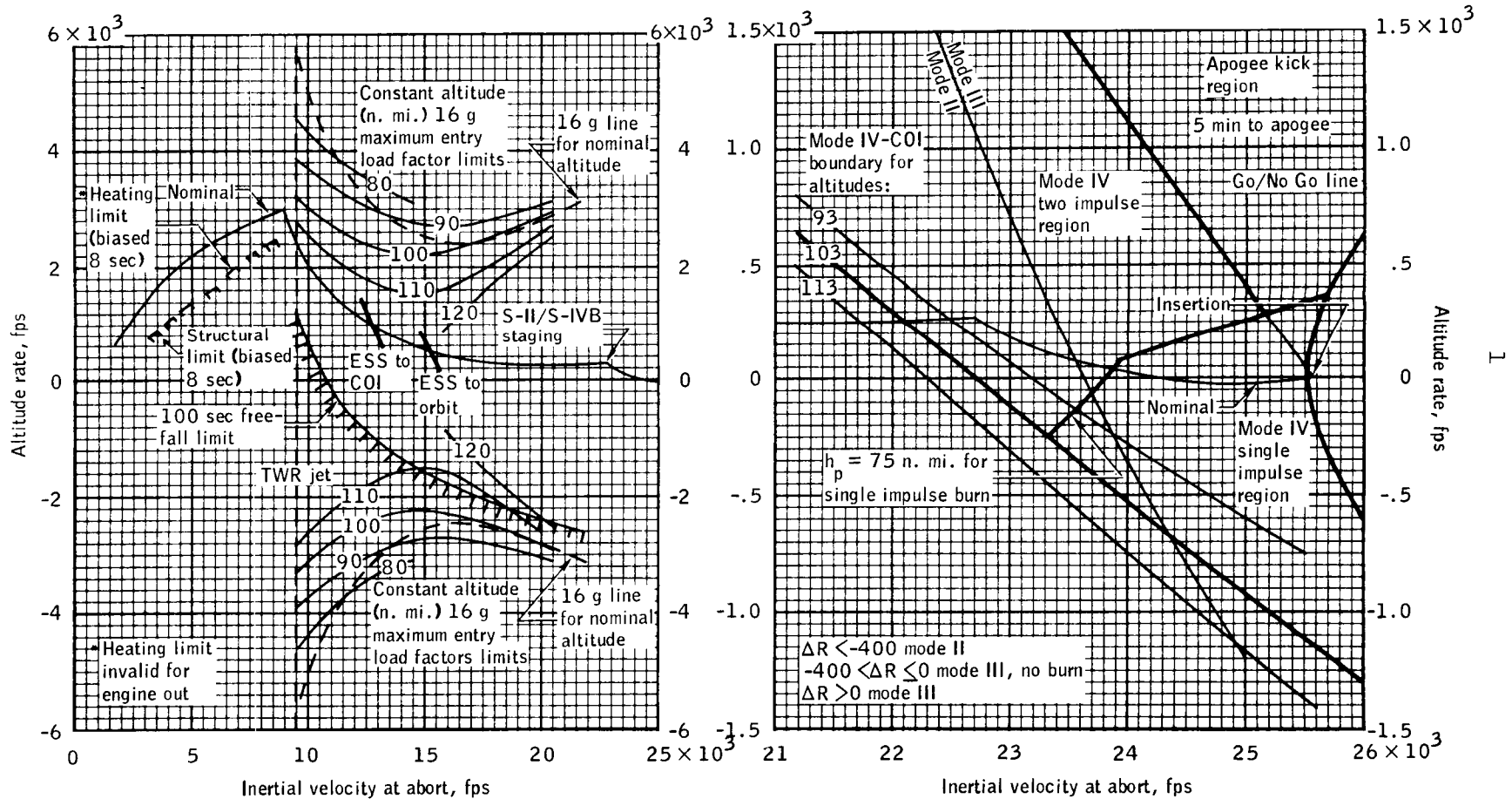
Chart 23: SPS versus RCS criteria, CSM alone - minimum preburn  
ullage - O. Graf, GPB/MPAD

Chart 24: Hydrogen remaining in one tank - W. Scott, GPB/MPAD

Chart 25: Onboard readout of ascent oxygen remaining, percentage -  
W. Scott, GPB/MPAD

Detailed sighting schedules for May 20, 23, 24, and 25 launch days  
will be provided to Flight Crew Support Division by the Data Management  
Group in the form of crew charts on May 13, 1969.

Any questions concerning this document should be directed to  
Mike Collins, Data Management Group, Mission Planning Support Office,  
HU3-4908.



Crew chart 1. - Launch abort curves.

Henderson/FAB/MPAD  
4/18/69

Time from first motion, g.e.t., min:sec	SC IMU pitch gimbal angle, $\theta$ , deg	DSKY displays		
		Inertial velocity, $V_i$ , fps	Altitude rate, h, fps	Altitude, h, n. mi.
00:00.0	90	1 340	0	0.0
00:30.0	87	1 390	296	0.7
01:00.0	69	1 847	828	3.3
01:30.0	48	3 051	1486	9.0
02:00.0	33	5 127	2200	18.2
02:15.0*	27	6 567	2582	24.1
02:30.0	23	7 928	2822	30.7
02:39.9**	22	8 998	3009	35.5
03:00.0	22	9 239	2626	44.8
03:30.0	29	9 805	2153	56.6
04:00.0	26	10 449	1801	66.4
04:30.0	23	11 190	1474	74.5
05:00.0	20	12 030	1178	81.1
05:30.0	17	12 976	916	86.2

\*S-IC center-engine cutoff (TB<sub>2</sub>)

\*\*S-IC outboard-engine cutoff (TB<sub>3</sub>)

Time from first motion, g.e.t., min:sec	SC IMU pitch gimbal angle, $\theta$ , deg	DSKY displays		
		Inertial velocity, $V_i$ , fps	Altitude rate, h, fps	Altitude, h, n. mi.
06:00.0	14	14 038	691	90.2
06:30.0	10	15 230	507	93.2
07:00.0	7	16 574	369	95.4
07:30.0	3	18 097	289	97.1
08:00.0	3	19 566	267	98.4
08:30.0	0	20 801	248	99.8
09:00.0	356	22 053	256	101.0
09:13.9***	354	22 682	280	101.7
09:30.0	350	22 872	207	102.3
10:00.0	346	23 426	103	103.1
10:30.0	343	24 011	27	103.5
11:00.0	341	24 625	-13	103.5
11:30.0	339	25 269	-19	103.4
11:43.2****	339	25 562	0	103.4

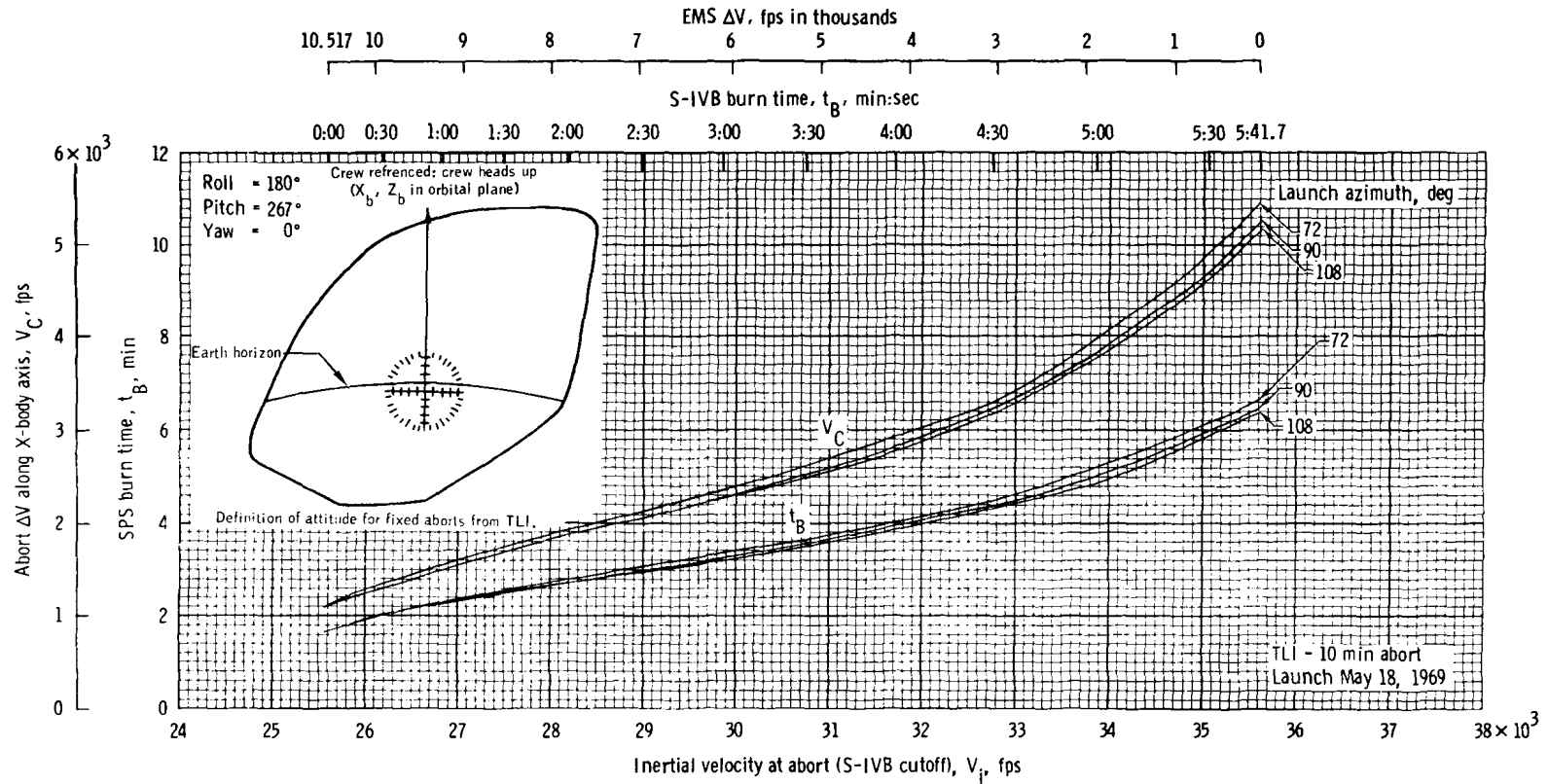
\*\*\*S-II engine cutoff (TB<sub>4</sub>)

\*\*\*\*S-IVB guidance cutoff signal

2

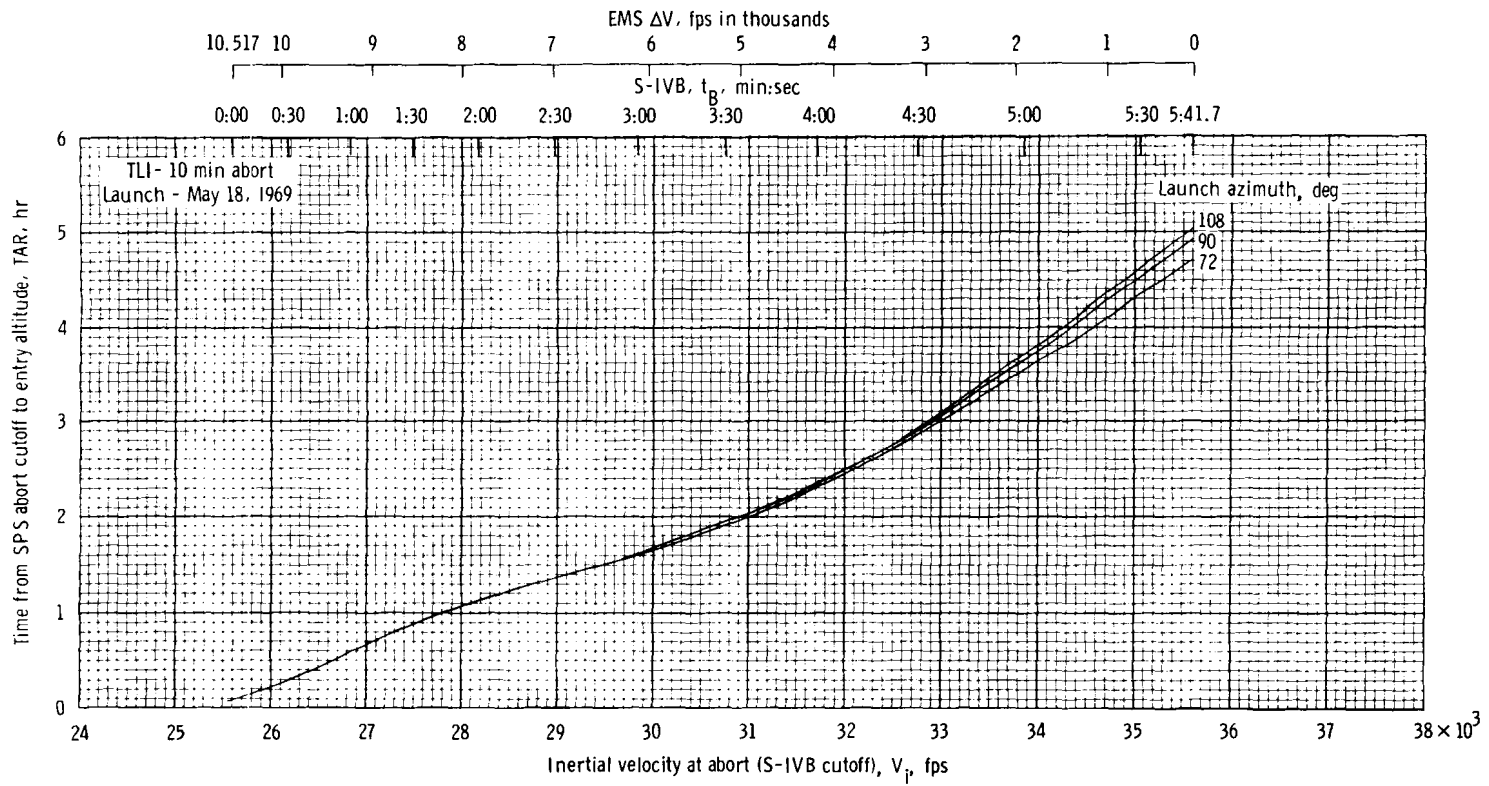
Crew chart 2. - Listing of planned launch trajectory parameters.

Weber/FAB/ MPAD  
3/31/69



Crew chart 3. - TLI + 10 minute abort

Weber/FAB/MPAD  
3/31/69

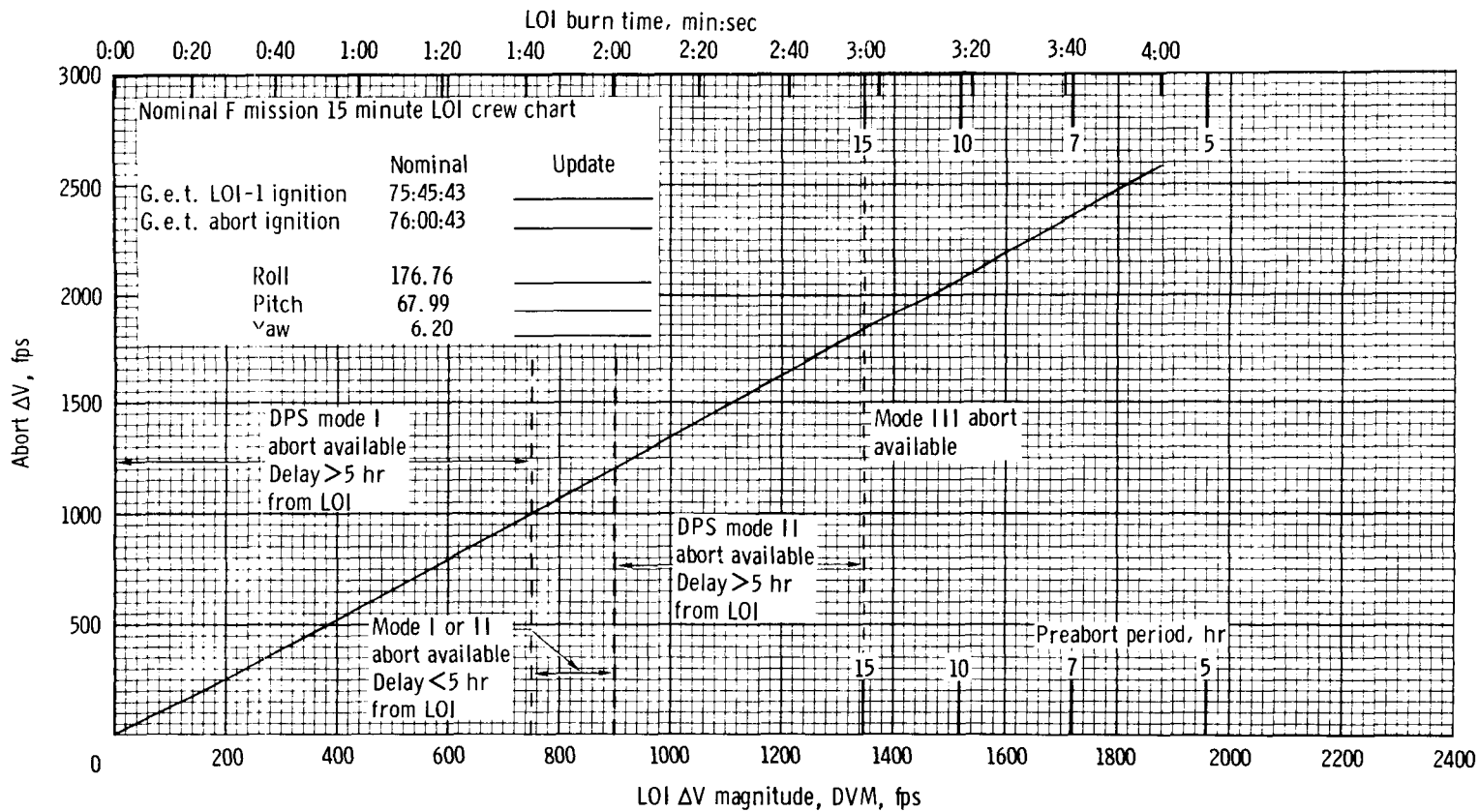


Crew chart 4. - TLI + 10 minute abort

7



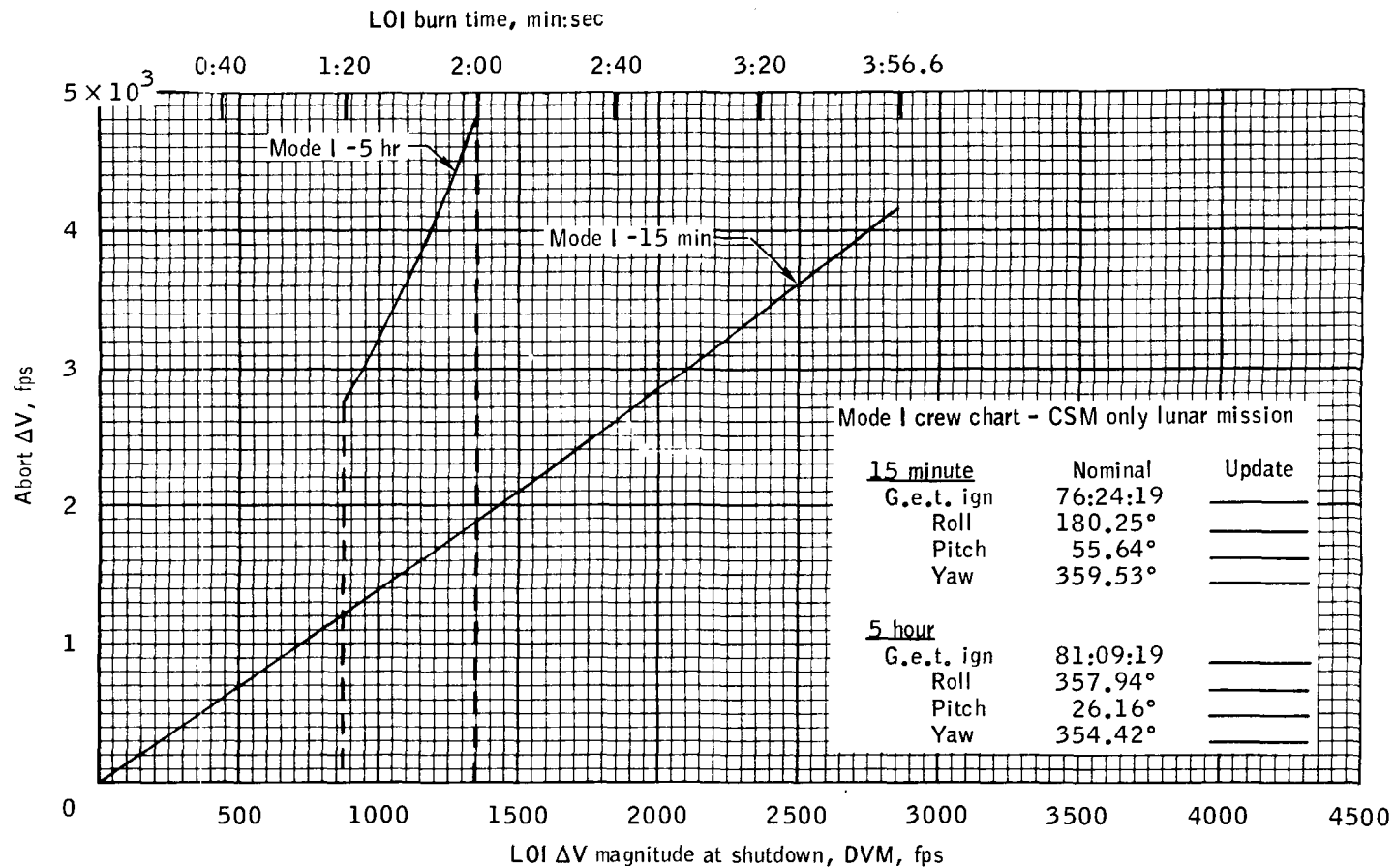
Foggatt/FAB/MPAD  
3/31/69



Crew chart 5. - Nominal LOI 15 minute abort CSM/LM.

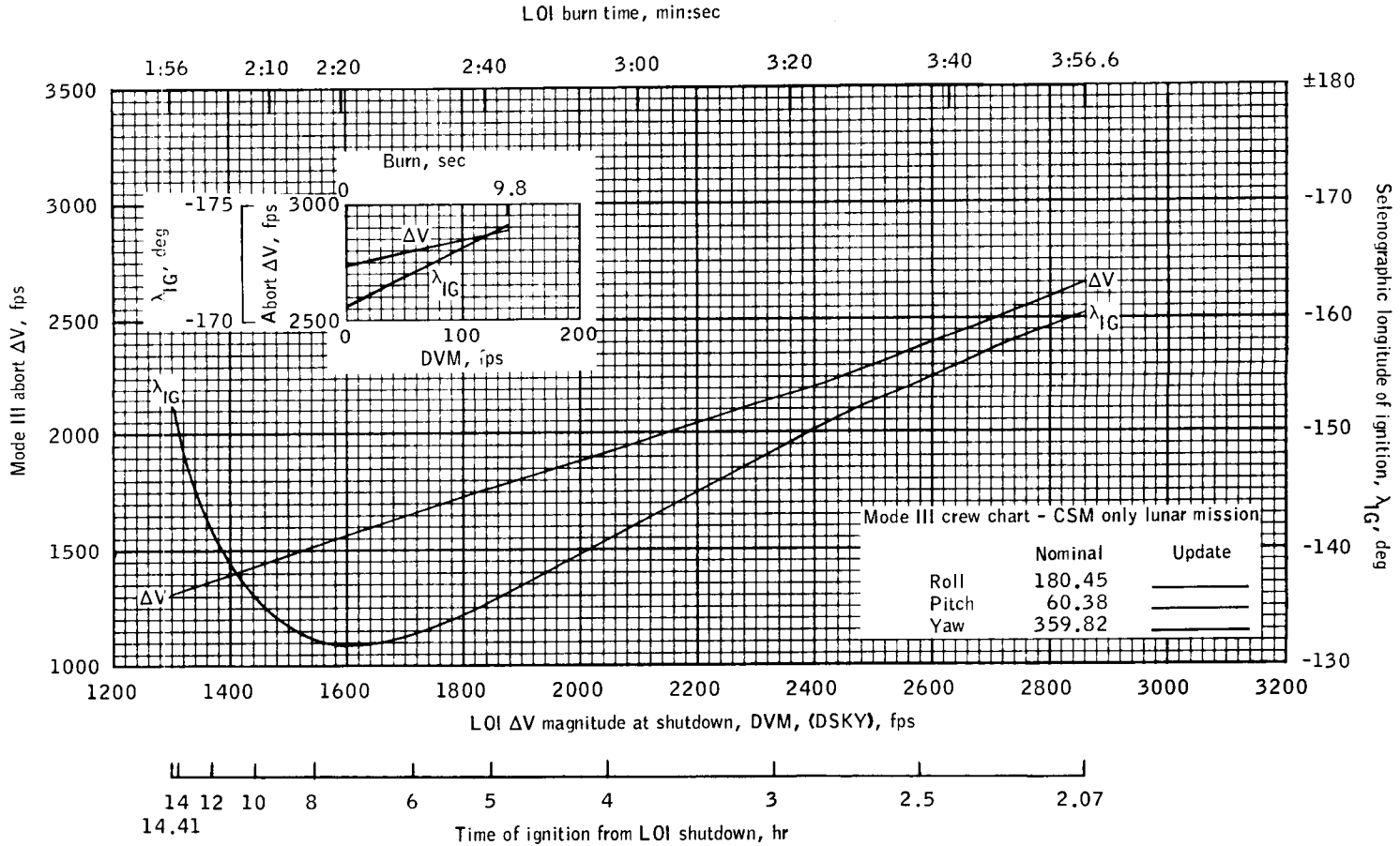
5

Foggatt/FAB/MPAD  
3/31/69



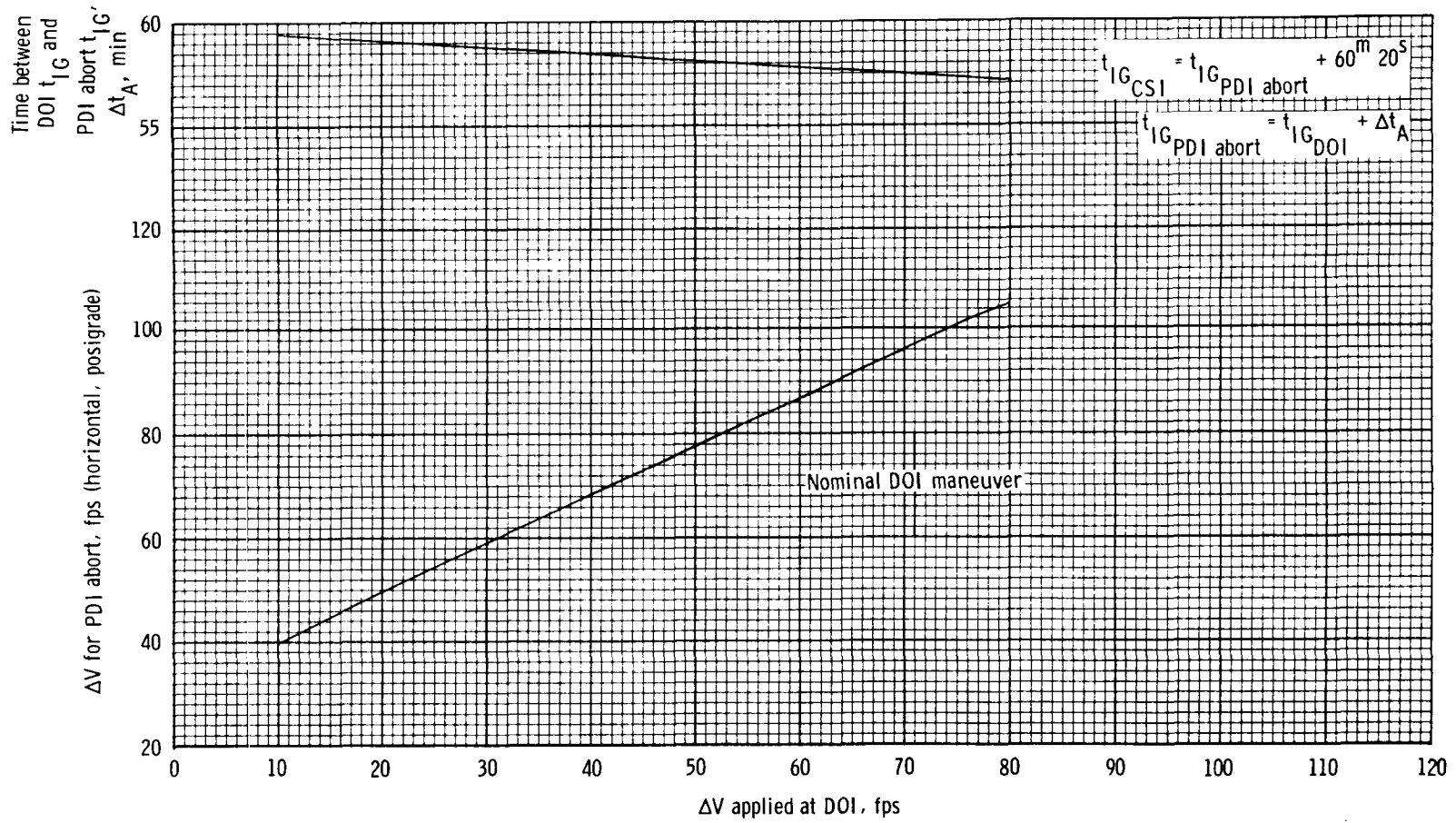
Crew chart 6.- LOI mode I 15 min and 5 hour abort curves, CSM only.

Foggatt/FAB/MPAD  
3/31/69



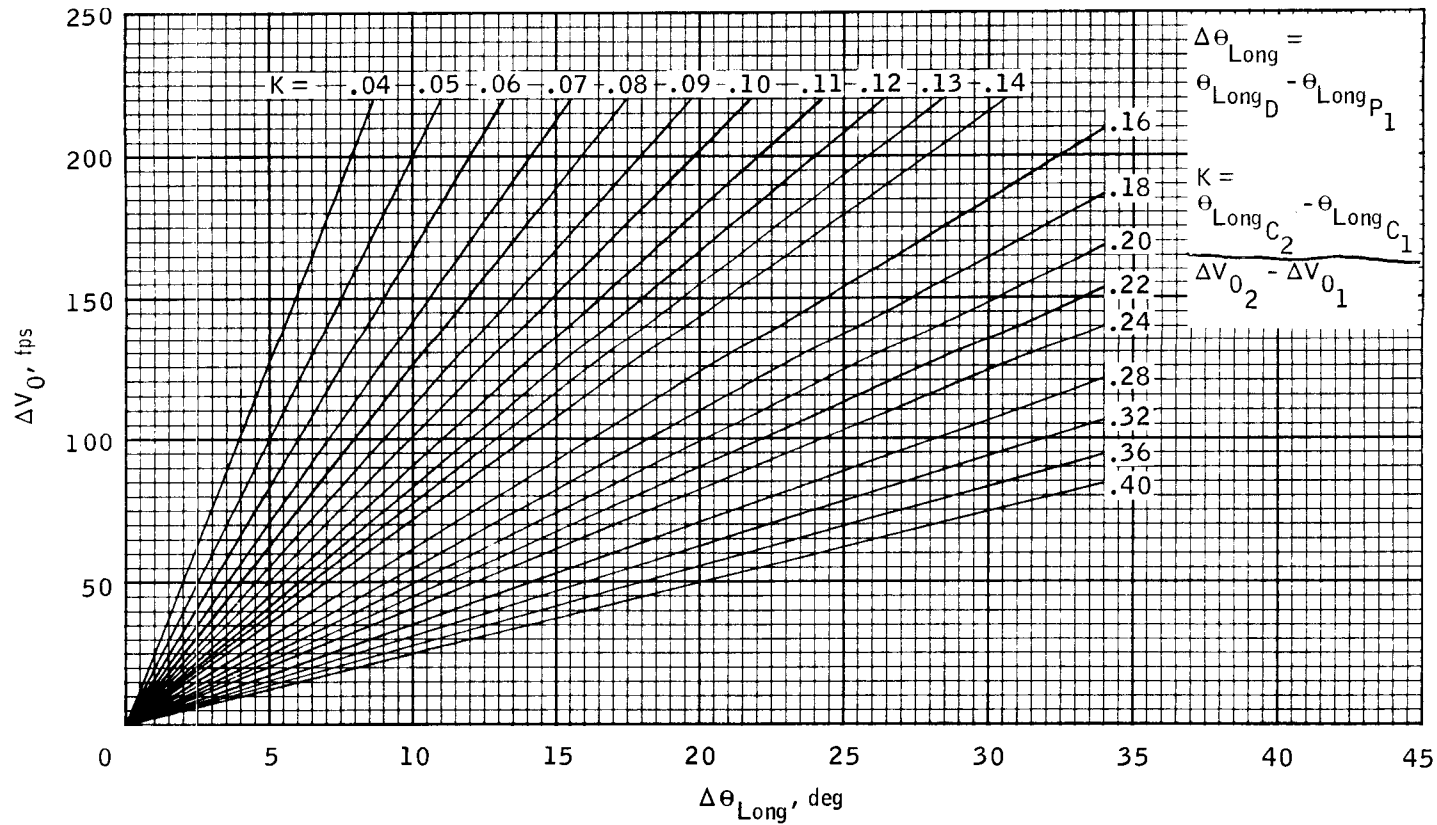
Crew chart 7. - LOI mode III abort curves, CSM only.

Bell/OMAB/MPAD  
3/31/69



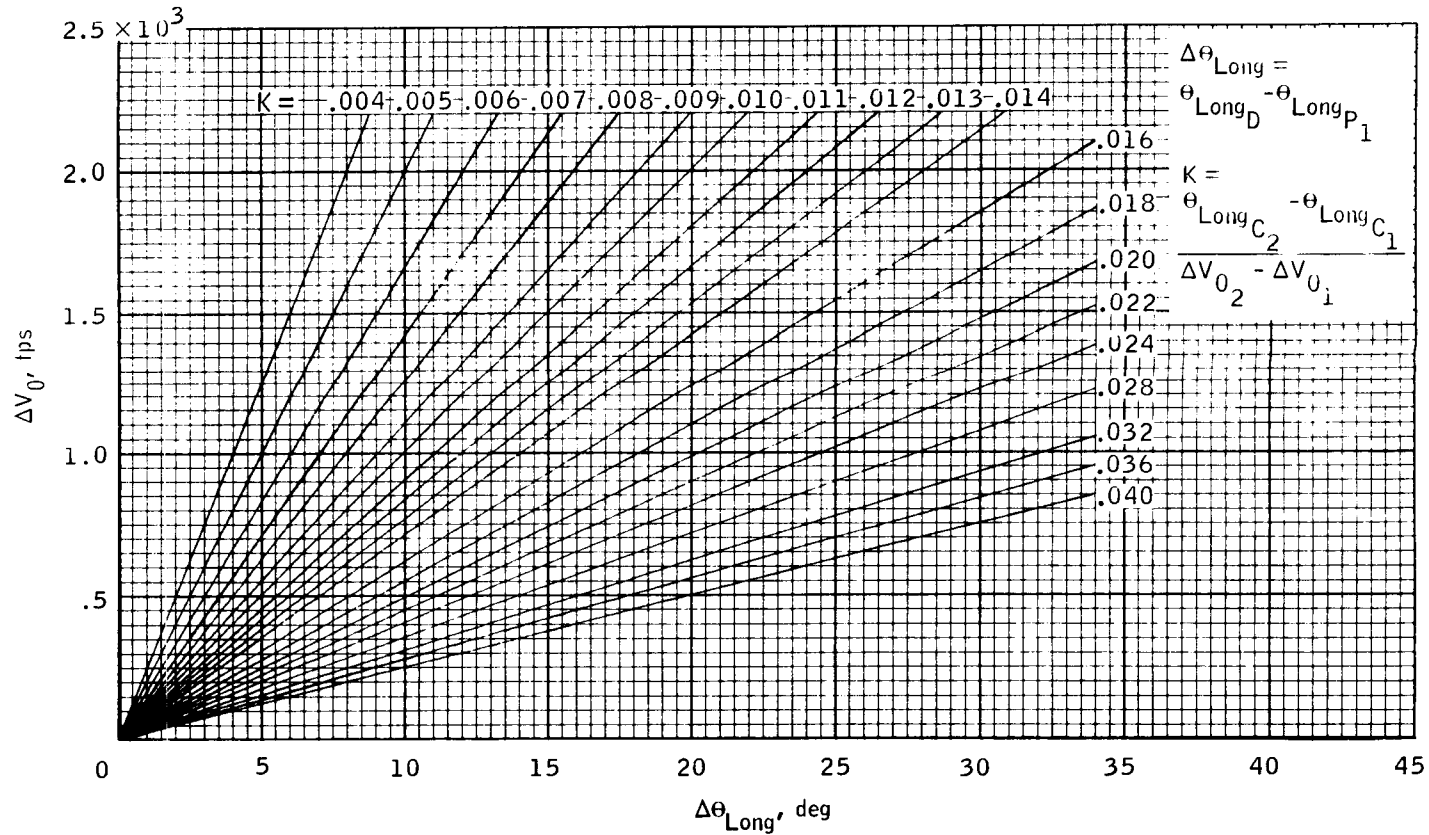
Crew chart 8. - LM PDI abort maneuver.

Yencharis/LMAB/MPAD  
3/31/69



Crew chart 9. -  $\Delta V_0$  versus  $\Delta \theta_{Long}$ ,  $K = .4$  to  $.04$ .

Yenciaris LMAB/MPAD  
3/31/69



Crew chart 10.-  $\Delta V_0$  versus  $\Delta \theta_{Long}$ ,  $K = .04$  to  $.004$ .

Yencharis/LMAB/MPAD  
4/29/69

Crew chart 11. - P37 return to earth program - corridor control.

1A

V37E 37E  
F 06 33 TIG (hrs, min, .01 sec)  
Load desired TIG  
PRO

2 F 06 60

BLANK, ΔV DESIRED, GAMMA EI DESIRED (1/1000 .01)  
Check desired values  
R2 00000 (MIN ΔV)  
R3 00000 (ENTRY ON TARGET LINE)  
PRO

\* F 05 09 00612 STaTz Vector  
\* IN LUNAR  
\* INFLUENCE  
\* 00605 Solution not  
\* CONVERGENT  
\* 00607 Conic Routine  
\* Failed  
\* 00610 STaTz vector  
\* is below 400K  
\* ft ALTITUDE  
\* V32 E, RSET TO 1

## PAGE 2A

- 3 F 06 61 IMPACT LAT, IMPACT LONG (.01°)  
 (RECYCLE) V32E TO 1  
 PRO
- 4 F 06 39 ΔT TRANSFER (hrs, min, .01 sec)  
 (RECYCLE) V32E TO 1  
 PRO
- 5 F 06 60 BLANK, VPRED, GAMMA EI (fps, .01°)  
 (RECYCLE) V32E TO 1  
 PRO
- 6 F 06 81 ΔVXYZ (LV) ΔT TIG (.1 fps)  
 (OPTION) V06E 40E ΔV MAG. available in N40  
 and N80  
 PRO (To 3 on first pass.)  
 \* F 05 09 00605 Solution not  
 \* Convergent  
 \* 00613 FLT. Path Angle  
 \* 00607 not reached  
 \* RSET CONIC ROUTINE  
 \* V32E TO 1 FAILED
- 7 F 04 06 THRUST OPTION



PAGE 3A

R1 00007

R2 0000X

X = 1 (SPS)

2 (RCS)

PRO (IF R03 HAS BEEN COMPLETED)

8 F 06 33

TIG

(has, min, .01 sec)

PRO

9 F 16 45

MARK, TFI, MGA

(mark, min-sec, .01")

PRO (MGA set To -00002 IF NO

REFSMMAT SET)

10 F 37

(40E OR 41E)

## PAGE 18

P37 RETURN TO EARTH PROGRAM - LONGITUDE CONTROL  
 (CANNOT USE WHEN TIME TO ENTRY IS < 4 HRS)

18 V37E 37E  
 F 06 33 TIG (hrs, min, .01 sec)  
 Load desired TIG  
 PRO

2 F 06 60 BLANK,  $\Delta V$  DESIRED, GAMMA EI DESIRED ( $1/\text{fs}, .01^\circ$ )  
 Load desired  $\Delta V$  ~~XXXXXXXXXX~~  
 Load  $\frac{\text{PAD } \Delta V}{\text{XXXXXXXXXX}}$  if on TLC  
 Load 0. fps if on TEC  
 R2 XXXXX  
 PRO

\* F 05 09 00612 State vector in  
 \* Lunar Influence  
 \* 00605 Solution not  
 \* Convergent  
 \* 00607 Conic Routine Failed  
 \* 00610 State vector is  
 \* below 400K ft  
 \* altitude  
 \* V32E, RSET TO 18

PAGE 28

3 F 06 61 IMPACT LAT, IMPACT LONG (.01°)  
 (RECYCLE IF LONG IS NOT WITHIN 30° OF  
 DESIRED. INCREASE  $\Delta V$  DESIRED TO OBTAIN A  
 MORE EASTERLY LONG, DECREASE TO OBTAIN MORE  
 WESTERLY) V32 E TO 1B  
 PRO (AFTER RECORDING LONG AS  $\theta_c$ )

4 F 06 39 AT TRANSFER (hrs, min, .01sec)  
 PRO

5 F 06 60 BLANK, VPRED, GAMMA EI (fps, .01°)  
 PRO

6 F 06 81  $\Delta V$ XYZ (LV) AT TIG  
 PRO

\* F 05 09 00605 Solution not  
 \* Convergent  
 \* 00613 FLT. Path Angle  
 \* not reached  
 \* 00607 Conic Routine  
 \* Failed  
 \* RSET  
 \* V32 E TO 1B

PAGE 3B

- 7 F 06 61 IMPACT LAT, IMPACT LONG (.01°)  
Record LONG as  $\theta_p$ ,  
PRO
- 8 F 06 39  $\Delta T$  TRANSFER  
PRO
- 9 F 06 60 BLANK, VPRED, GAMMA EI (fps, .01°)  
PRO
- 10 F 06 81  $\Delta VXYZ(LV)$  AT TIG  
V 06 E 40E  
R2 xxxxx Record as  $\Delta V_0$ ,  
(Check To see if  $\theta_p$  is an acceptable  
LONG. IF IT IS V32E TO 1A OF  
CORRIDOR CONTROL CHECKLIST AND  
LOAD  $\Delta V_0$  IN R2)  
V32 E TO 11
- 11 F 06 33 TIG (has, min, .01 sec)  
load same value used initially  
PRO
- 12 F 06 60 BLANK,  $\Delta V$  DESIRED, GAMMA EI DESIRED (1fps, .01°)

PAGE 48

Load a desired  $\Delta V$  \* 100 fps greater  
 Than or less Than  $\Delta V_0$ , recorded above  
 and record value as  $\Delta V_{02}$  ( $\Delta V_{02}$   
 must be nonzero)

R2 XXXXX

PRO

\* F 05 09 SAME AS IN 2

\* V32E, RSET TO #1

13 F 06 61 IMPACT LAT, IMPACT LONG (.01°)  
 Record LONG as  $\Theta_{c2}$   
 PRO

14 F 06 39 AT TRANSFER  
 PRO

15 F 06 60 BLANK, VPRED, GAMMA EI  
 PRO

16 F 06 81  $\Delta V_{XYZ}(LV)$  at TIG  
 V06E 40E  
 R2 XXXXX ( $\Delta V$  MAG)

PAGE 5B

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IF value in R2 is equal To  $\Delta V_{o_2} \pm 2. \text{fps}$   
 use crewchart To find  $\Delta V_o$  after  
 computing K and  $\Delta \Theta_{\text{LONG}}$  WHERE

$\Delta V_{o_1}$  is from step 10

$\Theta_{c_1}$  is from step 3

$\Theta_{p_1}$  " " " 7

$\Delta V_{o_2}$  " " " 12

$\Theta_{c_2}$  " " " 13

$\Theta_{\text{LONG}_D}$  is The desired LONG

V32E TO 1A OF CORRIDOR CONTROL

CHECKLIST WITH  $\Delta V$  DESIRED =

$\Delta V_{o_1} \pm \Delta V_o$  LOADED INSTEAD OF 0.

(IF VALUE IN R2 IS NOT EQUAL TO  
 $\Delta V_{o_2}$ ) PRO

18 F 06 61

IMPACT LAT, IMPACT LONG

(01°)

IF LONG WAS OVERSHOT, RECYCLE WITH

$|\Delta V_{o_1} - \Delta V_{o_2}| < 100 \text{ fps}$  V32E TO 11

PAGE 6B

IF LONG WAS NOT REACHED, P37 HIT  
CONSTRAINT. LONG IS NOT ATTAINABLE  
V32E TO IB AND TRY DIFFERENT TIG.

## Loss of Communications Navigation Procedures

1. TL+4 hours abort (detailed schedules provided for 72.1 and 108.2 injections)

- a. Make abort burn
- b. Re-initialize W-matrix
- c. Initiate sighting as soon as possible after abort following the schedule given in the crew chart.

(1.) The horizontal lines represented the start of the sighting intervals.

(2.) The vertical lines represent stars which are available for use with P23.

(3.) The numbers adjacent to the vertical lines are the required sightings with the given star.

(4.) Only earth horizon marks will be made.

d. Two charts are provided for each launch day; one is for a short return time using the 72.1 injection (approximately 19 hours or less), the second for longer returns using the 108.2 injection (19 hours or greater). Targets for aborts from other injection opportunities are nearly identical to these schedules with variations in star AOS and LOS.

2. LO aborts (detailed schedules provided)

- a. The first and last 17 hours of the schedule should not be changed.
- b. The data in the middle of the TE leg may be moved around for rest periods and MCC's.

c. Change to EI chart at EI-40

d. The key for the detailed schedule is:

Vertical Solid Line: Star/Horizon combination available for earliest TLI (72°, 1st opportunity).

Vertical Dashed Line: Star/Horizon combinations available for latest TLI (108°, 2nd opportunity).

Horizontal Solid Line: Sighting interval.

N: N sets of 3 marks on this star/horizon or star/landmark combination.

3. General TE optical navigation rules

a. A sighting is to consist of three marks.

b. A sighting interval is to consist of at least three star/horizon sightings; although as many as five are advisable (five should be used at the end of every sleep period). Observations using stars in the orbit plane should be emphasized. One sighting using an out-of-plane star (angle  $\geq 45$  degrees to the orbit plane) in every five sets is sufficient. If only three stars are grouped together, all stars should be in plane.



### 3. General TE optical navigation rules, cont'd.

c. The navigation sighting intervals should be scheduled so that, immediately following a period of length  $\Delta t$ , not to exceed 3 hours in a non-PTC mode, five times  $\Delta t$  should be spent in a PTC mode (thermal constraints), provided it does not interfere with navigation sightings which are essential for a safe entry.

d. The sextant calibration routine will be exercised at least every half hour while navigation sightings are in progress. The sextant calibration will be repeated until agreement of at least two checks (not necessarily sequential ones) are within 0.003 degree.

e. If an abort burn is performed during translunar coast, the W-matrix will be reinitialized to its launch value of 3,300 feet and 3.3 feet per second for onboard processing of the transearth sighting data. Navigation sightings intervals will be scheduled every 2.5 hours, and only star/earth horizon sightings should be made. The last sighting will be scheduled just after the last midcourse correction at EI-3 hours.

f. The transearth navigation sighting schedule in the flight plan is designed for a 54-hour return trajectory. In the event that the return time is altered (i.e., early TLI because of a communication loss, etc.) the following rules are to be followed for setting up a navigation schedule which will ensure a safe entry:

#### (1.) TEI through TEI+17

The nominal schedule is to be adhered to from TEI to TEI+17. The first two batches of sightings are to be on the moon, and the second two batches are to be on the earth. They are scheduled at TEI+1:30, TEI+12:30, TEI+13:30, and TEI+16:00 hours. The corresponding sightings are shown in the flight plan.

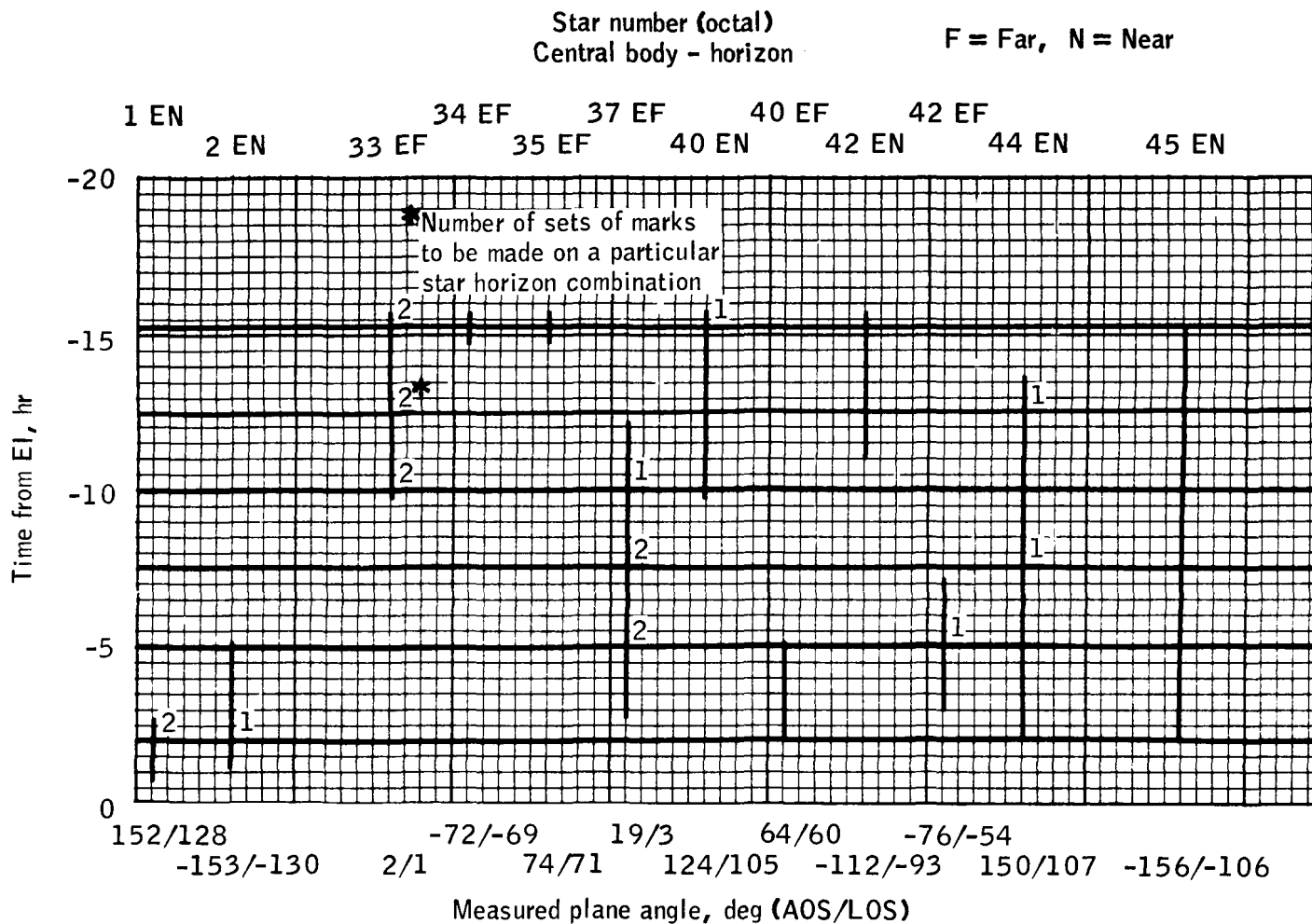
#### (2.) EI-17 through EI

The nominal schedule is also to be adhered to from EI-17 to EI. The navigation sightings are scheduled at EI-16, EI-11:20, EI-10:20, EI-7:40, EI-5, and EI-2:20. The corresponding central body for the star/horizon sightings is shown in the flight plan.

#### (3.) TEI+17 through EI-17

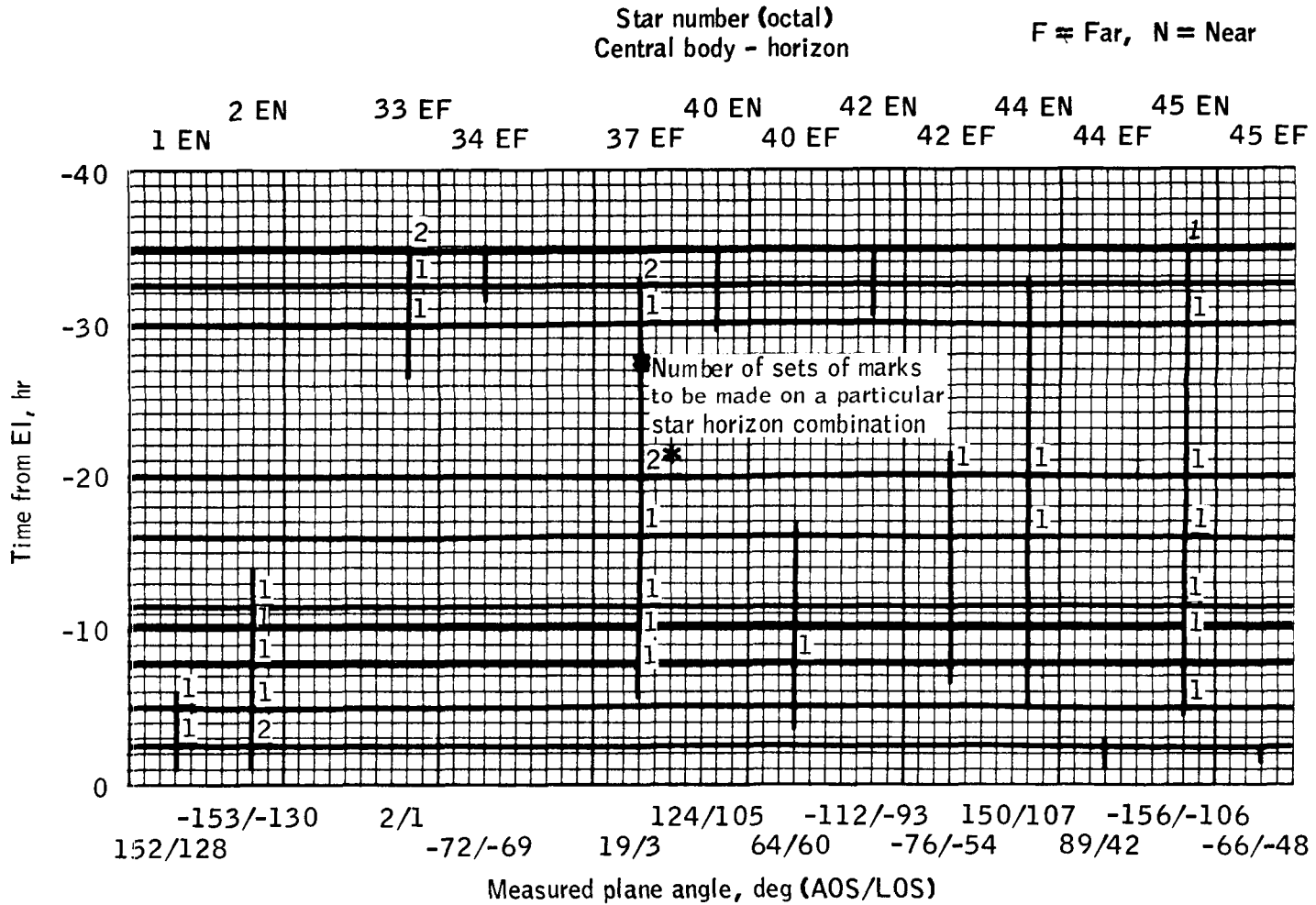
Between TEI+17 and EI-17 schedule two-thirds as many sightings as there are hours of coast during this period. Sightings should be scheduled in a ratio of 2 to 1, earth to moon, with a minimum of 17 sightings during this coast period (i.e., if the time between TEI+17 and EI-17 is less than 25.5 hours, 17 sightings will be required).

Denham/MPB/MPAD  
4/30/69



Crew chart 12.- Detailed sighting schedule for aborts at TLI + 4 hr for a May 18, 1969, launch (15.5 hr return).

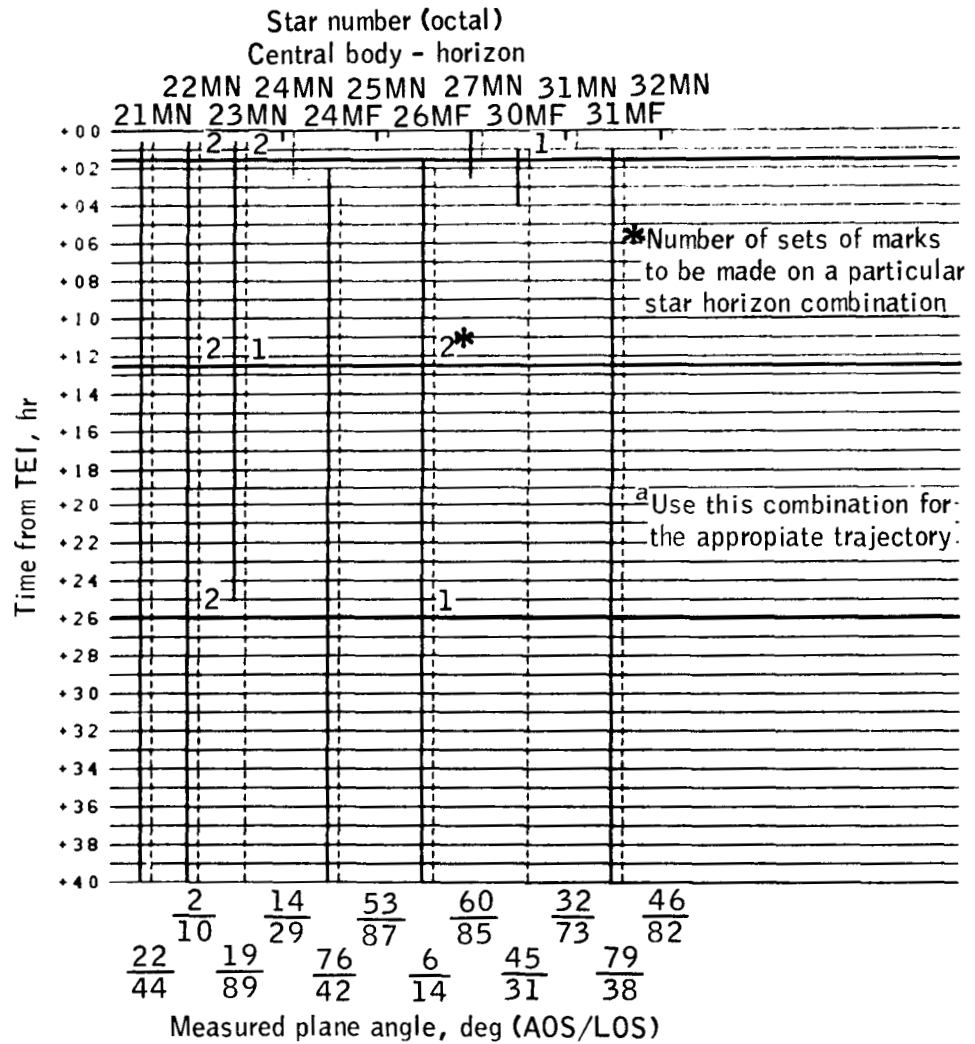
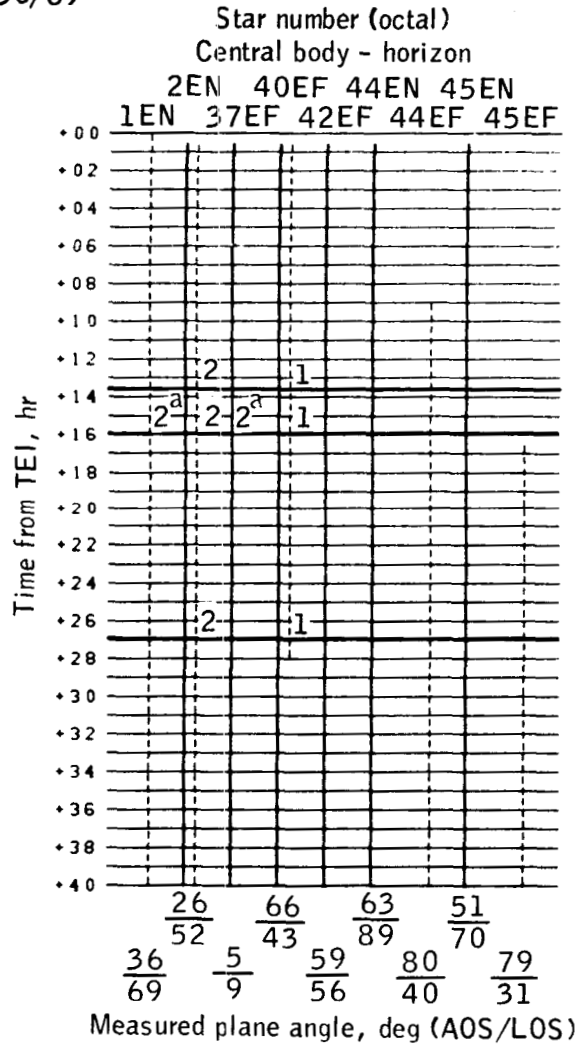
Denham/MPB/MPAD  
4/30/69



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Crew chart 13.- Detailed sighting schedule for aborts at TLI + 4 hr for a May 18, 1969, launch (greater than a 15.5 hr return).

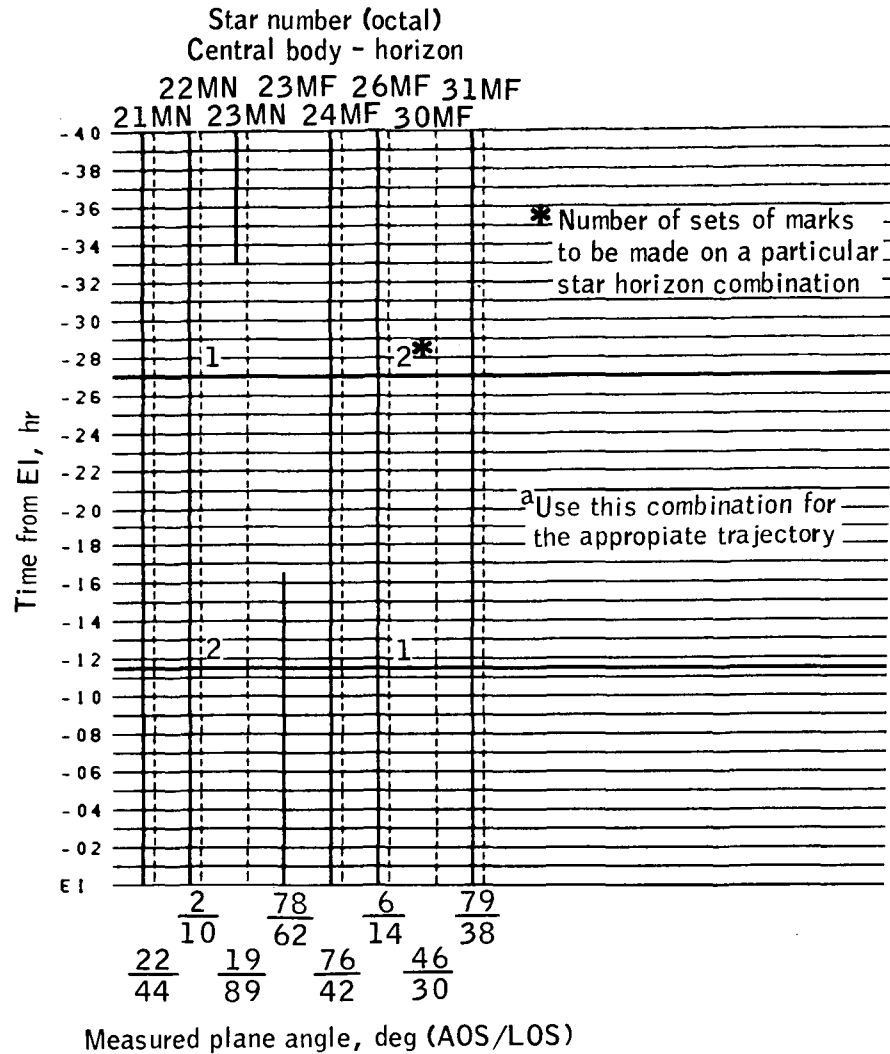
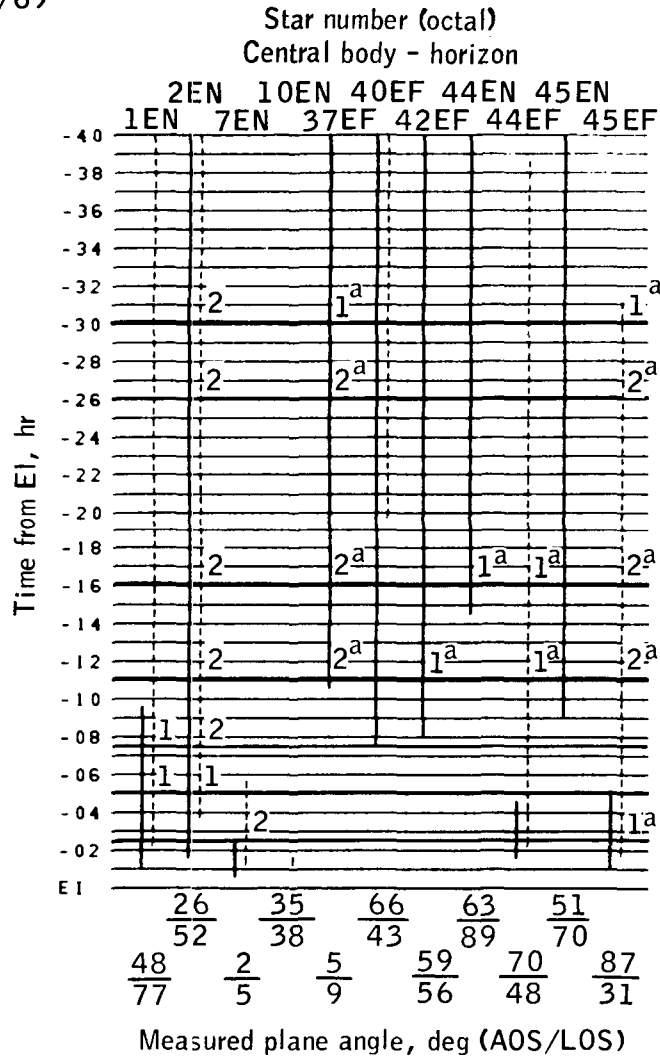
Denham/MPB/MPAD  
4/30/69



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Crew chart 14.- Detailed sighting schedule for aborts from lunar orbit after rev 17 for a May 18, 1969, launch (TEI to TEI plus 40 hr).

Denham/MPB/MPAD  
4/30/69



Crew chart 15.- Detailed sighting schedule for aborts from lunar orbit after rev 17 for a May 18, 1969, launch (EI minus 40 hr to EI).

Planet half-unit vectors.  
Blucker/MPB  
3/31/69

Crew chart 16.- Planet half-unit vectors.

PLANET = VENUS		HOURS FROM FIRST RECORDED	VECTOR FROM POINT K = .50			MEAN APP.	RT. ASC.			DECL.		
TIME (GMT)	HR		X	Y	Z		HR	MIN	SECOND	DEG	MIN	SECOND
69	5 18 16	.0	.48048	.12044	.05178	0	59	22.731	5	52	37.721	
						0	59	22.850	5	52	41.212	
69	5 18 2	10.0	.47986	.13048	.05212	1	0	20.093	5	54	46.639	
						1	0	20.221	5	54	50.226	
69	5 18 12	20.0	.47926	.13255	.05246	1	1	18.228	5	57	3.136	
						1	1	18.363	5	57	6.820	
69	5 18 22	30.0	.47864	.13462	.05282	1	2	17.121	5	59	27.087	
						1	2	17.265	5	59	30.870	
69	5 19 8	40.0	.47800	.13671	.05320	1	3	16.761	6	1	58.371	
						1	3	16.913	6	2	2.253	
69	5 19 18	50.0	.47735	.13882	.05358	1	4	17.136	6	4	36.863	
						1	4	17.296	6	4	40.846	
69	5 20 4	60.0	.47669	.14093	.05398	1	5	18.234	6	7	22.445	
						1	5	18.402	6	7	26.528	
69	5 20 14	70.0	.47601	.14306	.05439	1	6	20.044	6	10	14.993	
						1	6	20.220	6	10	19.176	
69	5 21 0	80.0	.47531	.14520	.05481	1	7	22.554	6	13	14.390	
						1	7	22.737	6	13	18.672	
69	5 21 10	90.0	.47460	.14736	.05525	1	8	25.753	6	16	20.516	
						1	8	25.944	6	16	24.897	
69	5 21 20	100.0	.47387	.14952	.05569	1	9	20.631	6	19	33.255	
						1	9	29.829	6	19	37.732	
69	5 22 6	110.0	.47312	.15170	.05615	1	10	34.177	6	22	52.489	
						1	10	34.381	6	22	57.061	

PLANET = VENUS

TIME (GMT)				HOURS FROM	VECTOR FROM POINT K = .50			RT, ASC.			DECL.			
YR	MO	DA	HR	FIRST RECORDED	X	Y	Z	HR	MN	SECOND	DEG	MN	SECOND	
69	5	22	16	120.0	.7235	.15388	.05661	MEAN	1	11	39.382	6	26	18.102
								APP.	1	11	39.591	6	26	22.767
69	5	23	2	130.0	.47158	.15508	.05709	MEAN	1	12	45.234	6	29	49.980
								APP.	1	12	45.449	6	29	54.736
69	5	23	12	140.0	.47078	.15629	.05758	MEAN	1	13	51.724	6	33	28.009
								APP.	1	13	51.945	6	33	32.653
69	5	23	22	150.0	.46997	.16051	.05808	MEAN	1	14	58.843	6	37	12.077
								APP.	1	14	59.068	6	37	17.007
69	5	24	8	160.0	.46014	.16274	.05860	MEAN	1	16	6.582	6	41	2.072
								APP.	1	16	6.811	6	41	7.084
69	5	24	18	170.0	.46829	.16498	.05912	MEAN	1	17	14.931	6	44	57.883
								APP.	1	17	15.164	6	45	2.975
69	5	25	4	180.0	.46742	.16723	.05966	MEAN	1	18	23.881	6	48	59.400
								APP.	1	18	24.118	6	49	4.570
69	5	25	14	190.0	.46654	.16949	.06020	MEAN	1	19	33.425	6	53	6.516
								APP.	1	19	33.665	6	53	11.760
69	5	26	0	200.0	.46563	.17176	.06076	MEAN	1	20	43.553	6	57	19.122
								APP.	1	20	43.796	6	57	24.437
69	5	26	10	210.0	.46471	.17404	.06133	MEAN	1	21	54.258	7	1	37.112
								APP.	1	21	54.504	7	1	42.497
69	5	26	20	220.0	.46377	.17633	.06192	MEAN	1	23	5.532	7	6	.380
								APP.	1	23	5.780	7	6	5.833
69	5	27	6	230.0	.46281	.17863	.06251	MEAN	1	24	17.366	7	10	28.822
								APP.	1	24	17.618	7	10	34.341

PLANET = VENUS

TIME (GMT)				HOURS FROM FIRST RECORD	VECTOR FROM POINT K = .50			MEAN APP.	RT. ASC.			DECL.			
YR	MO	DA	HR		X	Y	Z		HR	NN	SECOND	DEG	NN	SECOND	
69	5	27	16	240.0	.46082	.18093	.06312	1 25	29.755	7 15	2,334	1 25	30.009	7 15	7,919
69	5	28	2	250.0	.46082	.18327	.06374	1 26	42.689	7 19	40,814	1 26	42.947	7 19	46,464
69	5	28	12	260.0	.45980	.18061	.06437	1 27	56.164	7 24	24,160	1 27	56.425	7 24	29,876
69	5	28	22	270.0	.45875	.18796	.06502	1 29	10.170	7 29	12,271	1 29	10.436	7 29	18,054
69	5	29	8	280.0	.45768	.19032	.06568	1 30	24.703	7 34	5,047	1 30	24.973	7 34	10,899
69	5	29	18	290.0	.45659	.19270	.06635	1 31	39.755	7 39	2,389	1 31	40.031	7 39	8,313
69	5	30	4	300.0	.45547	.19509	.06703	1 32	55.320	7 44	4,197	1 32	55.602	7 44	10,197
69	5	30	14	310.0	.45433	.19749	.06773	1 34	11.392	7 49	10,375	1 34	11.682	7 49	16,454
69	5	31	0	320.0	.45317	.19990	.06844	1 35	27.966	7 54	20,824	1 35	28.263	7 54	26,987
69	5	31	10	330.0	.45198	.20233	.06917	1 36	45.034	7 59	35,447	1 36	45.340	7 59	41,698
69	5	31	20	340.0	.45076	.20477	.06991	1 38	2.592	8 4	54,147	1 38	2.906	8 5	,490
69	6	1	6	350.0	.44952	.20723	.07067	1 39	20.634	8 10	16,828	1 39	20.957	8 10	23,266



PLANET = VENUS				HOURS FROM FIRST RECORD	VECTOR FROM POINT K = .50				RT. ASC.			DECL.		
YR	MO	DA	HR		X	Y	Z		HR	MIN	SECOND	DEG	MIN	SECOND
69	6	1	16	360.0	.44825	.20970	.07143	APP.	1 40	39.154	8 15	43.392		
									1 40	39.487	8 15	49.929		
69	6	2	2	370.0	.44696	.21218	.07221	MEAN	1 41	58.147	8 21	13.745		
								APP.	1 41	58.480	8 21	20.383		
69	6	2	12	380.0	.44565	.21468	.07301	MEAN	1 43	17.607	8 26	47.788		
								APP.	1 43	17.959	8 26	54.528		
69	6	2	22	390.0	.44428	.21719	.07382	MEAN	1 44	37.530	8 32	25.427		
								APP.	1 44	37.891	8 32	32.269		
69	6	3	8	400.0	.44290	.21971	.07464	MEAN	1 45	57.910	8 38	6.566		
								APP.	1 45	58.279	8 38	13.509		
69	6	3	18	410.0	.44149	.22225	.07547	MEAN	1 47	18.741	8 43	51.108		
								APP.	1 47	19.118	8 43	58.150		
69	6	4	4	420.0	.44006	.22480	.07632	MEAN	1 48	40.019	8 49	38.957		
								APP.	1 48	40.403	8 49	46.096		
69	6	4	14	430.0	.43859	.22736	.07717	MEAN	1 50	1.738	8 55	30.020		
								APP.	1 50	2.129	8 55	37.252		

PLANET = MARS

TIME (GMT)				HOURS FROM FIRST RECORD	VECTOR FROM POINT K = .50			RT. ASC.			DECL.			
YR	MO	DA	HR		X	Y	Z	HR	MN	SECOND	DG	MN	SECOND	
69	5	17	16	0.0	-.13593	-.43711	-.20117	MEAN	16	50	51.949	-23	43	23.707
								APP.	16	50	54.600	-23	44	6.459
69	5	18	12	20.0	-.13790	-.43642	-.20131	MEAN	16	49	56.107	-23	45	11.128
								APP.	16	49	58.779	-23	45	23.938
69	5	19	8	40.0	-.13993	-.43572	-.20145	MEAN	16	48	58.429	-23	46	25.068
								APP.	16	49	1.122	-23	46	37.949
69	5	20	4	60.0	-.14199	-.43498	-.20158	MEAN	16	47	58.988	-23	47	35.408
								APP.	16	48	1.701	-23	47	48.376
69	5	21	0	80.0	-.14410	-.43423	-.20170	MEAN	16	46	57.859	-23	48	42.039
								APP.	16	47	.591	-23	48	55.104
69	5	21	20	100.0	-.14622	-.43347	-.20183	MEAN	16	45	55.119	-23	49	44.854
								APP.	16	45	57.869	-23	49	58.026
69	5	22	16	120.0	-.14837	-.43268	-.20195	MEAN	16	44	50.855	-23	50	43.756
								APP.	16	44	53.619	-23	50	57.039
69	5	23	12	140.0	-.15052	-.43188	-.20206	MEAN	16	43	45.150	-23	51	38.654
								APP.	16	43	47.928	-23	51	52.047
69	5	24	8	160.0	-.15267	-.43107	-.20218	MEAN	16	42	38.098	-23	52	29.465
								APP.	16	42	40.886	-23	52	42.967
69	5	25	4	180.0	-.15481	-.43026	-.20229	MEAN	16	41	29.791	-23	53	16.120
								APP.	16	41	32.587	-23	53	29.724
69	5	26	0	200.0	-.15694	-.42943	-.20240	MEAN	16	40	20.326	-23	53	58.557
								APP.	16	40	23.128	-23	54	12.250
69	5	26	20	220.0	-.15905	-.42861	-.20250	MEAN	16	39	9.801	-23	54	36.725
								APP.	16	39	12.609	-23	54	50.495

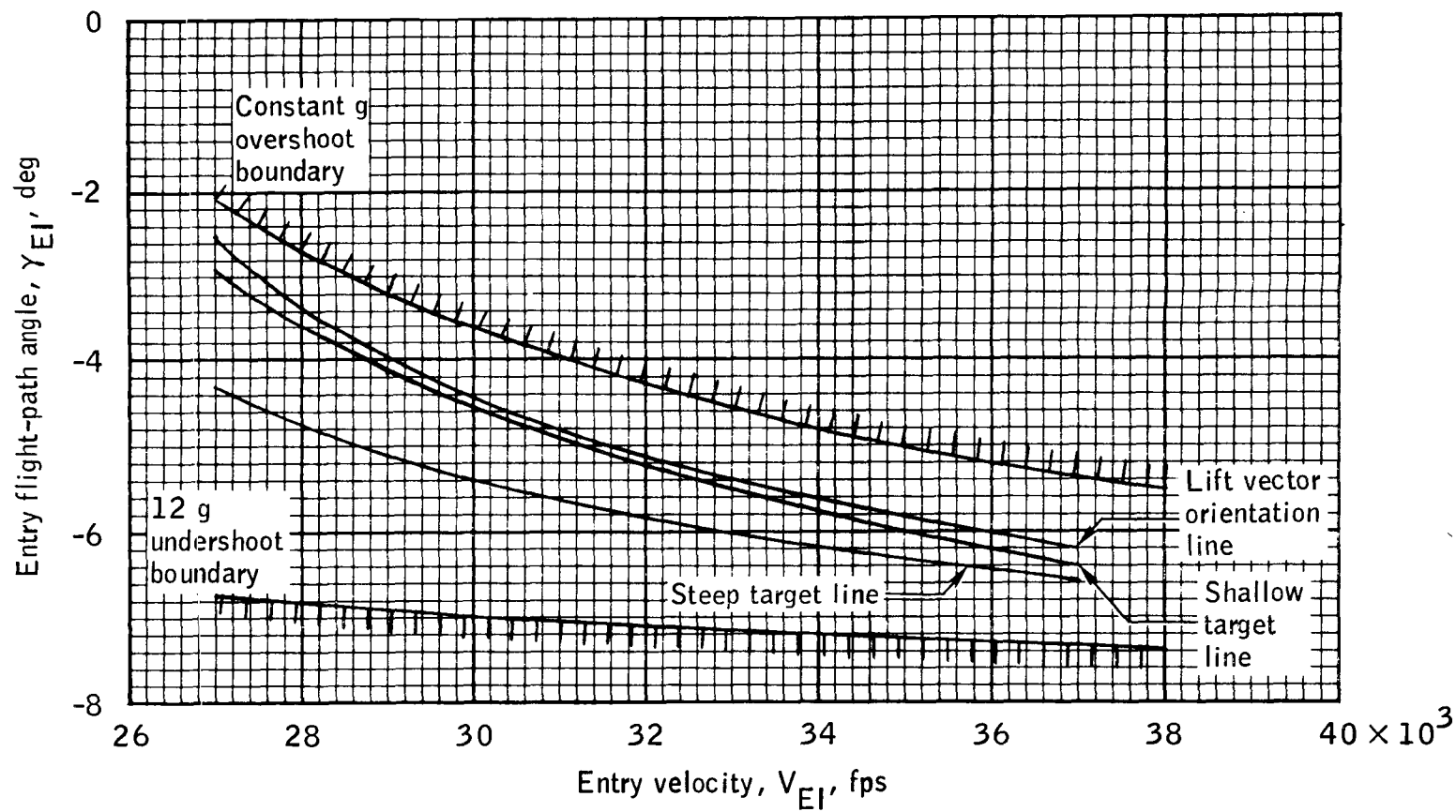
PLANET = MARS				HOURS FROM FIRST RECEFD	VECTOR FROM POINT K = ,50			MEAN APP.	RT, ASC.			DECL.		
TIME (GMT)	YR	MO	DA HR		X	Y	Z		HR	MN	SECOND	DG	MN	SECOND
69	5	27	16	240.0	-.16115	-.42778	-.20260	16	37	58.316	-23	55	10.586	
								16	38	1.130	-23	55	24.419	
69	5	28	12	260.0	-.16322	-.42694	-.20270	16	36	45.977	-23	55	40.112	
								16	36	48.797	-23	55	53.997	
69	5	29	8	280.0	-.16528	-.42610	-.20279	16	35	32.886	-23	56	5.289	
								16	35	35.714	-23	56	19.219	
69	5	30	4	300.0	-.16735	-.42526	-.20288	16	34	19.146	-23	56	26.115	
								16	34	21.985	-23	56	40.093	
69	5	31	0	320.0	-.16936	-.42442	-.20296	16	33	4.864	-23	56	42.601	
								16	33	7.718	-23	56	56.636	
69	5	31	20	340.0	-.17140	-.42357	-.20303	16	31	50.146	-23	56	54.773	
								16	31	53.015	-23	57	8.883	
69	6	1	16	360.0	-.17345	-.42270	-.20309	16	30	35.098	-23	57	2.675	
								16	30	37.984	-23	57	16.881	
69	6	2	12	380.0	-.17552	-.42183	-.20314	16	29	19.827	-23	57	6.366	
								16	29	22.732	-23	57	20.691	
69	6	3	8	400.0	-.17761	-.42093	-.20317	16	28	4.443	-23	57	5.929	
								16	28	7.364	-23	57	20.388	
69	6	4	4	420.0	-.17974	-.42002	-.20318	16	26	49.059	-23	57	1.463	
								16	26	51.991	-23	57	16.064	

PLANET = JUPITER				VECTOR FROM POINT K = .50			RT, ASC,			DECL,				
TIME (GMT)				HOURS FROM			HR MN SECOND			DG MN SECOND				
YR	MO	DA	HR	FIRST RECCFD	X	Y	Z							
69	5	17	16	0	-.49870	.02591	.02508	MEAN	11	48	9.519	2	52	2.001
								APP.	11	48	11.316	2	51	51.449
69	5	26	0	200.0	-.49870	.02622	.02489	MEAN	11	47	57.987	2	51	7.900
								APP.	11	47	59.718	2	50	57.809
69	6	3	8	400.0	-.49881	.02487	.02398	MEAN	11	48	32.376	2	45	14.026
								APP.	11	48	34.051	2	45	4.257

PLANET = SATURN

TIME (GMT)				HOURS FROM FIRST RECEFD	VECTOR FROM POINT K = .50			RT, ASC,			DECL,			
YR	MO	DA	HR		X	Y	Z	HR	MN	SECOND	DG	MN	SECOND	
69	5	17	16	.0	.42279	.25205	.08789	MEAN APP.	2 2	3 3	11.271 11.166	10 10	7 7	14.526 19.322
69	5	19	18	50.0	.42162	.25375	.08860	MEAN APP.	2 2	4 4	8.452 8.396	10 10	12 12	10.594 15.681
69	5	21	20	100.0	.42046	.25543	.08930	MEAN APP.	2 2	5 5	5.134 5.126	10 10	17 17	2.214 7.623
69	5	23	22	150.0	.41931	.25708	.08997	MEAN APP.	2 2	6 6	1.279 1.311	10 10	21 21	49.213 54.922
69	5	26	0	200.0	.41818	.25869	.09064	MEAN APP.	2 2	6 6	56.851 56.915	10 10	26 26	31.431 37.384
69	5	28	2	250.0	.41703	.26028	.09129	MEAN APP.	2 2	7 7	51.814 51.910	10 10	31 31	8.719 14.862
69	5	30	4	300.0	.41593	.26183	.09192	MEAN APP.	2 2	8 8	46.135 46.274	10 10	35 35	40.942 47.289
69	6	1	6	350.0	.41482	.26337	.09255	MEAN APP.	2 2	9 9	39.783 39.984	10 10	40 40	7.972 14.626
69	6	3	8	400.0	.41372	.26489	.09317	MEAN APP.	2 2	10 10	32.724 32.993	10 10	44 44	29.678 36.736

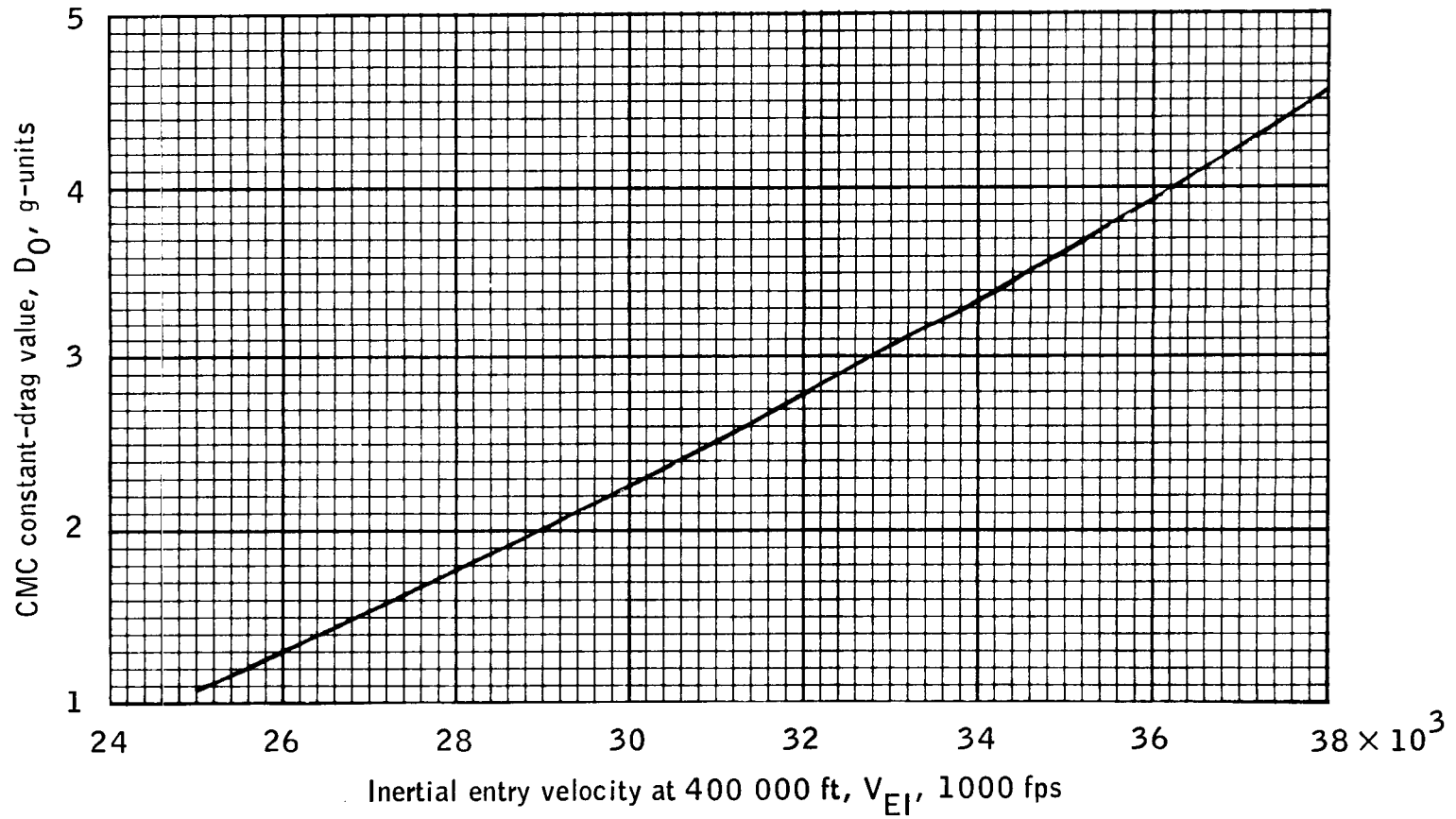
Burton/LAB/MPAD  
3/31/69



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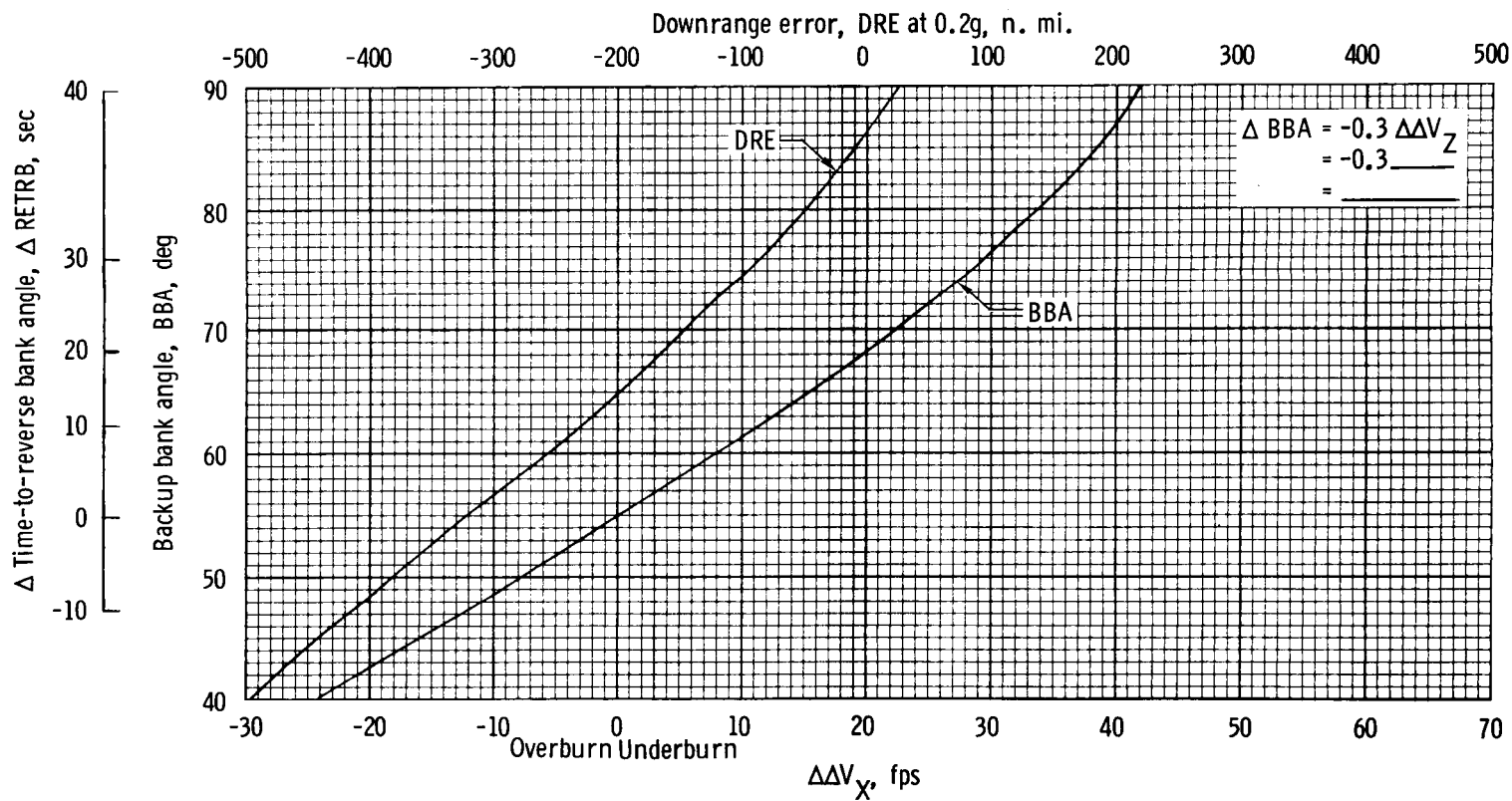
Crew chart 17.- Entry corridor.

Burton/LAB/MPAD  
3/31/69



Crew chart 18.- Command module computer constant-drag value.

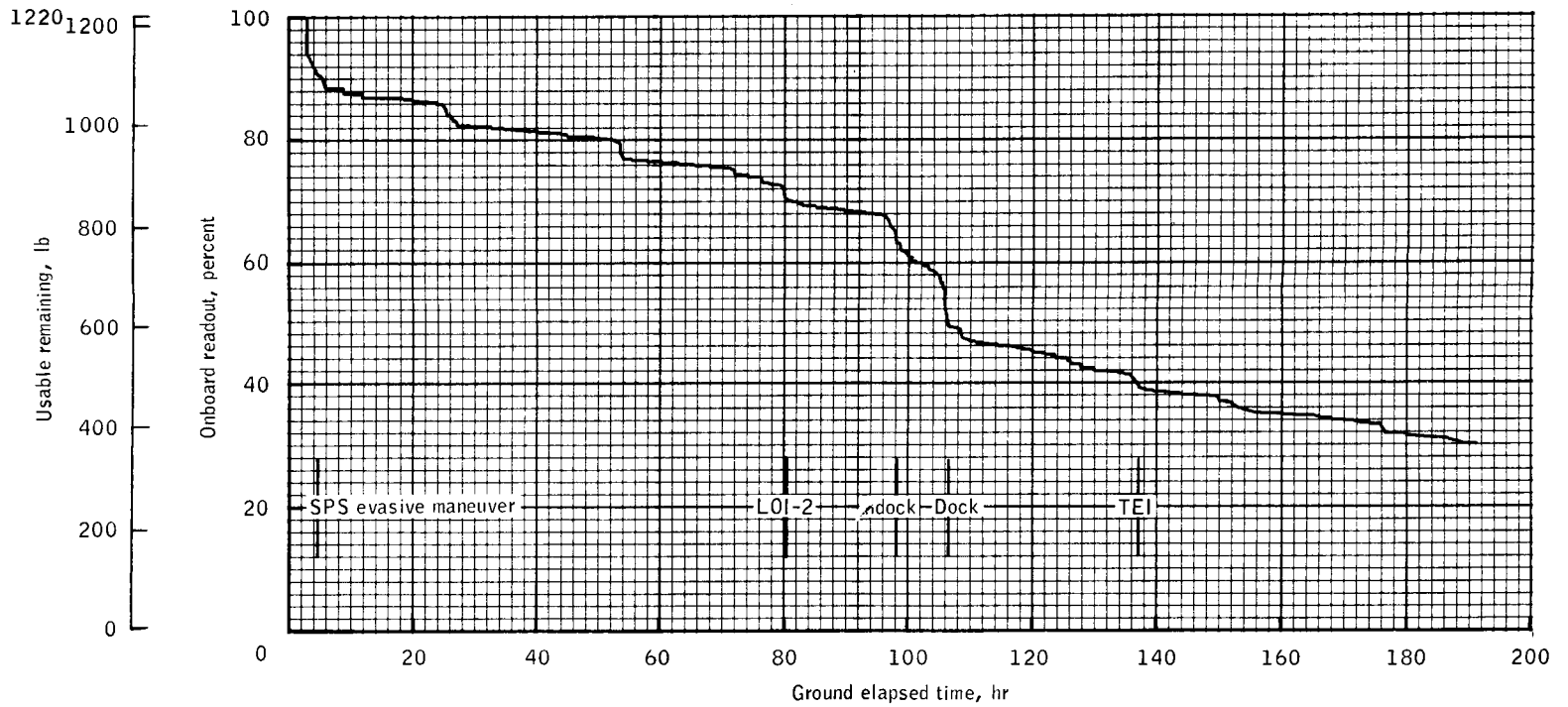
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Crew chart 19. - Earth orbit BBA versus  $\Delta\Delta V_x$ .



Loyd/GPB/MPAD  
5/5/69



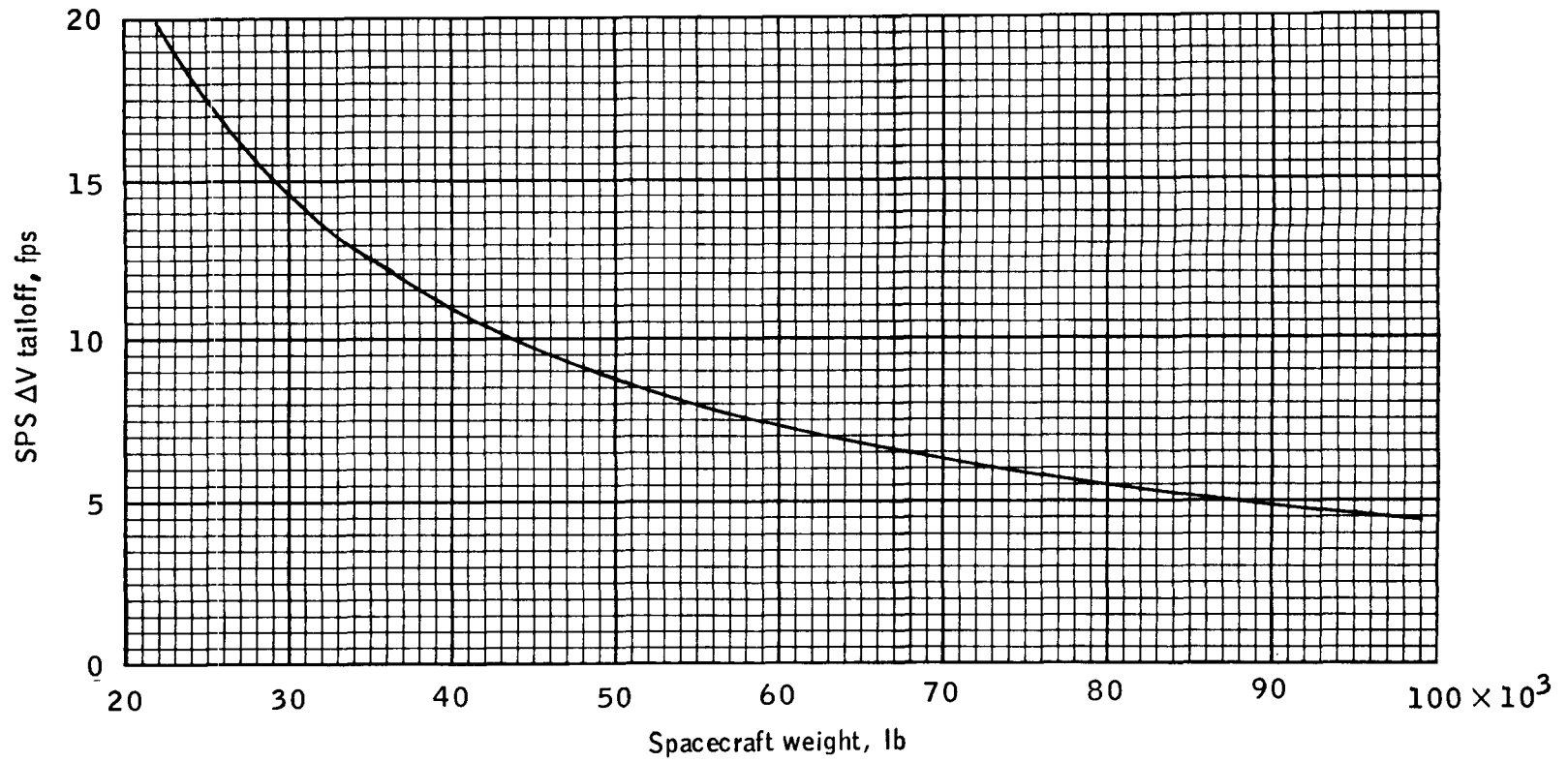
Crew chart 20.- SM RCS propellant profile (Total).

Mayfield/GPB/MPAD  
4/28/69

EVENT	SYSTEM A	SYSTEM B
Post DOI	96 %	94 %
Post phasing	93	89
Post insertion	85	82
Post CSI	79	75
Post CDH	75	71
Post TRI	69	65
Post braking	54	51
Post docking	51	47

Crew chart 21.- Onboard reading of LM RCS propellant remaining, percentage.

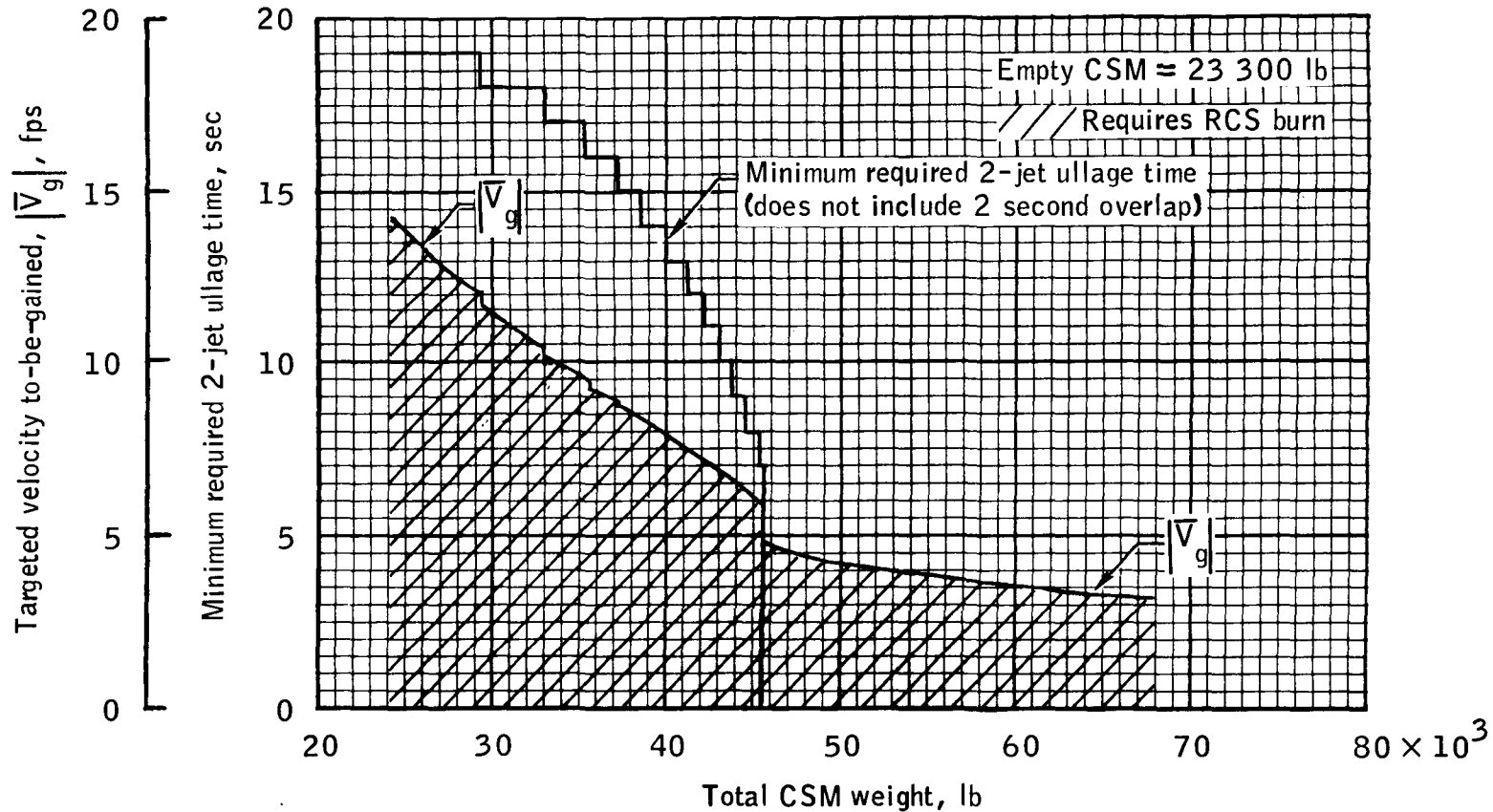
Graf/GPB/MPAD  
3/31/69



Crew chart 22.- SPS tailoff  $\Delta V$  versus spacecraft weight.

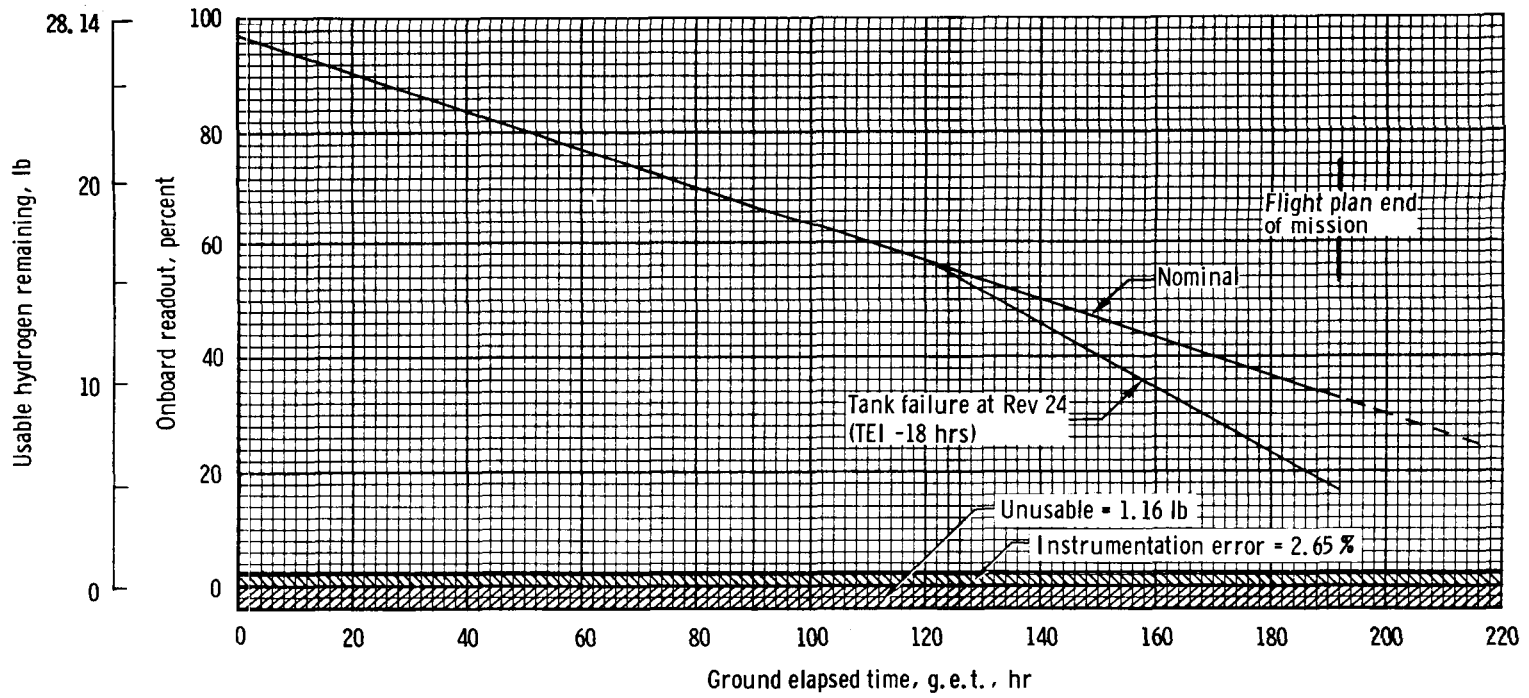
Graf/GPB/MPAD  
3/31/69

This chart assumes that the minimum desired SPS  
burn time is 0.5 sec. and that the ullage time is  
the minimum time shown on the chart.



Crew chart 23.- SPS versus RCS criteria, CSM alone - minimum pre-burn ullage.

Scott/GPB/MPAD  
4/30/69



Crew chart 24. - Hydrogen remaining in one tank.

Swalin/GPB/MPAD  
4/28/69

<u>Event</u>	<u>Ascent oxygen</u> <u>Tank 1</u>
Switch to ascent 1 O <sub>2</sub>	100 %
Post staging	97
Post insertion	95
Post CSI	86
Post CDH	74
Post TPI	67
Post braking	61
Post docking	53

Crew chart 25.- Onboard readout of ascent oxygen remaining, percentage