

## What is different about transition modeling?

- Many non-local and global parameters
- Interface region with turbulence model is weird
  - ➔ Lots of babies, less bathwater
- Less physics-based, more data-driven (by construction)
- Less theory guidance (e.g. can't hang our hats on homogeneous turbulence)
- Feature selection is harder, and more empirical/intuitive
- BUT, there is a much higher possibility of running DNS for most (all) regimes of interest

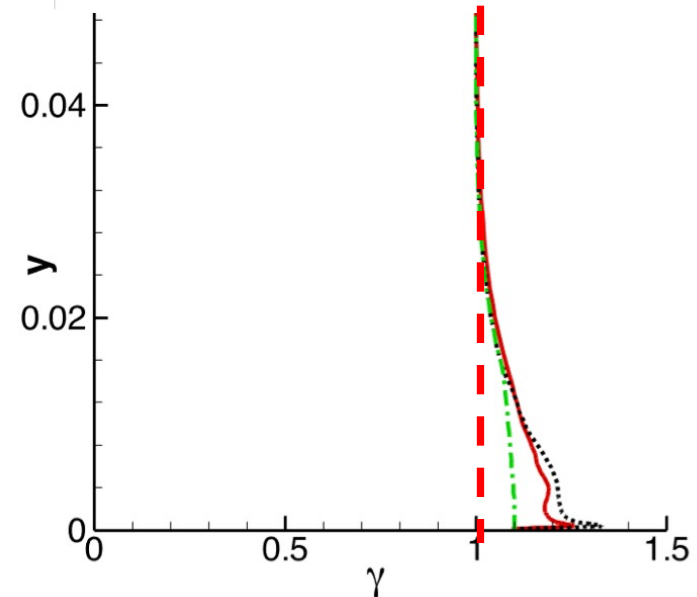
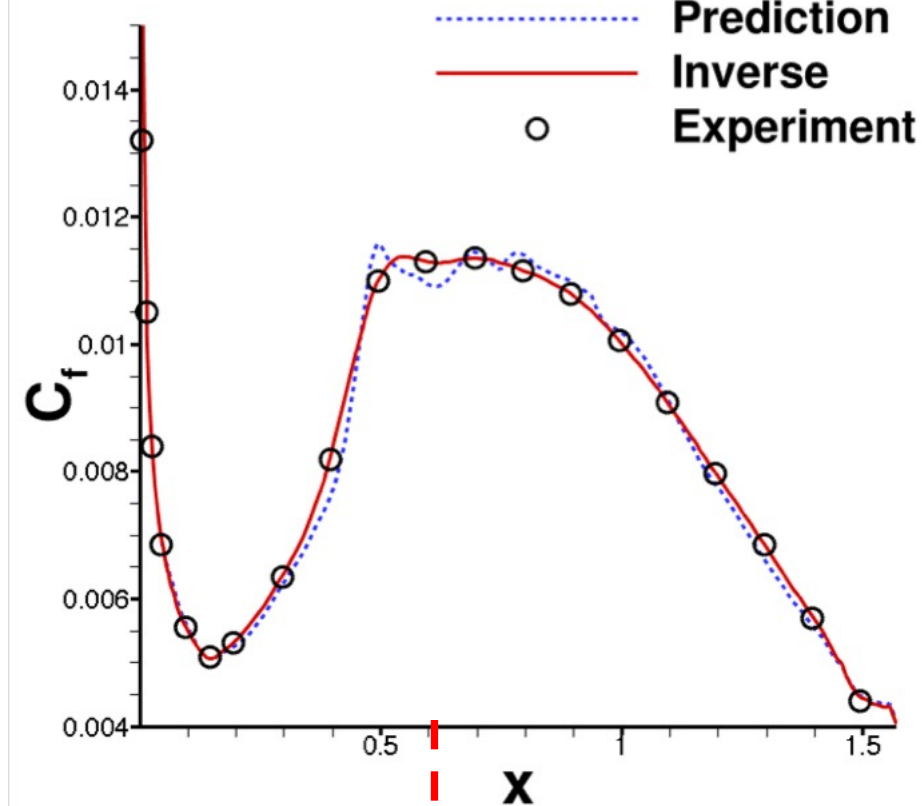
## A thought experiment

$$\frac{Dk}{Dt} = 2\nu_T |S|^2 \gamma - C_\mu k \omega + \partial_j \left[ \left( \nu + \frac{\nu_T}{\sigma_k} \right) \partial_j k \right]$$

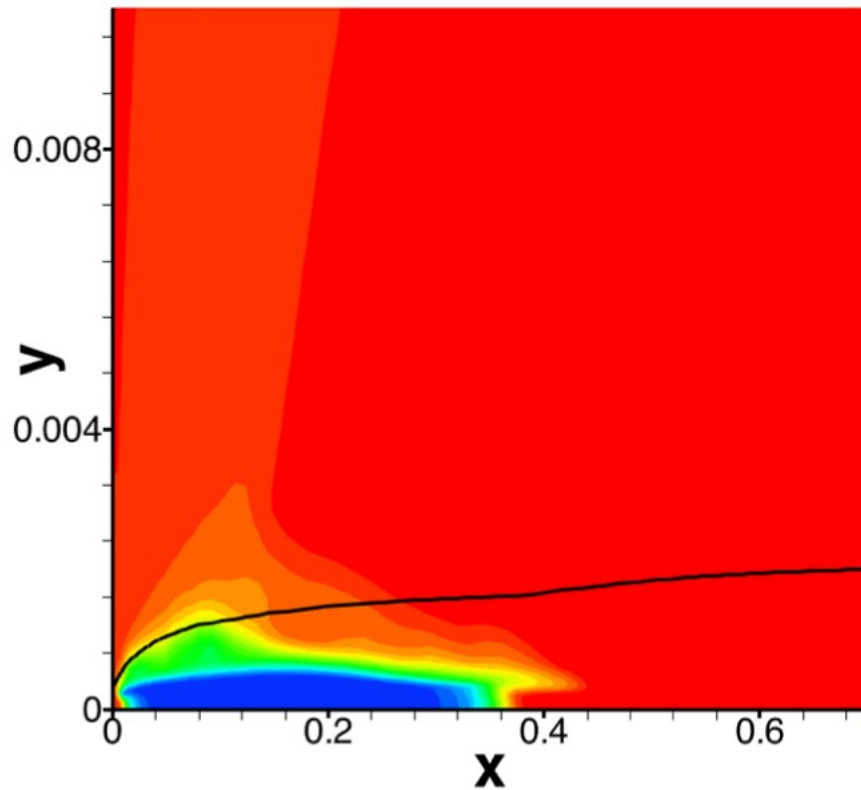
$$\frac{D\omega}{Dt} = 2C_{\omega 1} |S|^2 - C_{\omega 2} \omega^2 + \partial_j \left[ \left( \nu + \frac{\nu_T}{\sigma_\omega} \right) \partial_j \omega \right]$$

~~$$\frac{D\gamma}{Dt} = \partial_j \left[ \left( \frac{\nu}{\sigma_l} + \frac{\nu_T}{\sigma_\gamma} \right) \partial_j \gamma \right] + P_\gamma - E_\gamma$$~~

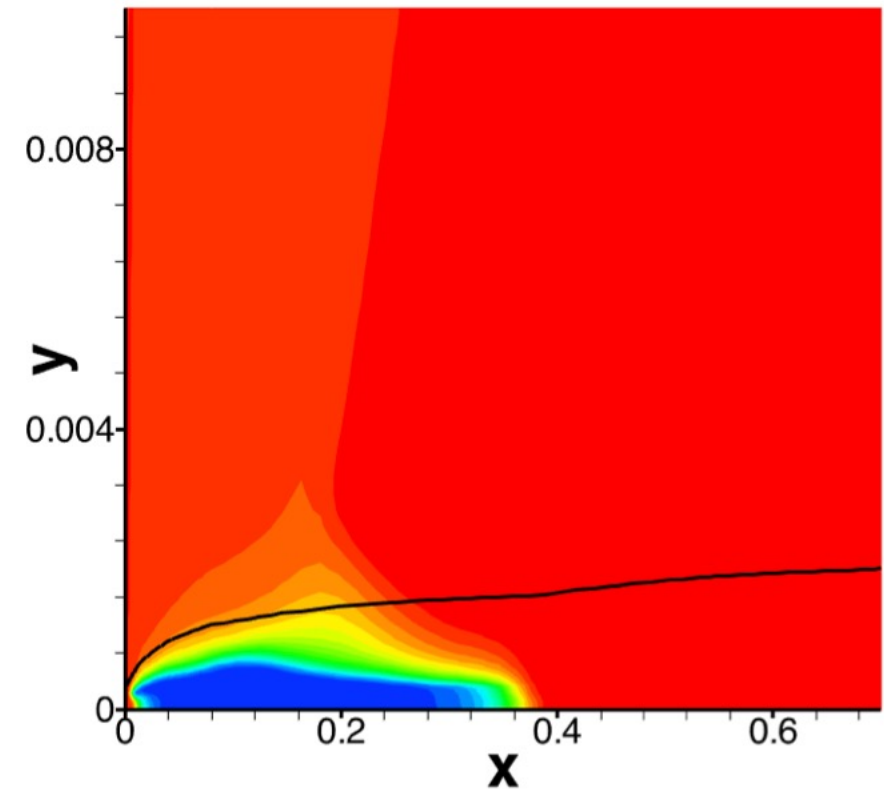
- Variables are more operational
- Interfacing of turbulence and transition models is critical !!



## A thought experiment



(c) T3C1: Optimal  $\gamma$



(d) T3C1: Model  $\gamma$

# Feature to help determine transition onset

$$Re_{\Omega} = \frac{\Omega d^2}{2.188\nu} \quad \max_d Re_{\Omega} \approx Re_{\theta}$$

Physics-informed  
choice of features

Praisner and Clark (J. Turbomachinery, 2007) gave the correlation

$$\theta_{tr} \approx \sqrt{\frac{7\nu}{9\omega_{\infty}}}$$

Physics-based non-  
dimensionalization

Then, we have

$$\frac{Re_{\theta}}{Re_{\theta, tr}} \approx \max_d \frac{Re_{\Omega}}{U_{\infty} \theta_{tr} / \nu} \approx \max_d \frac{\Omega d^2 \sqrt{9\omega_{\infty}}}{U_{\infty} \sqrt{7\nu}}$$

Freestream quantities are extracted from a constant wall distance.

Applying a conservative bound

$$\eta_1 = \min \left( \frac{d^2 \Omega \sqrt{9\omega_{\infty}}}{U_{\infty} \sqrt{7\nu}}, 3 \right)$$

Bounded features

# Reducing extrapolation in feature space via feature design

$$\eta = \{\nu_t, \nu\}$$

$$\eta = \left\{ \frac{\nu_t - \nu_{t,\min}}{\nu_{t,\max} - \nu_{t,\min}}, \frac{\nu - \nu_{\min}}{\nu_{\max} - \nu_{\min}} \right\}$$

$$\eta = \left\{ \frac{\nu_t}{\nu} \right\} \qquad \eta = \left\{ \frac{\nu + \nu_t}{\nu} \right\}$$

$$\eta = \left\{ \frac{\nu}{\nu_t + \nu} \right\}$$

$$\eta = \left\{ \frac{\nu^n}{\nu_t^n + \nu^n} \right\}, \quad \eta = \left\{ \left( \frac{\nu}{\nu_t + \nu} \right)^{1/n} \right\}, \quad \eta = \left\{ \frac{\log(\nu)}{\log(\nu_t) + \log(\nu)} \right\}, \dots$$

# Reducing extrapolation in feature space via feature design

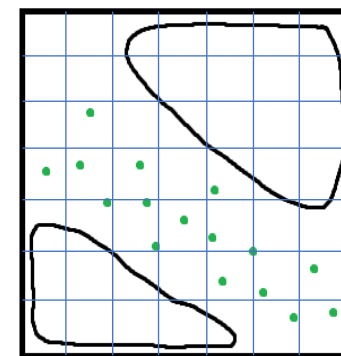
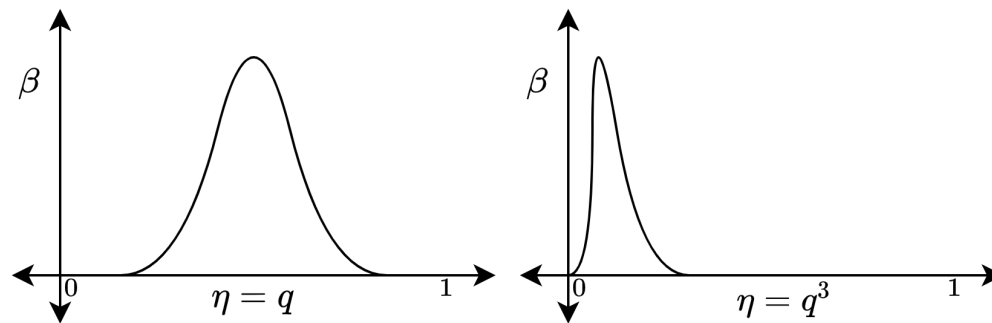
$$\eta = \{\nu_t, \nu\}$$

$$\eta = \left\{ \frac{\nu_t - \nu_{t,\min}}{\nu_{t,\max} - \nu_{t,\min}}, \frac{\nu - \nu_{\min}}{\nu_{\max} - \nu_{\min}} \right\}$$

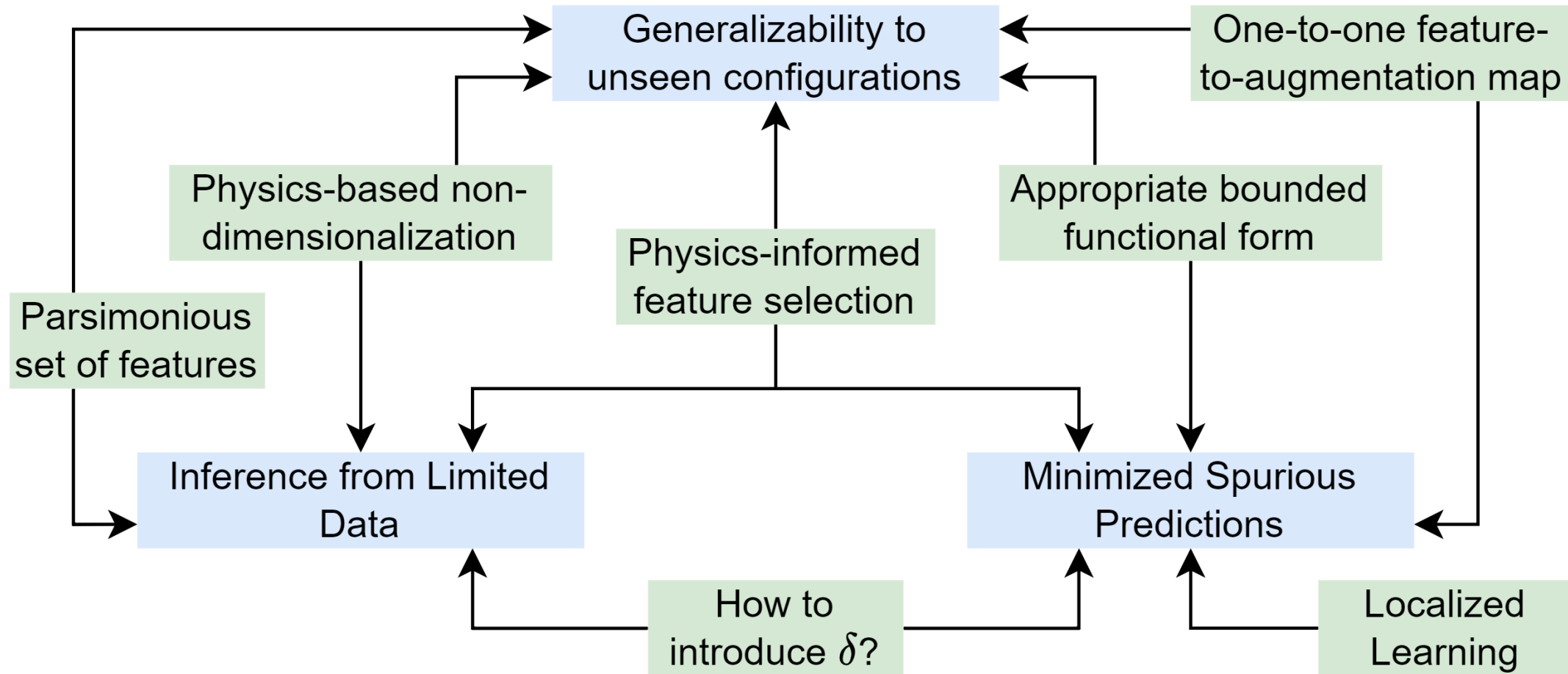
$$\eta = \left\{ \frac{\nu_t}{\nu} \right\} \qquad \eta = \left\{ \frac{\nu + \nu_t}{\nu} \right\}$$

$$\eta = \left\{ \frac{\nu}{\nu_t + \nu} \right\}$$

Interpolation in feature space can give you extrapolation in physical space



# Learning & Inference Assisted by Feature Space Engineering (LIFE)



# Feature(s) to identify laminar/turbulent regions

Compare  $\nu$  and  $\nu_t$ . What about the viscous sublayer, though?

Compare  $d$  and  $\ell_t$  to see if  $d$  is significantly larger. For  $k$ - $\omega$  model,  $\mathcal{O}(\ell_t) = \mathcal{O}(\sqrt{k}/\omega)$

Mathematically bound both the features as:

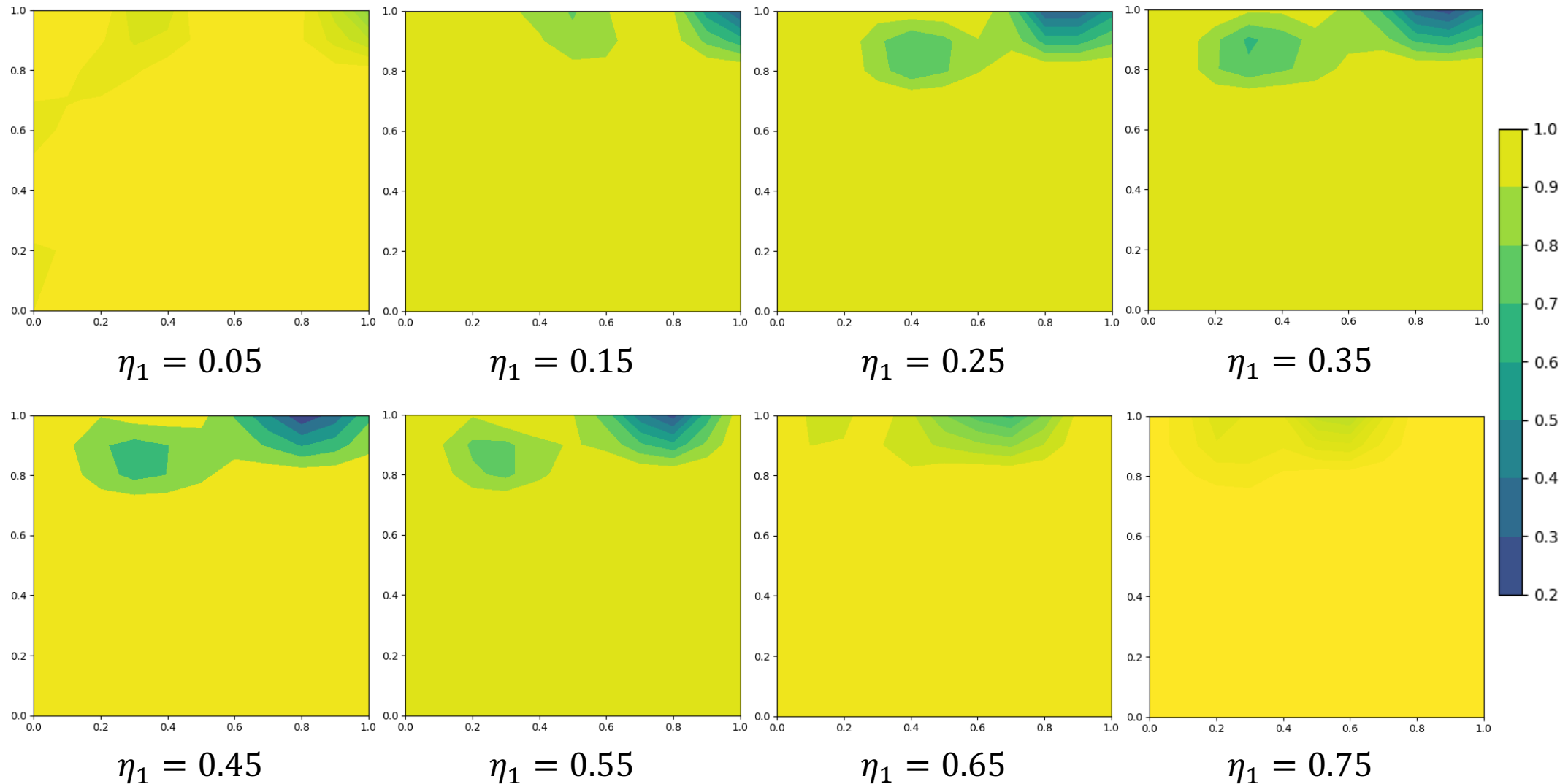
$$\eta_2 = \frac{d}{d + \sqrt{k}/\omega}$$

$$\eta_3 = \frac{\nu}{\nu_t + \nu}$$

- Too many features over-specify physical conditions and reduce generalizability
- Too few features can result in lower predictive accuracy even for the training cases



# How does the feature-space look like?



**For all plots:** X-axes:  $\eta_2$  (0 to 1) Y-axes:  $\eta_3$  (0 to 1)

# Prediction on turbine cascade (Model trained on only 2 flat plate cases – T3A, T3C1)

