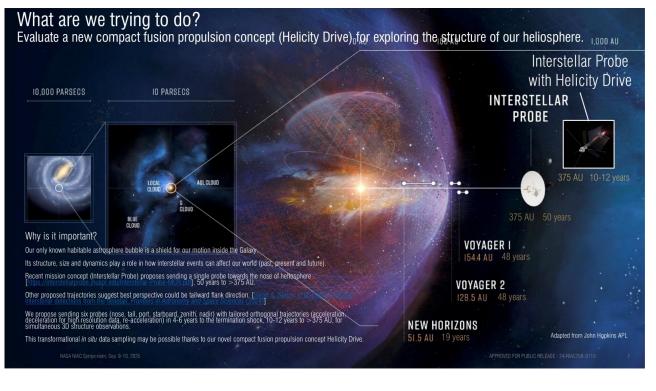
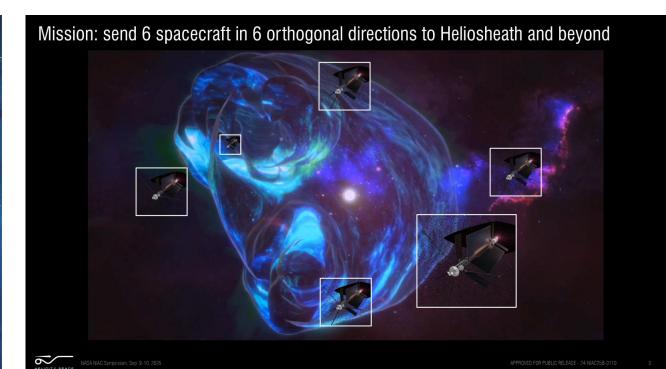


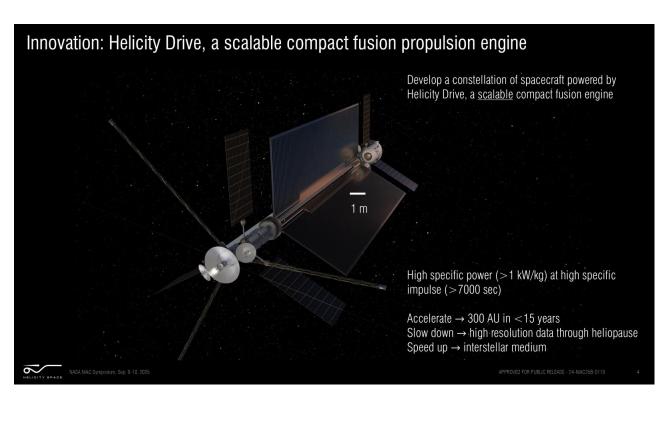
Fusion-Enabled Comprehensive Exploration of the Heliosphere

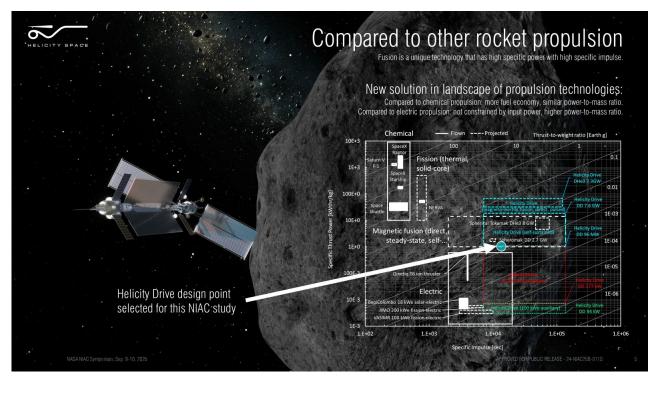
Dr Setthivoine You, Helicity Space (PI) Dr Ryan Weed, Helicity Space (Co-I) Dr Alan Stern, Helicity Space (Co-I) Prof Merav Opher, Boston Univ. (Co-I) Dr Seth Pree, Helicity Space

Overview

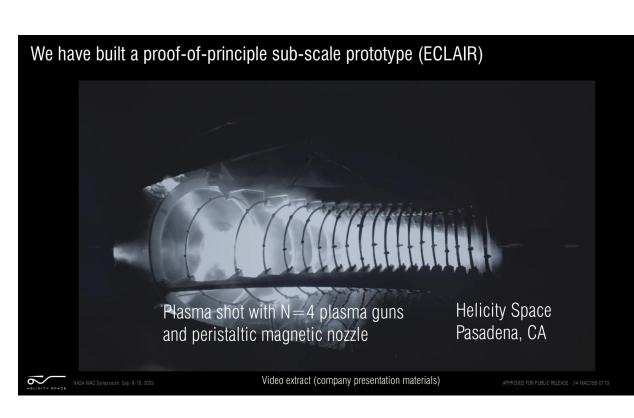


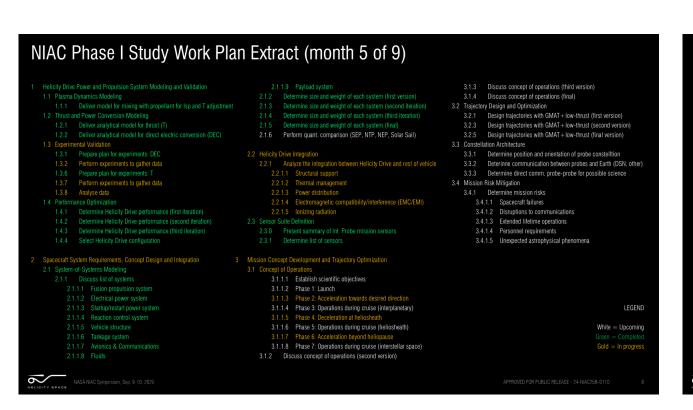








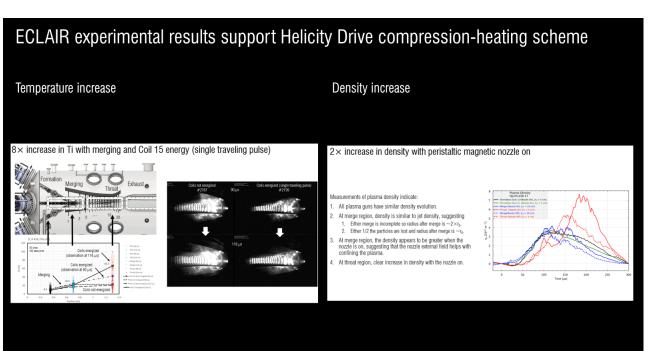




COMPACTNESS & SIMPLICITY: By preheating plasma with reconnection and merging multiple plectonemes, the Helicity Drive reduces the compression ratio and engineering complexities associated with traditional MIF

concepts, achieving a mass power density and volumetric power density at least 10x higher than other Nuclear Fission, Fission-Fusion, and CW magnetic confinement fusion approaches5.





Comparison with other rocket propulsion

Specific Impulse [sec]

Compared to other efficient MIF concepts

Reduced compression ratio, gun energy density (cf. ZaP SFS-Z [6])

nplosion symmetry, magnetic liner, pulse rate (cf. Helion FDR [7])

Non-radioactive fuel, pulse rate (cf. MSFC PuFF [5])

Low pulse rates $\leq 1 \text{ Hz}$

Safety factors (\sim 2)

Radiation vented to space

Pragmatic assumptions

Fission (thermal.

Magnetic fusion (direct,

BepiColombo 18 kWe solar-electric

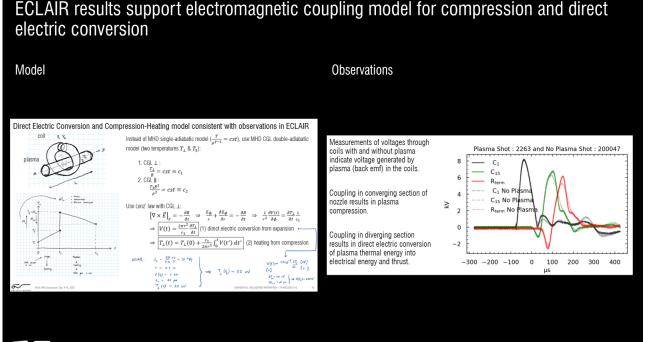
VASIMR 100 kWe fission-electric

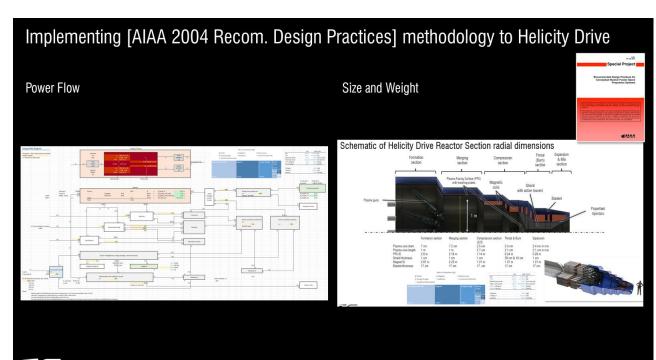
MAGNETIC RECONNECTION HEATING: Directly heats ions, eliminates the need for complex plasma shaping, and

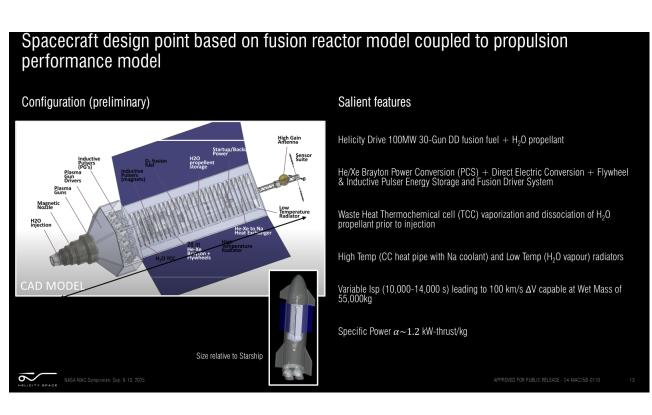
PERISTALTIC MAGNETIC COMPRESSION: passive arrangement of magnetic coils to compress the plasma in 3D

Scaling of fusion power and propulsive

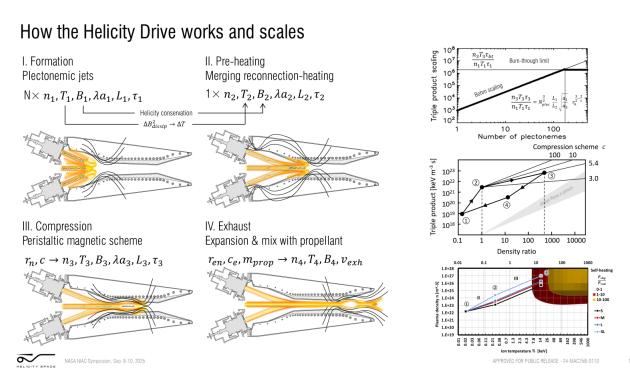
steady-state, self-sustained)







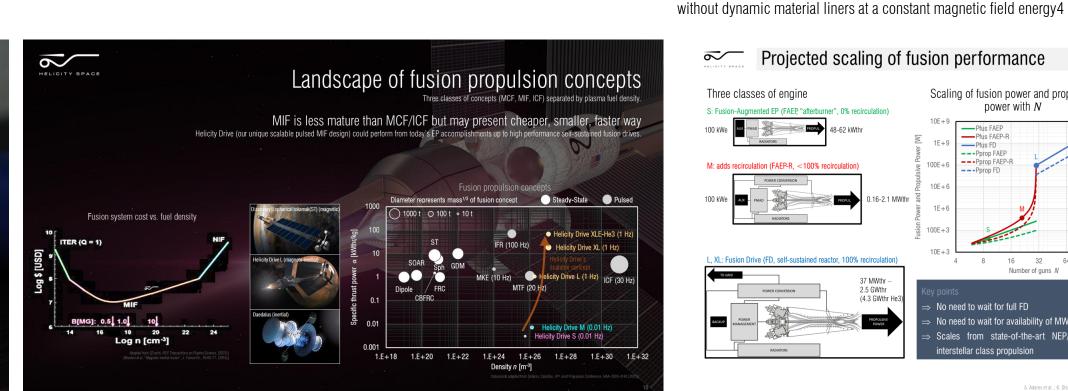
Innovation: Helicity Drive



USE NEW PLASMA HEATING TECHNIQUES FOR FUSION Leverages recent breakthroughs in magnetic reconnection heating to achieve a scalable, efficient, and more compact fusion solution compared to traditional methods.

A. Plectonemic Taylor states [4-7] B. Reconnection-heating [8,9] C. Peristaltic compression [10] MOCHI, SSX experiments SSX, TS, MAST, ST-40 experiments Caltech experiments Compact (far from walls) High power (MW) No moving parts Self-stable, high beta Efficient (~90%) No cold liquid/plasma/material liner Nested flux surfaces Direct heating of ions Constant energy Rotational transform Internal Simplified symmetry Tilted already No need for perfect geometry Long aspect ratio PLECTONEMIC MAGNETIC CONFINEMENT: This recently discovered, stable magnetic configuration provides

inherent plasma confinement without requiring solid walls. Its robustness to translation and merging capabilities, combined with reconnection heating, offer a unique pathway to achieving fusion conditions



HIGH POWER DENSITY LEADS TO EXTREME DELTA-V's

Philosophy behind our novel fusion concept

enables rapid temperature increases with feasible magnetic field strengths

est net gain is viable for space pro

d scalability is key to develo

Fusion has high specific power and high specific impulse when the hot plasma is exhausted directly to thrust.

Together, both enable fast, reusable, agile, efficient space travel.

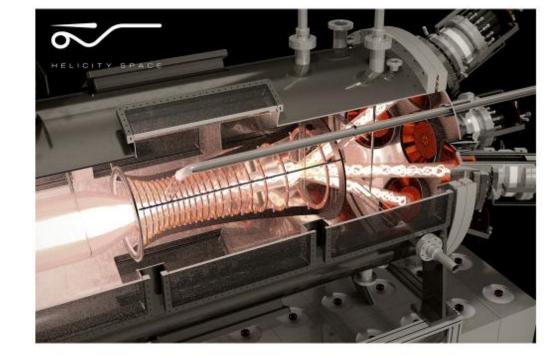
Scaling estimates shows that the minimum viable Helicity Drive could perform like state-of-the-art NEP/SEP concepts.

Scalability of Helicity Drive is key to rapid development.

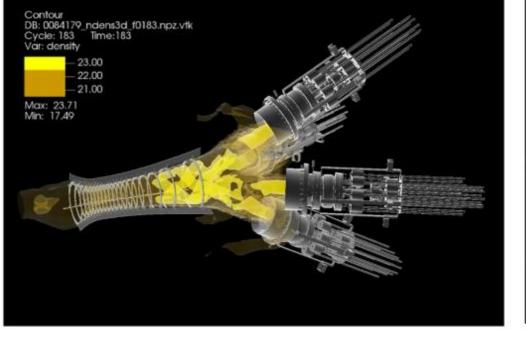
Our scaling is simplified, potentially cost-effective, from developmen sizes to minimum viable (green) to peak performance (blue).

High specific power is necessary for fast travel.

ECLAIR: sub-scale proof-of-principle prototype of Helicity Drive



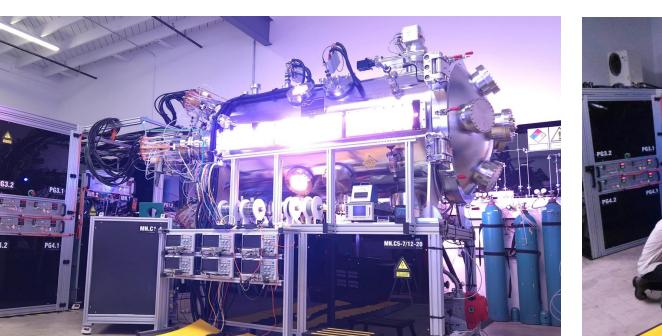
Schematic of ECLAIR experiment showing salient features: 4 plasma guns forming plectonemic plasma jets merging at the inlet of the peristaltic magnetic nozzle. Reconnection-heated plasma is compressed in the diverging section to peak conditions at the throat for further expansion in the diverging section.



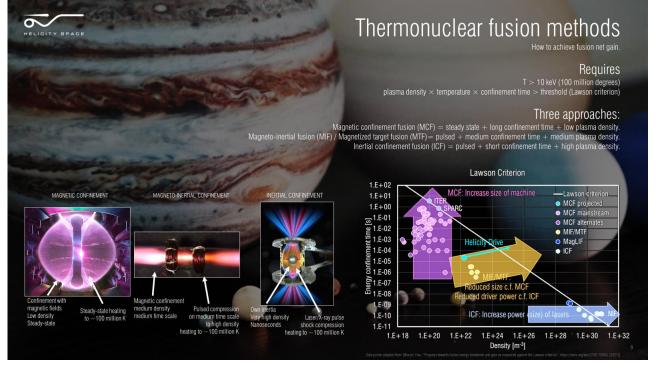
3D MHD simulations performed on the LA-COMPASS supercomputer simulation inc collaboration with Los Alamos National Laboratory, with the support of the DOE INFUSE program. The simulations show merging and braiding of the four plasma jets in the magnetic nozzle (passive, non-peristaltic in this run).

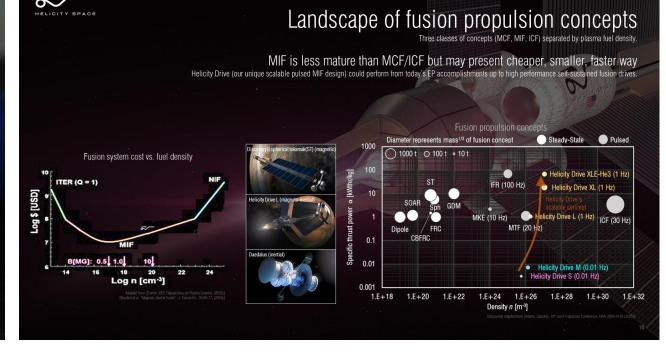
Single frame from a high speed (5M frames per second) camera showing typical plasma shot with four collimated jets merging and travelling inside the peristaltic

MODEL RESULTS

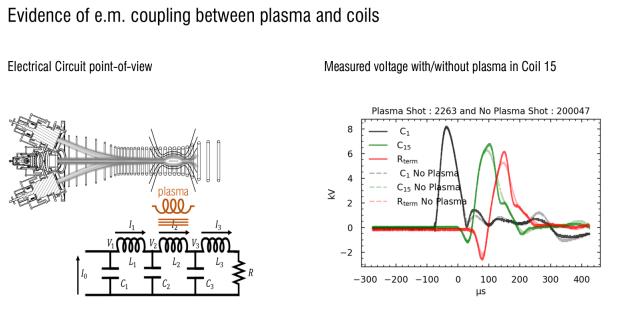


ECLAIR experiment (April 2025) as seen during a plasma shot with a phone camera and with operator.





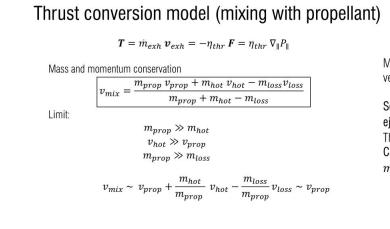




model (two temperatures T_{\perp} & T_{\parallel}): 2. CGL || : $\frac{T_{\parallel}B^2}{c^2} = cst \equiv c_2$ ECLAIR: C1 ~ 20 eV ~ 33 eVT r ~ 0.1 m V (t) ~ 1 kV

Direct Electric Conversion (and Compression-Heating) model Instead of MHD single-adiabatic model $(\frac{T}{c^{\gamma-1}} = cst)$, use MHD CGL double-adiabatic $\Rightarrow V(t) = \frac{2\pi r^2}{c_1} \frac{\partial T_\perp}{\partial t}$ (1) direct electric conversion from expansion $\Rightarrow |T_{\perp}(t) = T_{\perp}(0) + \frac{c_1}{2\pi r^2} \int_0^t V(t') dt' |$ (2) heating from compression t, ~ 60 ps
T₁ (0) ~ 20 eV

Thrust conversion model proposes scaling of lsp and T [no mixing here, at next step] $\vec{F} = \vec{J} \times \vec{B} - \nabla \cdot \vec{\Pi} = \frac{B^2}{u_*} \left(\hat{b} \cdot \nabla \right) \hat{b} - \nabla_{\perp} \left(P_{\perp} + \frac{B^2}{2u_*} \right) - \nabla_{\parallel} P_{\parallel}$ (1) Use CGL || for pressure gradient term: $\frac{T_{\parallel}B^2}{c^2} = cst \equiv c_2 \quad \Rightarrow \quad P_{\parallel} = \rho T_{\parallel} = \sqrt{\frac{r_{\parallel}}{c^2}}$ Limit 1: prior to fusion, $J \times B \gg \nabla P$ Lorentz force accelerates plasma to Alfvenic velocities $v_A \sim B/\sqrt{\mu_0 \rho}$. ECLAIR I \sim 41 km/s [0.6 T, 10²³ m⁻³] c.f. Doppler shift observations \sim 30 km/s (lsp \sim 2700 s, 75%) Limit 2: after fusion, $\nabla P \gg J \times B$ Pressure gradient accelerates to $v_{th}{\sim}\sqrt{k_BT_{\parallel}/m}$ velocity.

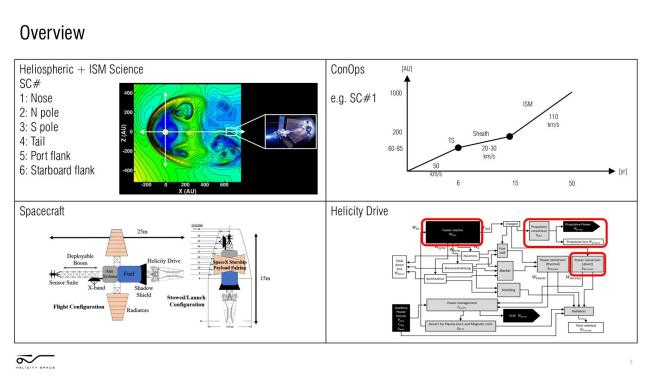


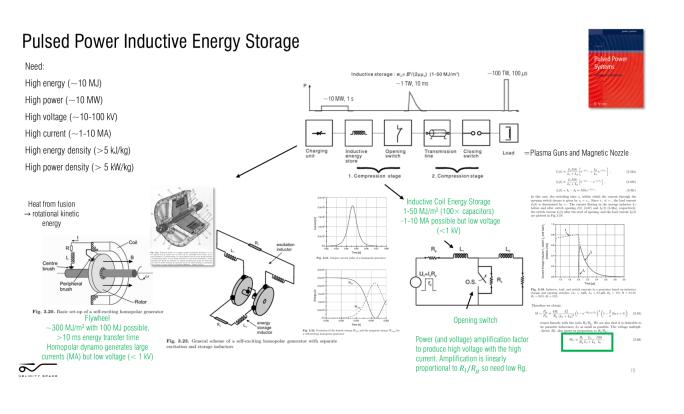
Mixture velocity is basically the injected propellant velocity, increased as the mixture fraction decreases. So we can choose an I_{sp} by injecting cooler plasma ejected at Alfvénic velocities $v_{prop} \sim v_A$. This will give maximum T. Can increase I_{sp} by reducing cooler plasma density

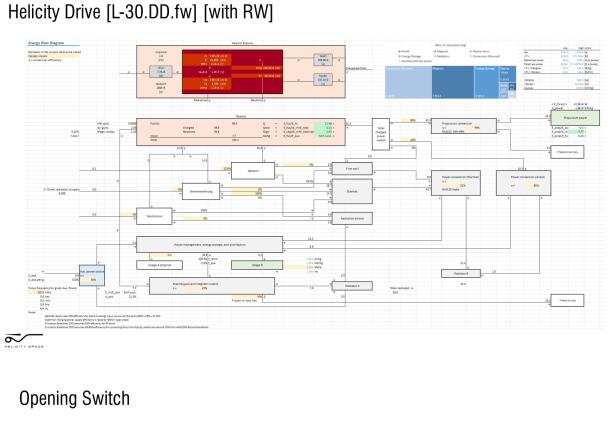
ECLAIR II estim. \sim 280 km/s [$T_i \sim$ 1.3 keV, no mixing] $\Rightarrow I_{sp} \sim 28000 s \Rightarrow T \sim 4.3 \text{ kN}$ Need ECLAIR II and III machines (under dev.) to validate

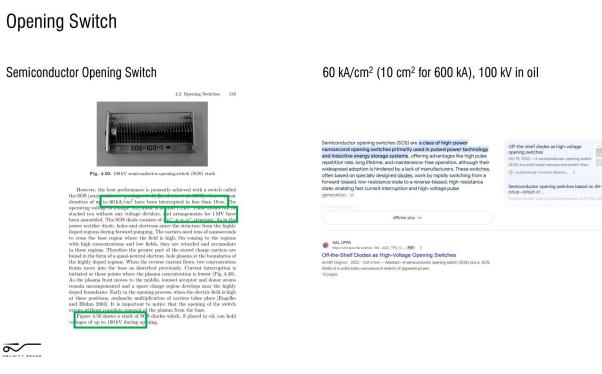
Mix with cooler denser propellant to adjust $I_{sp} = \frac{v_{exh}}{a}$.

Design Point for Heliosphere Spacecrafts







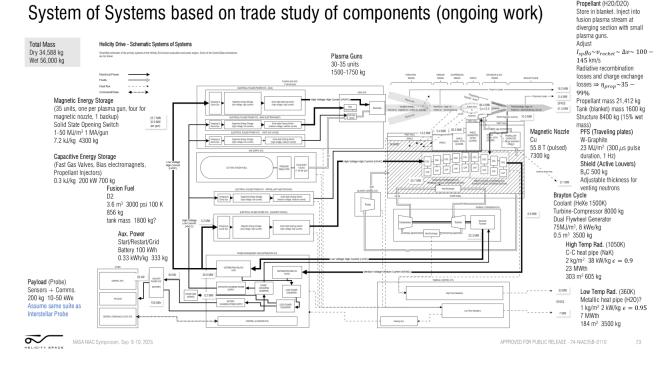


HELICITY SPACE

Merav's inputs: I suggest refining the objectives to highlight the 6 different trajectories;

In the tail through regions of the heliotail that potentially will allow us to study acceleration and turbulence and mixing

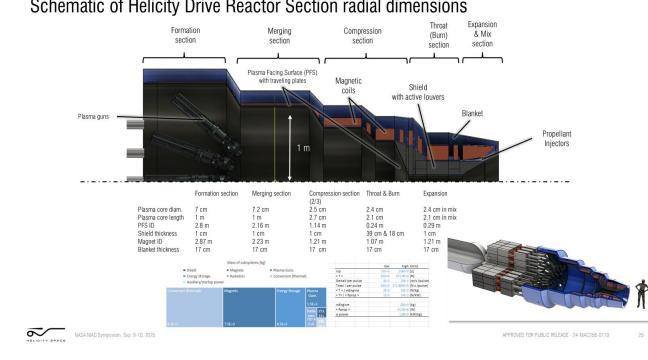
In the poles/flanks we will be going through the turbulent region of the heliosphere.

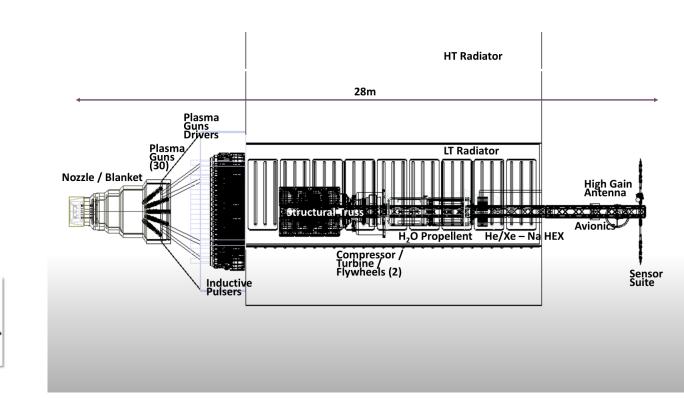


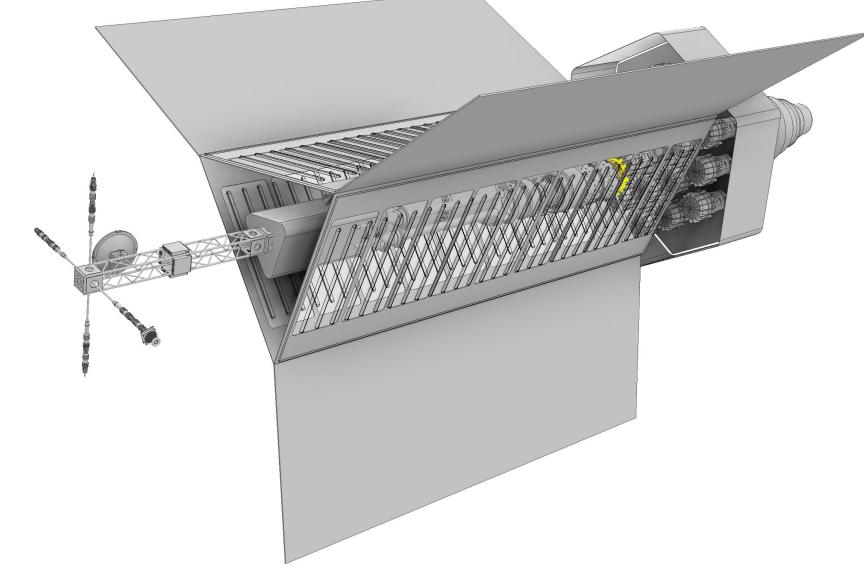
FIELDS AND WAVES

ENERGETIC NEUTRAL ATOM IMAGIN

LYMAN-ALPHA Lyman-Alpha Spectrograph (LYA)







Propellant Mix Model

PERFORMANCE MODEL

- Matlab model varies H₂O aux propellent injection rate • Calculates plasma temperature (w/ radiative and recombination losses) for various ionization • Calculates subsystem mass based on aux propellent flow rate (e.g. TCC mass proportional to
- Calculates propulsion performance based on thrust efficiency → delta-V calculation based on mass fraction and ISP

ASSUMPTIONS % --- Mission & Spacecraft Parameters $mission.m_wet_max = 56000;$ % Maximum total initial mass (wet mass) in kg mission.m_engine_payload = 13700; % Mass of the fusion engine and payload in kg (magnets, shield, PGs, Energy storage, startup power) %mission.eta thrust = 0.7 % Thrust conversion efficiency (nozzle efficiency) % --- Fusion & Power System Parameters % 104.1MW of total fusion power % Fraction of power emitted as neutrons power.neutron_fraction = 0.38; P_recirc_electric = 30.9E6; % Required electrical power input to plasma guns $power.alpha_pcs = 0.36;$ % kg/kW, for power conversion system [williams 1998] $P_{charged} = 52.3E6;$ % from HelicityL-30-DD calculations % direct energy conversion from charged particles in fusion plasma expansion $P_DEC_frac = 0.2;$ P_charged_thrust = P_charged*(1-P_DEC_frac); % from HelicityL-30-DD calculations DEC_eff = 0.85; P_DEC = P_charged*P_DEC_frac*DEC_eff;

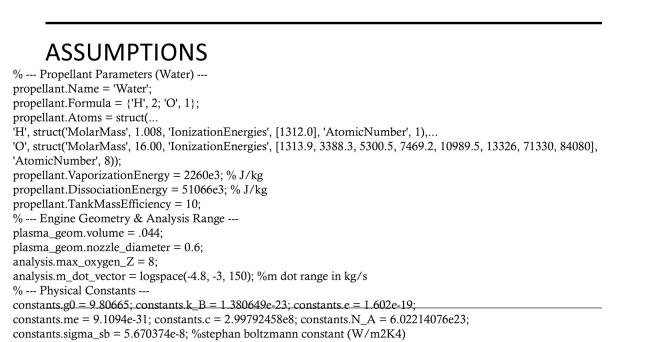


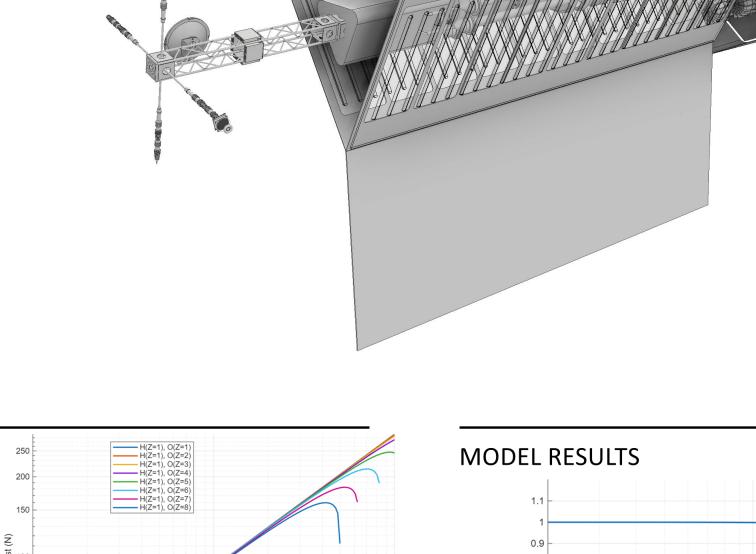
radiator.areal_massHT = 2.0; % kg/m^2 radiator.areal_massLT = 1.0; % kg/m^2

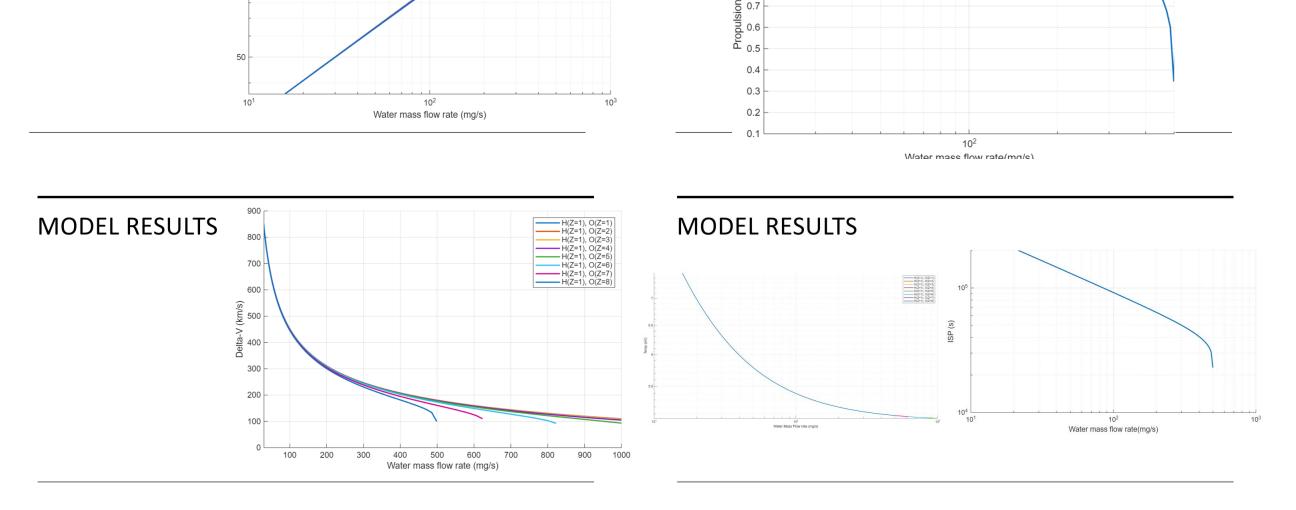
radiator.lowtempK = 800: % maximum radiator temperature (low temp coolar

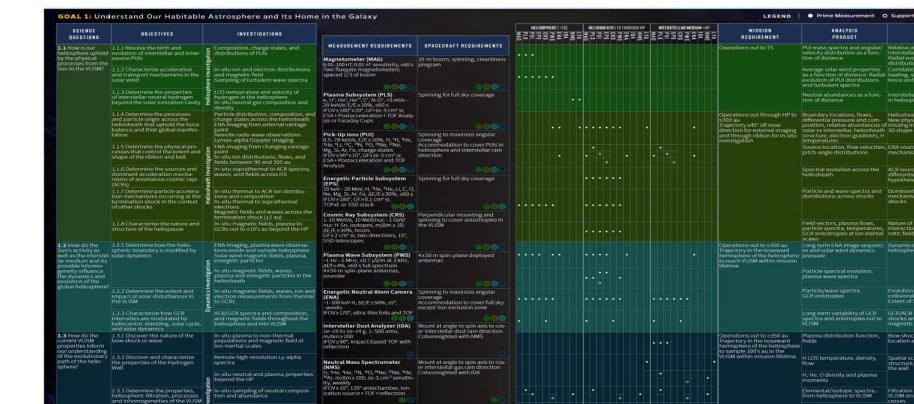
radiator.emissivityHT = 0.9;

radiator.emissivityLT = 0.95;









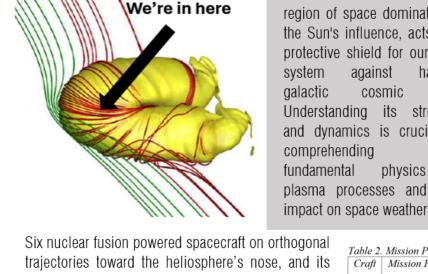


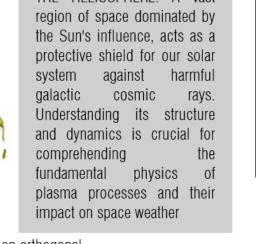




1 You, Setthivoine et al, "Helicity Drive: A Novel Scalable Fusion Concept for Deep Space Propulsion", AIAA Propulsion & Energy Forum, AIAA 2020-3835, (2020) https://doi.org/10.2514/6.2020-3835 2 Brown, Michael, Kaitlin Gelber, and Matiwos Mebratu. "Taylor state merging at SSX: experiment and simulation." Plasma 3.1 (2020): 27-37. 3 You, Setthivoine, et al. "The Mochi LabJet experiment for measurements of canonical helicity injection in a laboratory astrophysical jet." The Astrophysical Journal Supplement Series 236.2 (2018): 29. 4 Bellan P. M., "Traveling mirror compressor delay line with nonconstant capacitance.", Phys. Fluids, 24, 11 (1981) 5 Cassibry, Jason, et al. "Case and development path for fusion propulsion." Journal of Spacecraft and Rockets 52.2 (2015): 595-612. 6 Opher, Merav, et al. "Solar wind with Hydrogen Ion charge Exchange and Large-Scale Dynamics (SHIELD) DRIVE Science Center." Frontiers in Astronomy and Space Sciences 10 (2023): 1143909 7 Lapointe, M. R., et al. Gradient Field Imploding Liner Fusion Propulsion System: NASA Innovative Advanced Concepts Phase I Final Report. No. M-1471. 2018

Mission





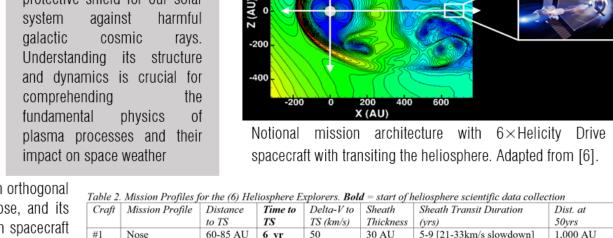


 Table 2. Mission Profiles for the (6) Heliosphere Explorers. Bold = start of heliosphere scientific data collection

 Craft
 Mission Profile
 Distance
 Time to
 Delta-V to
 Sheath
 Sheath Transit Duration
 Dist. at
 north, south, east, and west flanks. Each spacecraft 30 AU 5-9 [21-33km/s slowdown] 1,000 AU 100 AU 5 [no slowdown] 1,450 AU carries a suite of scientific instruments to #1 Nose 60-85 AU 6 yr 50 #2-3 N & S Poles 115 AU 5.75 yr 95 comprehensively measure plasma wave properties, #4 Tail 145 AU 4.6 yr 150 300 AU 10 [no slowdown] #5 Port Flank 105 AU 5.5 yr 90 80 AU 5 [14km/s slowdown] magnetic fields, heliospheric and interstellar dust #6 Starboard Flank 115 AU 5.75 yr 95 100 AU 5 [no slowdown] properties, and energetic particle distributions.

⁶Opher, Merav, et al. "Solar wind with Hydrogen Ion charge Exchange and Large-Scale Dynamics (SHIELD) DRIVE Science Center." Frontiers in Astronomy and Space Sciences 10 (2023): 1143909

We need to go farther, and we need to go faster, and we need to probe in multiple dimensions of the heliosphere simultaneously to resolve the key attributes of the heliosphere. Among these mysteries are – the width of the heliosheath the nature of the heliopause the source of anomalous cosmic rays

• the turbulent nature of the heliospheric tail Voyager and New Horizons have provided invaluable data, but modern instrumentation can now fully capture key phenomena like pickup ions and weak magnetic fields. Other information comes from Earth-based line-of-sight observations. This region is starved for in situ observational data.

INITIAL PAYLOAD CONSIDERATION Based on the Helio Decadal Interstellar Probe Study