

MISSION OPERATIONS DIRECTORATE FLIGHT DIRECTOR OFFICE



ENTRY OPTIONS TIGER TEAM

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ENTRY OPTIONS

Agenda/Contents

- Previous Results - Summarized
- STS-107 Weight Reduction Scenarios
- Results - Summarized
- Weight Reduction - Details/Assumptions
- Weight Reduction Combinations - Scenarios 1,2, & 3
- Cold Soak Results - Summarized
- Conclusions

ENTRY OPTIONS

Previous Results - Summary

- Best case sensitivity study using certified deorbit targeting and STS-107 trajectory initial conditions to evaluate wing leading edge (WLE) and two body points, one forward and one aft of MLG door. (see Backup Chart 1 for diagram)
 - Control parameters: altitude, weight, c.g., crossrange, N-cycles (trajectory steepness), approach (ascending/descending), hemisphere (atmosphere), and prebank.
- Results were as follows:
 - No significant thermal relief for **any single control variable**.
 - Best case **control variable combinations**:
 - WLE body point 5505 (RCC): ~ 5% reduction in WLE max. temp.
 - Body point 1602 (tile): ~ 20% reduction for heat load, ~ 30% reduction for heat rate.
 - Body point 2360 (tile): ~ 20% reduction for heat load, ~ 40% reduction for heat rate.
- Caveats to results:
 - All results were for a “no damage” scenario. For damage, the heat load and heat rate reductions would likely not be directly applicable, depending on the degree of damage.
 - Best case combinations were not proven to be achievable.
- Analysis results verified our previous understanding: Using certified deorbit targeting methods, the only way to reduce the STS-107 heating profile would be to significantly reduce the weight (while maintaining acceptable c.g.) and to lower the orbit altitude prior to deorbit.

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STS-107 Weight Reduction Scenarios

- OVE WG (3/17/03) and PRCB (3/13/03) direction was to finalize the best case analyses for STS-107 initial conditions, and to not pursue development of any uncertified or contingency deorbit/entry profiles at this time.
- The team developed three different weight reduction scenarios for STS-107, and combined them with other best-on-best case conditions (altitude reduction, approach trajectory, etc.) as in previous analyses.
 - Best case weight reduction categories included consumables (ECLSS, APU, Cryo, Prop), deployable items (middeck, flight deck, crew equipment, avionics, Spacehab), and jettison items (Spacehab, FREESTAR/GAS cans, and radiator panels).
 - Categories of weight reduction were not verified achievable, either alone (e.g. consumables), or in combination with other categories.
 - For each of the weight reduction scenarios, we assumed we could do it all.
 - This may not be realistic for some of the scenarios – the goal was to find the upper bound on the weight reduction.
 - Deployable and jettison items were grouped into scenarios that were limited only by available EVA time (12 hours).
- The associated entry trajectories were simulated, the results of which were analyzed using the TSEP model.

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Results - Summary

- Weight reduction scenario 3 (consumables, deployable items, Spacehab jettison, and FREESTAR jettison) yielded the best results, with a total weight reduction of 31,321 lbm.
- Using certified deorbit targeting and STS-107 trajectory initial conditions, and the best case combination of other control variables, scenario 3 yielded the following results:
 - WLE body point 5505 (RCC): ~ 7% reduction in WLE max. temp.
 - Body point 1602 (tile): ~ 24% reduction heat load, ~ 34% reduction heat rate.
 - Body point 2360 (tile): ~ 29% reduction heat load, ~ 56% reduction heat rate.
- Caveats to results:
 - Detailed risk assessment was not performed, however it is clear that the increase in risk would be very significant in order to achieve these weight reductions.
 - Numerous flight rule violations (e.g. consumables management, EVA, etc.).
 - Numerous undocumented/unverified procedures (e.g. EVA jettison tasks, IFM, etc.).
 - Combination of weight reduction categories (consumables, deployable items, and jettison) was not verified to be feasible (timeline, crew workload, detailed EVA task, etc.)
 - All results were for a “no damage” scenario. For damage, the heat load and heat rate reductions would likely not be directly applicable, depending on the degree of damage.
 - Best case combination of trajectory variables was not proven to be achievable.

ENTRY OPTIONS

Results – Summary (Cont'd)

- Weight reduction scenario 1 (consumables, deployable items, Spacehab deployable items, GAS cans, and radiator panels) yielded a total weight reduction of 20,387 lbm, the results of which were:
 - WLE body point 5505 (RCC): ~ 6% reduction in WLE max. temp.
 - Body point 1602 (tile): ~ 17% reduction heat load, ~ 33% reduction heat rate.
 - Body point 2360 (tile): ~ 23% reduction heat load, ~ 46% reduction heat rate.
- Weight reduction scenario 2 (consumables, deployable items, Spacehab deployable items, radiator panels, and FREESTAR jettison) yielded a total weight reduction of 22,924 lbm, the results of which were:
 - WLE body point 5505 (RCC): ~ 6% reduction in WLE max. temp.
 - Body point 1602 (tile): ~ 18% reduction heat load, ~ 33% reduction heat rate.
 - Body point 2360 (tile): ~ 23% reduction heat load, ~ 45% reduction heat rate.
- Caveats to results:
 - Same as for Scenario 3
- Trajectory/TSEP data included in backup charts.

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Weight Reduction – Consumables

- Consumables (total reduction 4159 lbm)
 - ECLSS (total 650 lbm)
 - All supply water tanks other than tank A dumped to zero (393).
 - Waste tank to minimum (79).
 - Both ammonia (NH₃) tanks depleted (92).
 - GN₂ systems at minimums (86).
 - APU/HYD (total 560 lbm)
 - One APU run to depletion (278).
 - Other two APU's run to minimum quantities (222).
 - Cooling water (WSB) reduction due to APU run time (60).
 - Cryo H₂/O₂ (total 1600 lbm)
 - Tanks 3-9 (EDO and Orbiter) reduced to minimum residuals.
 - Remaining cryo vented overboard through relief valves.
 - Tank heaters used to over-pressurize tanks.
 - Excess cryo at the end of the mission could be “dumped” in less than one day.
 - Tanks 1 and 2 at minimums to support deorbit/entry.

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Weight Reduction – Consumables (Cont'd)

- Consumables (cont'd)
 - PROP (total 1349 lbm)
 - FRCS dumped to zero – nominal ops.
 - ARCS reduced to minimum to support mean entry to 0.05g, at which point exactly 20% remains (1349).
 - Impacts include numerous flight rule violations and undocumented procedures.
 - Absolute minimums in critical systems.
 - No deorbit waveoff opportunities.
 - No postlanding capability (cooling or power).
 - Zero fault tolerance, or reduced fault tolerance.
- Itemized weight/c.g. details included in backup charts.

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Weight Reduction – Deployable Items

- Deployable items (total reduction 16,228 lbm)
 - All loose items, and items that could be made loose (via IFM, for example) and deployed overboard via EVA.
- Items included from the following areas:
 - Middeck, flight deck, avionics bays (LRU's), crew equipment (4663).
 - Spacehab module - systems, experiment payloads, racks (8017).
 - GAS cans (1891).
 - Radiator Panels (1657).
- Itemized weight/c.g. details included in backup charts.

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Weight Reduction – Spacehab Jettison

- Perform EVA to disconnect Spacehab module and jettison from payload bay. (18,071 lbm)
 - Use EVA torque multiplier tool to open all four sill passive latches, and use EVA pins to restrain floating latches.
 - Disconnect 23 electrical and water lines running from Orbiter to Spacehab.
 - Use EVA cable cutters to physically disconnect lines.
 - Only one inhibit to remove power prior to cutting lines.
 - Disconnect Spacehab from tunnel adapter at the flexible joint.
 - Flexible joint material is Kevlar, cloth, and wiring.
 - May have been able to use EVA and IFM tools to cut through joint.
 - Two potential options for getting Spacehab out of payload bay:
 - EVA crew (two) pull Spacehab out of the closed keel latch and open sill latches to gain clearance for Orbiter backaway.
 - Perform slow Orbiter backaway while Spacehab is in open sill latches and closed keel latch.
 - Impacts and Unknowns
 - No experience base to determine feasibility of either option.
 - EVA crew pull SH out of the keel latch – unknown forces. No foot restraints available, so task would be free floating.
 - Dynamics of separation from closed keel latch has not been analyzed.

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Weight Reduction – FREESTAR Jettison

- Perform EVA to disconnect FREESTAR and jettison from payload bay. (4428 lbm)
 - Use EVA torque multiplier tool to open all four sill passive latches, and use EVA pins to restrain floating latches.
 - 8 electrical lines running from Orbiter to FREESTAR.
 - Use EVA cable cutters to physically disconnect lines.
 - Only one inhibit to remove power prior to cutting lines.
 - Impacts and Unknowns
 - Same options and concerns as Spacehab for getting FREESTAR out of payload bay.
 - Probably more feasible than SH jettison, from a mass handling perspective.
 - STS-107 only had two EVA latch pins manifested.
 - If both SH and FREESTAR were jettisoned, would need alternate means for restraining 2 floating passive latches.

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FREESTAR/Spacehab Jettison and Separation

- Assume that EVA crew will completely detach FREESTAR (or Spacehab) and provide a clear path up out of the payload bay.
- Separation technique:
 - Orbiter performs small +Z body translation in free drift to slowly back away from FREESTAR (or Spacehab).
 - When FREESTAR (or Spacehab) clears the Orbiter mold line, the Orbiter will return to attitude hold and execute a standard separation sequence.
 - Separation Maneuver (1/2/3 Separation) Orbit Ops Checklist.
 - Provides a safe separation for any attitude.
 - Impacts and Unknowns
 - Small risk assuming the payload to be jettisoned is completely detached and cannot hang up as it exits the payload bay.
 - Separation techniques and procedures are published and well understood.

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Weight Reduction Combinations – Scenarios 1 thru 3

- Table includes weight reduction categories used to develop combination scenarios.

<u>Item</u>	<u>Description</u>	<u>Weight Reduction</u>
A	Consumables	4159
B	Deployable Items (Middeck, Flight Deck, Avionics, Crew Equip.)	4663
C	Deployable from Spacehab ⁽¹⁾	8017
D	GAS Cans ⁽²⁾	1891
E	Radiator Panels	1657
F	FREESTAR Jettison	4428
G	Spacehab Jettison	18071

(1) – Item C is a subset of the total weight from item G.

(2) – Item D is a subset of the total weight from item F.

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Weight Reduction Combinations – Scenarios 1 thru 3 (Cont'd)

- Three scenarios were developed from logical combinations of the items listed in the table.
 - Scenario 1: Total weight reduction = 20,387 lbm
 - Weight/c.g. changes resulting from combination of items A thru E.
 - Includes consumables, deployable items, SH deployable items, GAS cans, and radiator panels.
 - Assumes risks associated with jettison of Spacehab or FREESTAR are too great, or jettison unsuccessful (e.g. cannot physically detach).
 - Scenario 2: Total weight reduction = 22,924 lbm
 - Weight/c.g. changes resulting from combination of items A, B, C, E & F.
 - Includes consumables, deployable items, SH deployable items, radiator panels, and FREESTAR jettison.
 - Assumes risks associated with jettison of Spacehab are too great, or jettison unsuccessful (e.g. cannot physically detach).

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Weight Reduction Combinations – Scenarios 1 thru 3 (Cont'd)

- Scenario 3: Total weight reduction = 31,321 lbm
 - Weight/c.g. changes resulting from combination of items A, B, F & G.
 - Includes consumables, deployable items, FREESTAR jettison, and Spacehab jettison.
 - Radiator panel jettison was not included, because it was assumed that the EVA time required to perform both FREESTAR and SH jettison, as well as to deploy all other “deployables” would not leave time to also execute radiator jettison.
 - Assumes FREESTAR and Spacehab EVA jettison techniques can be developed and executed.
- Itemized weight/c.g. details for all three scenarios included in backup charts.

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Weight Reduction Combinations – Scenarios 1 thru 3 (Cont'd)

- General Overriding Assumptions
 - Decision to perform weight reduction occurs early enough in the mission to develop the required plans and techniques.
 - Consumables – usage, overboard dumps, depletion burns, etc.
 - Deployable Items - required IFM's, “deploy packaging”, etc.
 - Deployable Items - required EVA's, Orbiter maneuvers.
 - Jettison Items - required EVA's for detaching, jettisoning, cleanup of payload bay, etc.
 - Excessive risks associated with any of the three options (Scenario 1,2, or 3, or any other combination) would require that significant, and convincing data exists proving that the Orbiter could not survive entry.
 - Any and all possible weight reduction might be considered, depending on degree of concern, and time available.

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Results - On-Orbit Coldsoak Post-Flight Analysis

- The STS-107 EOM attitude timeline did provide cold wings for entry.
 - Actual EI temps were 6 deg F and 3 deg F on lower and upper surfaces, respectively (temp. limit is 92 deg at EI).
- Best case left wing cold soak protecting all STS-107 thermal constraints (MLG tires, PLBD BET, structure, wave-off days), ECLSS, pointing and payloads yielded a 10 deg reduction in the left wing temp at EI.
- Best case, protecting only a single deorbit opportunity, cold soaking for 2 days, yielded a 50 deg reduction in left wing temp at EI.
- Best case, maximum possible cold soak (2+ days) and not protecting any other constraints yielded a 65 deg reduction in left wing temp at EI.
 - Reductions limited by low beta angle on STS-107.
- These EI wing temperature reductions are not significant.
 - On STS-107, wing temps may have increased as much as 700 deg in 400 seconds (1.75 deg/sec) post EI.
 - A 65 deg decrease in EI wing temp would have resulted in ~37 second delay in onset of same max. temps and heat load.

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Conclusions

- Using certified deorbit/entry targeting:
 - WLE: No appreciable temperature reduction, even when considering extreme Orbiter weight reductions (Scenario 3).
 - Body points (Tile): Some heat rate and heat load reduction is possible with moderate-to-extreme Orbiter weight reductions (Scenarios 1 thru 3).
 - For damage scenarios, the reductions would likely not be directly applicable, depending on the degree of damage.
- In the final analysis, must balance heat rate and heat load for all body points.
 - Variations of the individual sensitivity parameters do not yield any significant results, especially for WLE.
 - Weight reduction scenarios to yield thermal relief are extremely aggressive and carry significant risk.
 - Have not identified method for determining if reduction in heat rate and heat load for bottom surface tiles is meaningful, especially for damage scenarios.

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Forward Work Considerations

- No further work is planned for STS-107 entry options.
- No further work is planned for development of uncertified or contingency deorbit/entry profiles.
- If requested (as part of Return-to-Flight efforts, or otherwise), primary candidates have been identified for consideration:
 - High angle of attack (WLE relief).
 - Low angle of attack (bottom surface relief).
 - High drag and low drag cases.
- Process could yield pros/cons for WLE and other body points in each case - i.e. higher alpha reduces WLE heat rate, but increases heat load for other body points.
- Currently no way to know whether or not these efforts would yield a viable contingency capability to optimize for TPS damaged areas.

ENTRY OPTIONS

Backup Charts

- Orbiter Body Points Diagram
- Trajectory/TSEP Data Plots
- Consumables – Weight/CG Details
- Deployable Items – Weight/CG Details
- Weight Reduction Scenarios – Weight/CG Details
- Sample Wing Leading Edge Stagnation Temperature
- Sample Lower Surface Heat Rate
- Sample Drag Profile

ENTRY OPTIONS

Orbiter Body Points

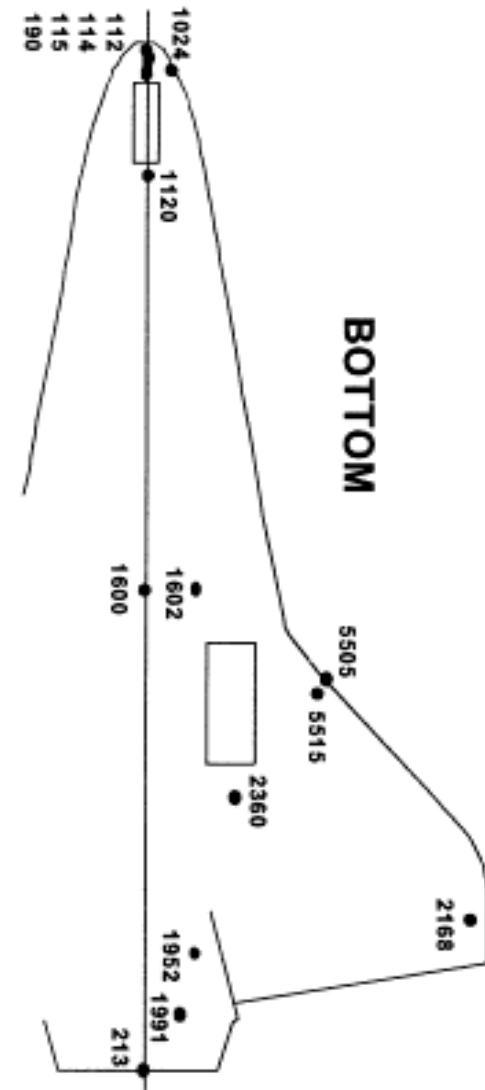
TSEP model includes 29 body points used by USA Flight Design for commit to flight analysis.

Utilized to evaluate key body points individually:

Wing Leading Edge Stagnation Temperature
(Body Point 5505 - RCC Panel 9)

Wing Lower Surface Heat Rate
(Body Point 2360 - aft of MLG door).

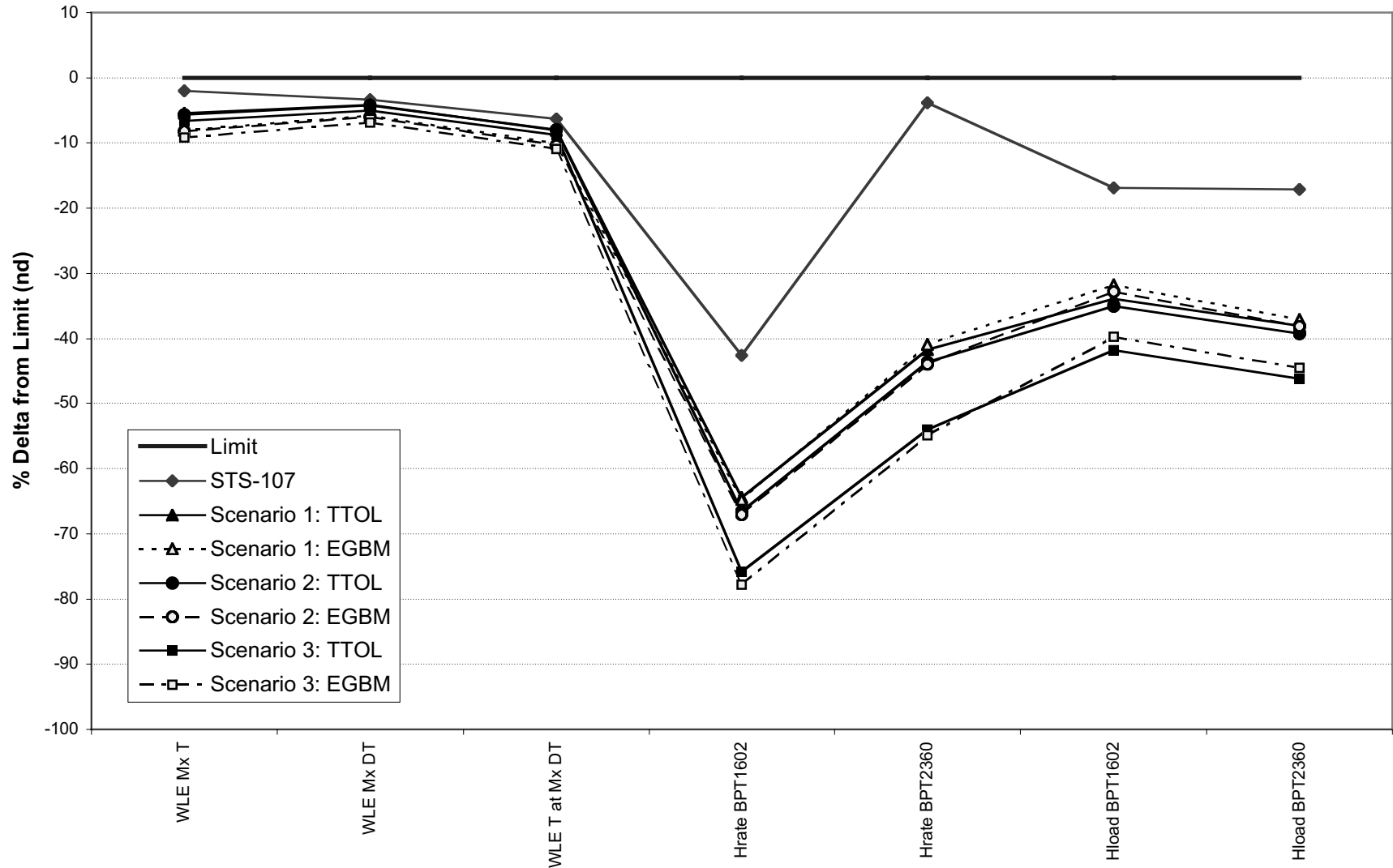
Mid Fuselage
(Body Point 1602 - forward of MLG door)



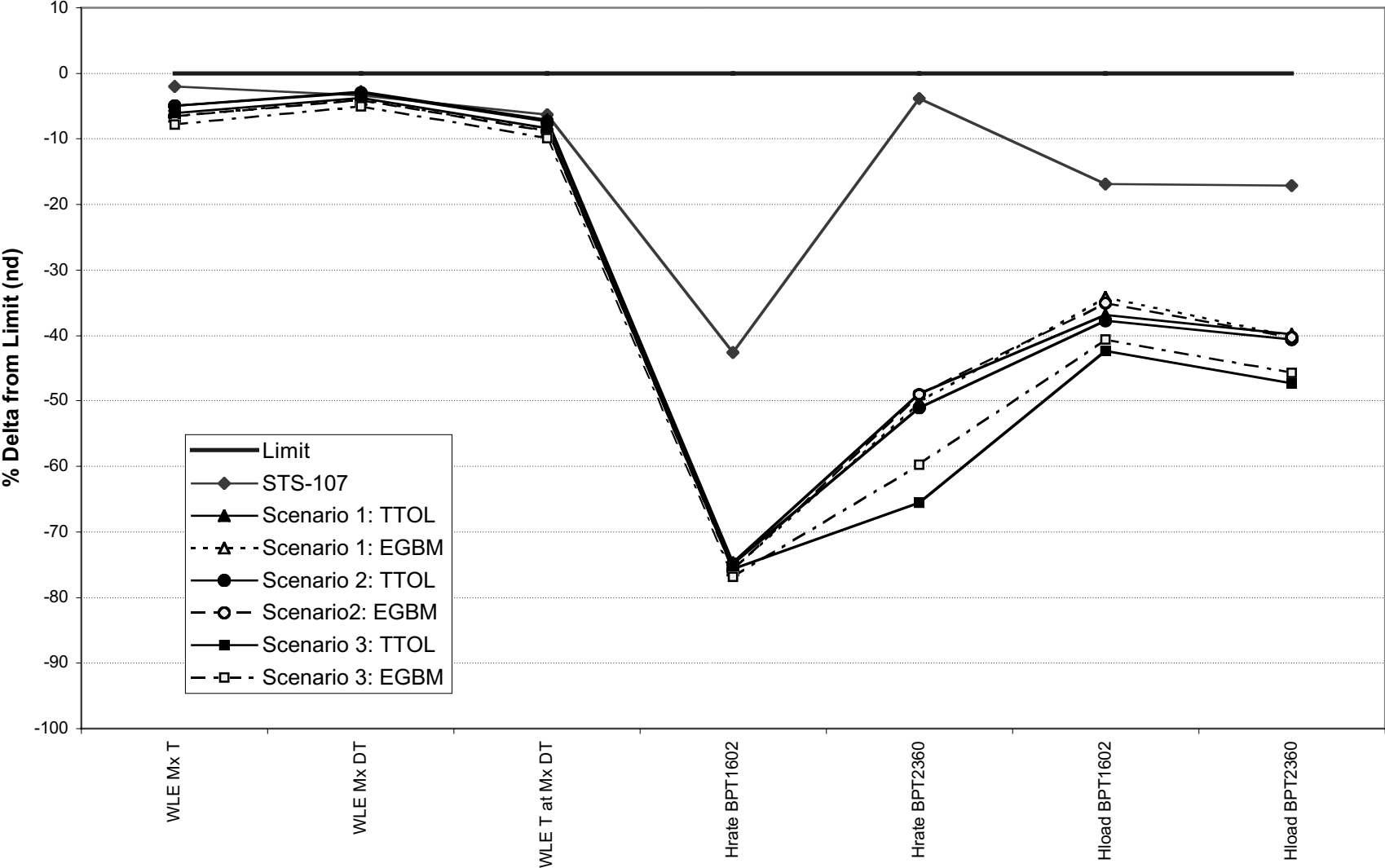
ENTRY OPTIONS
Trajectory/TSEP Data

(see following charts)

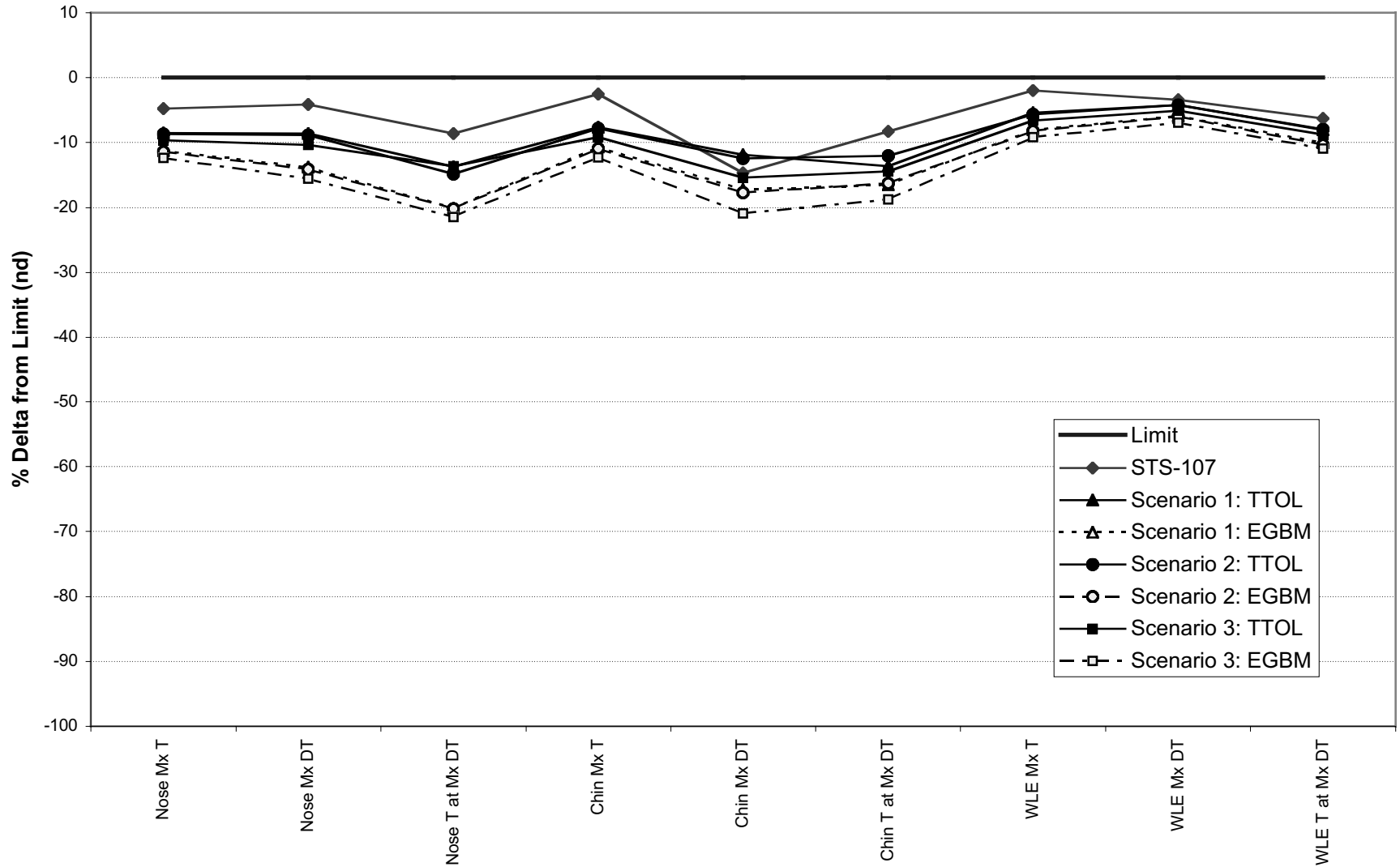
Best Wing Leading Edge Cases



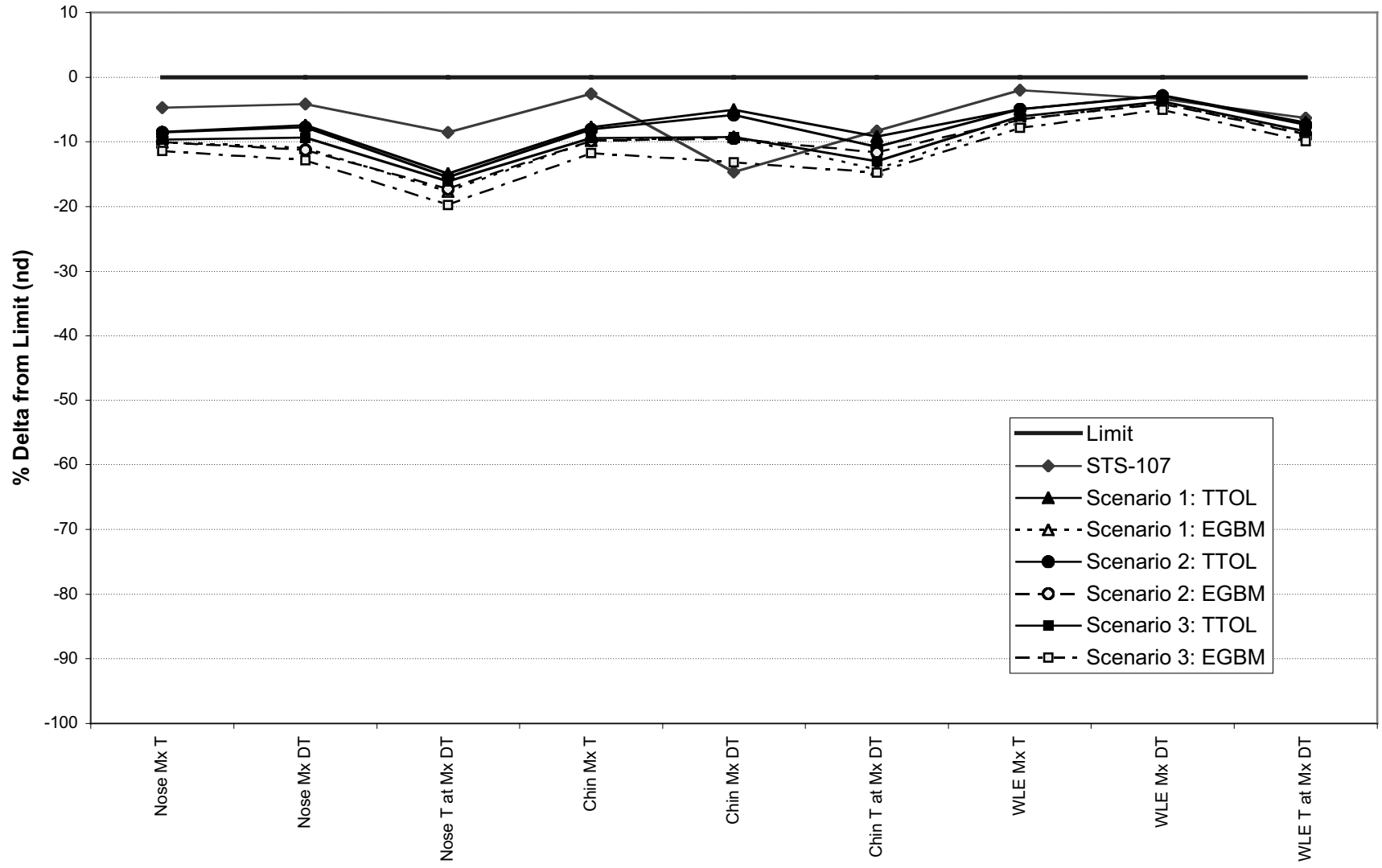
Best Lower Surface Cases



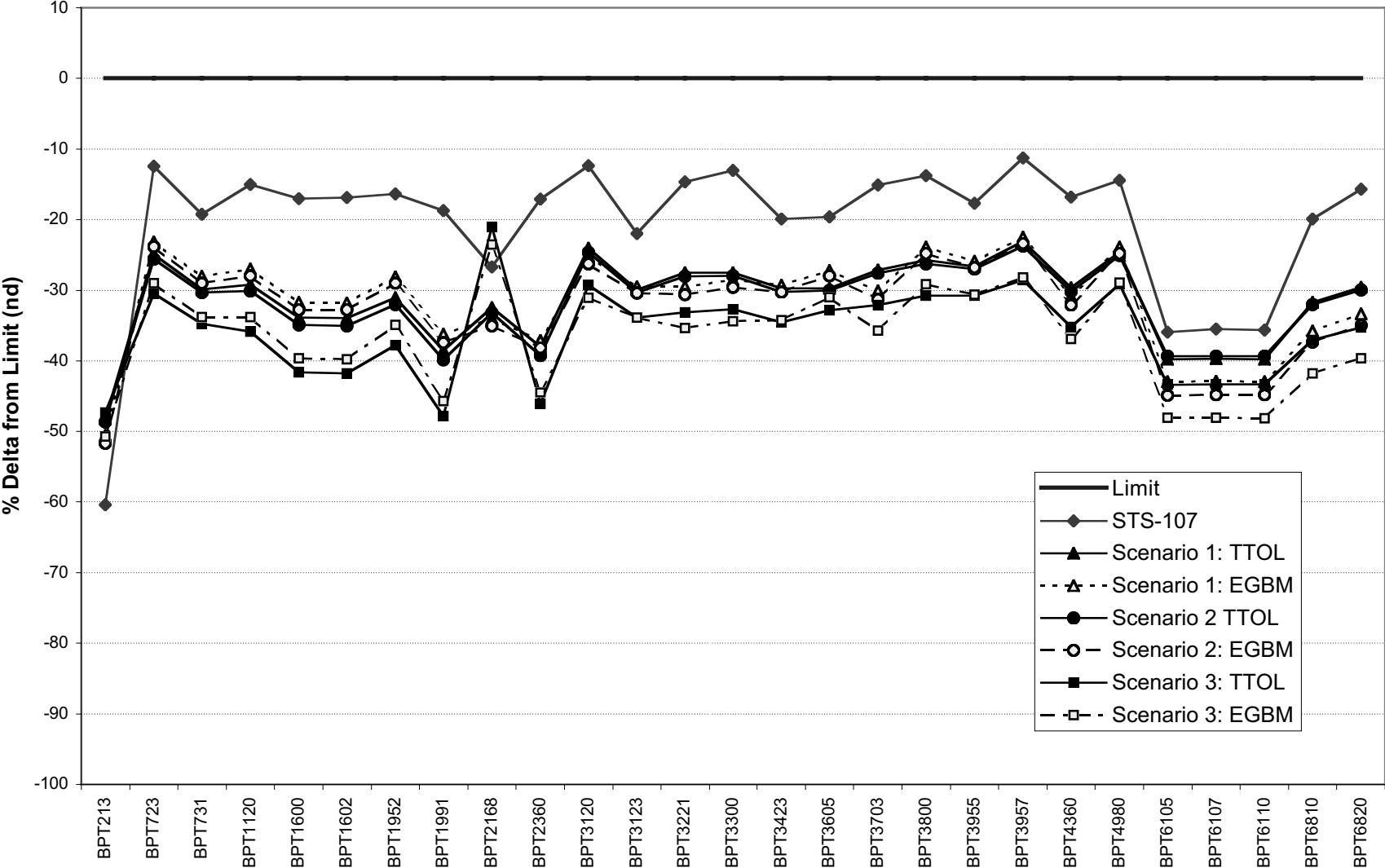
TMMs: Best Wing Leading Edge Cases



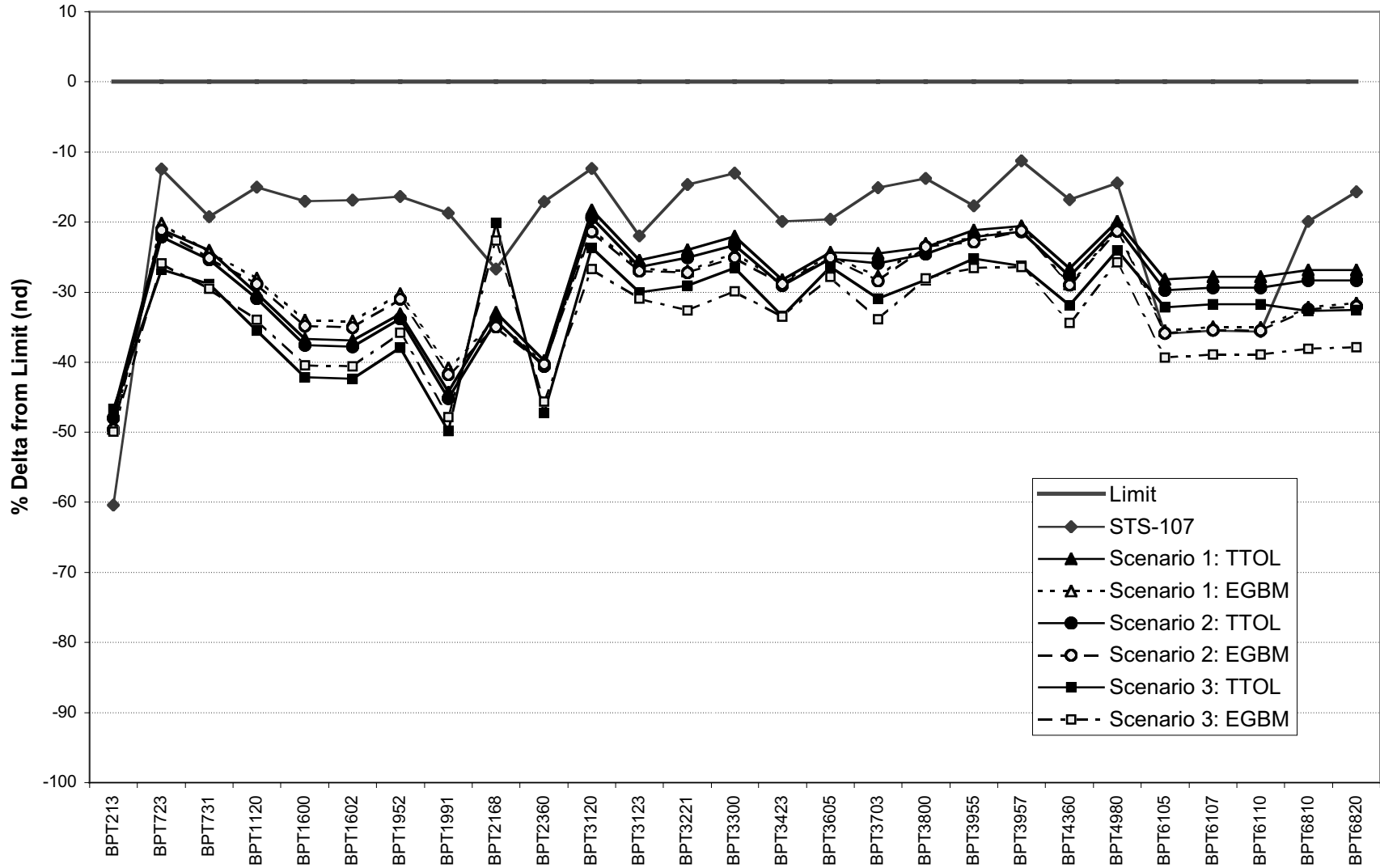
TMMs: Best Lower Surface Cases



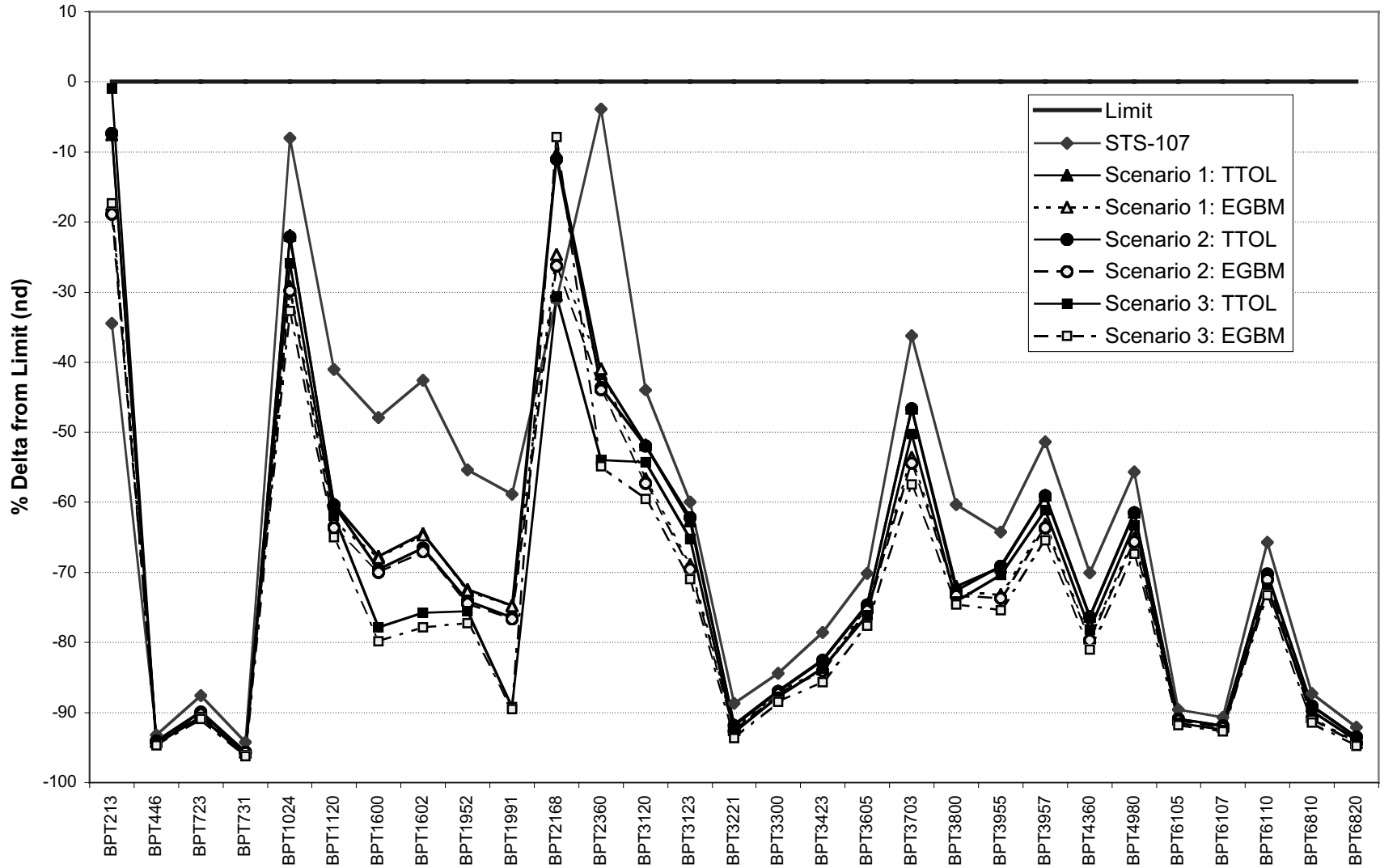
Heat Load: Best Wing Leading Edge Cases



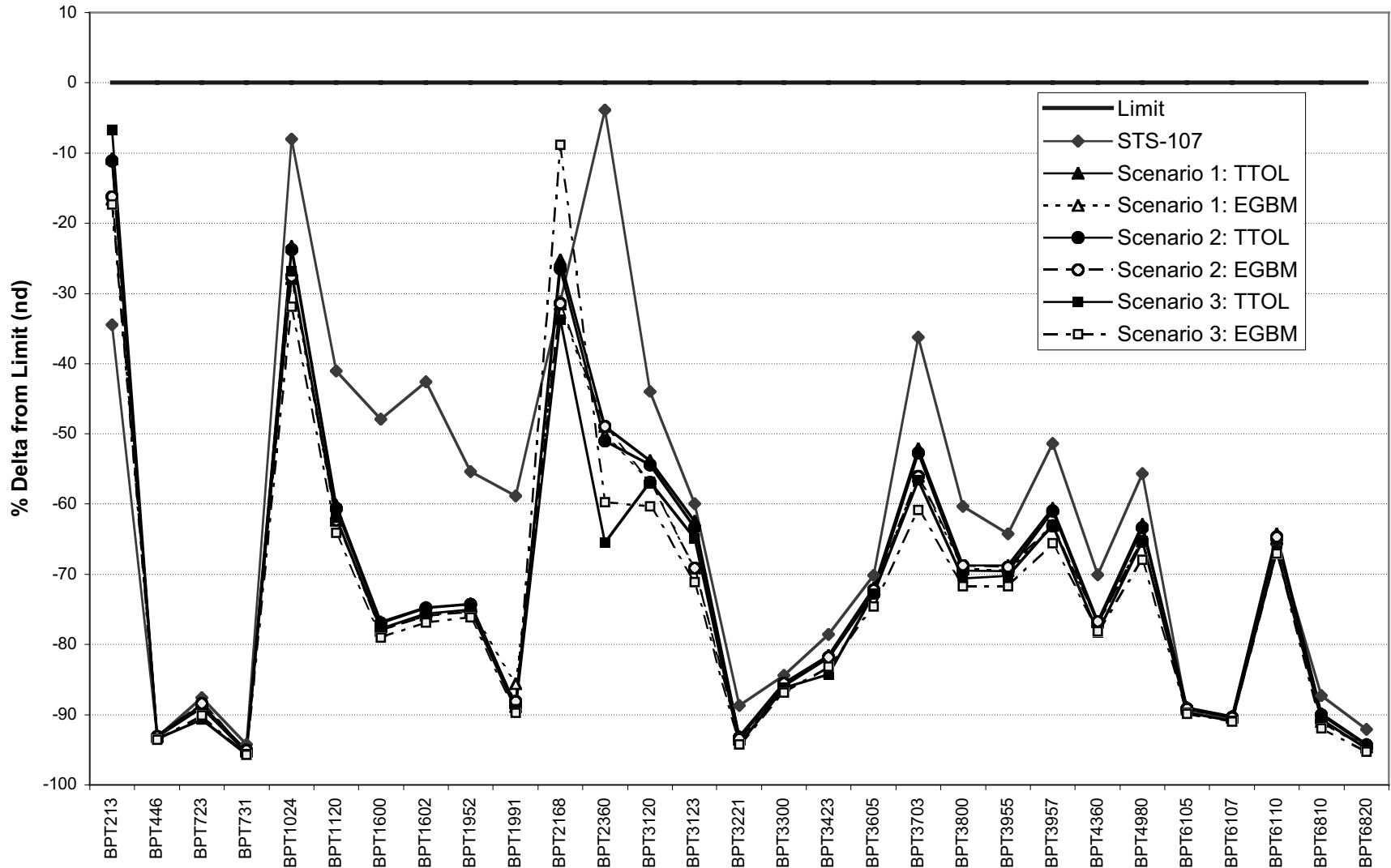
Heat Load: Best Lower Surface Cases



Heat Rate: Best Wing Leading Edge Cases



Heat Rate: Best Lower Surface Cases



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Consumables - Weight/CG Details

ECLSS	Δ Wt	Xcg	Ycg	Zcg	CRYO	Δ Wt	Xcg	Ycg	Zcg	PROP	Δ Wt	Xcg	Ycg	Zcg
GN2 SYS 1	-51	976.6	-29.7	328.7	O2 TK-1	-302.9	778.5	-77.5	308	OMS FU R	(-41)	1444.9	72.262	501.53
GN2 SYS 2	-35	707.8	89	328.7	H2 TK-1	-67.7	891	-76	306.1	OMS OX R	(-152.6)	1444.6	110.48	461.96
GN2 TK-5	0	678	-89	329	O2 TK-2	-286.8	721.5	77.5	308	OMS FU L	(-51)	1444.9	-72.26	501.53
NH3 TK-1	-46	1350	66	442	H2 TK-2	-66.7	835	76	307.1	OMS OX L	(-130.6)	1444.7	-110.5	461.97
NH3 TK-2	-46	1370	67	443	O2 TK-3	-205.7	1115.5	58.3	294.8	RCS FU FWD	0	317	-24	365
POT H2O TK-A	-123	518	0	294	H2 TK-3	-60.9	1009.8	-73.9	302.9	RCS OX FWD	0	317	24	365
POT H2O TK-B	-90	534	0	293	O2 TK-4	0.4	1065.2	-76.5	300.5	RCS FU AFT R	-252.3	1340	67	490
POT H2O TK-C	-90	545	0.9	313	H2 TK-4	0.2	891	76	306.1	RCS OX AFT R	-397.9	1340	99	457
POT H2O TK-D	-90	528	0	311	O2 TK-5	-0.5	949.3	-70	306.2	RCS FU AFT L	-271.2	1340	-67	490
WST H2O TK-1	-79	512	0	310	H2 TK-5	0.0	949.3	69	302.8	RCS OX AFT L	-427.7	1340	-99	457
					O2 TK-6	-340.1	1257.7	56.7	392					
					H2 TK-6	-6.3	1262.5	28.5	350					
APU/HYD	Δ Wt	Xcg	Ycg	Zcg	O2 TK-7	-254.0	1257.7	-56.7	392					
APU N2H4 TK-1	-109	1400	-80	414	H2 TK-7	-7.7	1262.5	-28.5	350					
APU N2H4 TK-2	-113	1400	-85	381	O2 TK-8	-1.3	1257.7	48.7	439					
APU N2H4 TK-3	-278	1400	80	414	H2 TK-8	-0.4	1262.5	0	399.4					
HYD H2O TK-1	-9	1373	0	481	O2 TK-9	0.2	1257.7	-48.7	439					
HYD H2O TK-2	-22	1393	0	483	H2 TK-9	-0.4	1262.5	0	454					
HYD H2O TK-3	-29	1353	0	479										

NOTE: Items shown in "()" not included in scenario buildups

ENTRY OPTIONS

Deployable Items - Weight/CG Details

					Deployables from Freestar Elements				
	Δ Wt	Xcg	Ycg	Zcg		Δ Wt	Xcg	Ycg	Zcg
Spacehab	-18071	892.3	-3.5	392.4	MEIDEX	-428	1152	40	404
Freestar	-4428	1119.8	0.7	396.9	SOLSE-02	-423	1152	-40	404
Radiator Panel	-1657	944	-55	450	CVX-2 Exp Package	-364	1093	13	400
					CVX-2 Avn Package	-361	1093	-13	400
					SEM	-315	1093	-40	400
Deployables from Spacehab Systems									
	Δ Wt	Xcg	Ycg	Zcg		Δ Wt	Xcg	Ycg	Zcg
PDU	-85.00	815	6	332	Halon Bottle 6 (filled)	-5.94	990	57	434
FSCU	-22.00	807	28	332	Halon Bottle 7 (filled)	-5.94	990	-57	434
CSA	-29.50	844	28	332	Halon Bottle 8 (filled)	-5.94	990	57	374
Fwd Inverters (3)	-13.71	859	33	332	Halon Bottle 9 (filled)	-5.94	988	12	330
Aft Inverters (3)	-13.71	972	1	332	Halon Bottle 10 (filled)	-5.94	885	-12	330
Scrubber	-15.00	879	30	332	Handheld Halon 1 (filled)	-5.25	793	-16	386
Fwd Luminaries (4)	-17.00	841	0	445	Handheld Halon 2 (filled)	-5.25	896	20	438
Aft Luminaries (4)	-12.48	943	0	445	SEBS (2)	-35.40	801	-19	420
ARS Fan	-3.29	844	-10	332	CST (dry)	-45.00	982	-29	332
Smoke Detectors (2)	-4.80	878	0	332	Air Balancing Box	-30.20	962	-27	332
Dew Point Elec + 2 Sensors	-9.30	840	1	332	Hab Fan Assembly	-35.00	947	-26	332
ACS	-34.70	801	19	402	Air Bypass Valve Assy	-26.70	930	-26	332
DMU	-12.80	859	-32	332	Condensing Hx (dry)	-60.22	905	-8	332
EDSMU	-47.36	801	0	414	PPO2 Sensors (2)	-3.62	796	0	402
EDS Hub	-21.35	801	-62	386	PPCO2 Sensors (2)	-7.26	878	0	332
ECU	-9.24	878	-28	332	Total Pressure Sensor	-0.58	796	0	402
CEWL Pumps (2)	-56.00	938	29	332	Temperaure Sensors (9)	-4.77	890	0	332
APDU	-93.00	932	12	332	Water Seperator	-18.42	927	-6	332
MCP	-34.50	801	-19	402	WFCV	-4.65	815	-31	332
CO2 Box	-6.73	942	-9	332	Exp HX 1 (dry)	-7.70	931	24	332
Fwd EXCPs (3)	-26.20	794	0	394	Exp HX 2 (dry)	-7.70	835	-24	332
Aft EXCPs (4)	-38.60	989	0	394	CEWL HX (dry)	-7.70	900	31	332
Halon Bottle 1 (filled)	-5.94	793	-57	434	Water Metering Valves (11)	-9.13	860	0	332
Halon Bottle 2 (filled)	-5.94	793	57	434	Water Flow meters (2)	-15.20	815	-32	332
Halon Bottle 3 (filled)	-5.94	800	-62	374	Water Temp Sensors (7)	-3.71	830	-10	332
Halon Bottle 4 (filled)	-5.94	793	57	374	VSU	-8.00	801	-43	386
Halon Bottle 5 (filled)	-5.94	885	12	330					

ENTRY OPTIONS

Deployable Items - Weight/CG Details (cont.)

	Deployables from Spacehab Payloads								
	Δ Wt	Xcg	Ycg	Zcg		Δ Wt	Xcg	Ycg	Zcg
ARMS	-369.10	801	43	386	AST 10/1	-78.92	983	0	362
EIU#2	-19.33	801	43	434	AST 10/2	-59.58	857	-31	368
STARS-Bootes	-65.02	983	-19	362	CPCG-PCF	-77.00	983	19	438
ERISTO	-71.50	983	-19	374	CIBX	-76.50	983	19	415
PhAB4	-202.61	850	-31	390	MSTRS	-20.00	801	19	438
EOR/F	-146.01	983	0	420	ZCG	-108.84	983	43	380
TEHM	-116.89	983	-19	408	FRESH	-367.60	801	31	420
Centrifuge	-32.54	801	-43	403	Biotube	-71.57	983	43	362
FAST	-130.31	983	43	432	SH FDF	-60.60	928	55	395
APCF	-75.15	983	19	403	Shared PGSC	-16.97	832	-31	430
Biobox	-116.70	983	19	374	Camcorders (2)	-30.00	801	-62	406
VCD FE (rack)	-944.27	915	55	390	35mm Camera	-22.63	837	-31	368
CM-2 (2 racks)	-2801.65	910	-55	390	Media Bag	-19.72	933	55	408
SAMS FF	-24.30	983	0	426	Stowage Bag/Straps	-5.00	842	-31	378
MGM	-305.28	983	43	403	Crew Ops H/W	-29.96	801	-43	374
BDS-05	-181.37	983	-10	386	Trash Stow	-19.28	801	-43	362
Ergometer	-106.08	801	62	402	Supplemental Equip	-44.70	982	-43	368
HLS AMS	-60.49	983	62	386	SSP Clothes/LiOH	-113.44	837	-31	385
4/23/2003	-19.33	983	-43	412	A8/LeRoy E. Cain				33

ENTRY OPTIONS

Deployable Items - Weight/CG Details (cont.)

	Deployables from Middeck								
	Δ Wt	Xcg	Ycg	Zcg		Δ Wt	Xcg	Ycg	Zcg
MF57A - Pantry Food	-61	434	9	407	MA9J - Clothing	-36	524.5	61.3	355.7
MF43C - IFM Tools	-69	433.6	-9.2	395.8	MA9L - Clothing	-41	524.5	61.3	344.5
MF57C - Crew Support	-20	433.6	9.3	395.8	MA9N -	-73	524.5	61.3	333.4
MF14E - LiOH Cans 49-57	-44	434.1	-46.2	384.7	MA16D - CMPCG	-66.9	524.5	42.9	389
MF28E - Printer Trays, GIRA	-26	434.1	-27.7	384.7	MA16F - Menu Food	-50	524.5	42.9	377.9
MF43E - IFM Breakout Box, etc.	-38	434.1	-9.2	384.7	MA16G - Clothing	-40	524.5	42.9	366.8
MF57E - Fresh Food	-58	434.1	9.3	384.7	MA16J - Clothing	-40	524.5	42.9	355.7
MF71E - HLS/CEBAS, ZCG Autoclaves	-36	434.1	27.7	384.7	MA16L - Clothing	-40	524.5	42.9	344.5
MF28G/H - Biopack	-61.23	434.7	-27.7	373.6	MA16N - Menu Food	-51	524.5	42.9	333.4
MF28G/H - Biopack	-61.23	435.3	-27.7	362.5	MAR	-100	482.1	-59.3	368.9
MF43G - Post Insertion	-46	434.7	-9.2	373.6	A/L Ceiling Bag - Clothing, Food, etc.	-107.5	560	0	410
MF57G - HLS	-36.72	434.7	9.3	373.6	A/L Floor Bag-LiOH Cans 31-48, etc.	-165.6	560	0	340
MF71G - Osteo	-60.6	434.7	27.7	373.6	Volume B - Hygiene	-85	521	79	375
MF14H - Menu Food	-46	435.3	-46.2	362.5	Volume 3B - OCAC	-30.5	535	43.5	370.1
MF43H - Biopack CB	-30.1	435.3	-9.2	362.5	A16 - 70mm Camera Bag, etc.	-55.43	562	15	429
MF57H - PTCU 1	-59	435.3	9.3	362.5	A17 - CC Sys Bag, 35mm Cam, etc.	-52.01	562	-15	429
MF71H - PTCU 2	-58.1	435.3	27.7	362.5	MD52M - (EDO LiOH Box) ATCO, etc.	-61.65	492	0	311
MF14K - Menu Food	-51	435.8	-46.2	351.4	MD52C - (Volume D) LiOH Cans 11-30	-137	439	0	314
MF28K - Med Kits, Dosimeter	-47	435.9	-27.7	351.4	MD75C - (Volume E) OFK, PPK	-65.5	437	27.7	329.2
MF43K - FDF and SH FDF	-45	435.9	-9.2	351.4	MD80R - (Volume G) Cont UCD's, etc.	-45	525	42	317
MF57K - FDF	-59	435.9	9.3	351.4	WMC - Towels and Resupply Items	-75.6	546	-49	365
MF71K - ZCG, Autoclaves Box	-54.5	435.9	27.7	351.4	Galley	-76.7	452	-64	353
MF14M - Menu food	-55	436.5	-46.2	340.3	Ergometer	-115	488.2	-10.3	357.4
MF28M - COAS, 70mm Film, etc.	-40	436.5	-27.7	340.3	Flight Deck Fire Extinguisher	-6.2	481.6	-0.3	459
MF43M - PTCU 3	-50.3	436.5	-9.2	340.3	Middeck Fire Extinguisher (Side Hatch)	-6.2	546	-49	365
MF57M - PTCU 4	-48.5	436.5	9.3	340.3	Middeck Fire Extinguisher (Airlock)	-6.2	560	0	410
MF71M - BDS-D5	-45.48	436.5	27.7	340.3	Av Bay Fan 1A	-4.1	406	-27	340
MF14O - Menu Food	-50	437	-46.2	329.2	Av Bay Fan 2B	-4.1	406	27	340
MF28O - Meidex, Solse, PGSC's	-47	437	-27.7	329.2	Av Bay Fan 3A	-9.38	560	51	350
MF71O - Bric	-65.5	437	27.7	329.2	IMU Fans A,C	-5.95	434	9	407
MA9D - Menu Food	-41	524.5	61.3	389	Cabin Fan B	-5.6	461	4	315
MA9F - Clothing	-42	524.5	61.3	377.9	Humidity Separator	0	461	4	315
MA9G - Clothing	-39	524.5	61.3	366.8					

ENTRY OPTIONS

Deployable Items - Weight/CG Details (cont.)

Deployables from Flight Deck / Avionics

LRU	SLOT	#	MASS	Location	Δ Wt	X CG	Y CG	Z CG	LRU	SLOT	#	MASS	Location	Δ Wt	X CG	Y CG	Z CG
GPC	2,4	2	60	Av Bay 2	-120	406	27	340	PCMMU	2	1	30	Av Bay 2	-30	406	27	340
GPC	3	1	60	Av Bay 3	-60	406	27	340	HUD	2	1	20	Av Bay 2	-20	406	27	340
MDM	LF1	1	38.5	Av Bay 1	-38.5	406	-27	340	HUDE	2	1	40	Av Bay 3B	-40	406	27	340
MDM	FF4, PL2	2	38.5	Av Bay 2	-77	406	27	340	RHC	A	1	10	A6	-10	568	-3	477
MDM	FF3	1	38.5	Av Bay 3	-38.5	406	27	340	DDU	A	1	23	A6	-23	568	-3	477
ADTA	2, 4	2	11	Av Bay 2	-22	406	27	340	MDU	AFT 1, CRT 4 2	17		R12	-34	541	53	445
ADTA	3	1	11	Av Bay 1	-11	406	-27	340	PL INTEROG	n/a for 107	0	46.5		0	0	0	0
TACAN	1	1	30	Av Bay 1	-30	406	-27	340	PDI		1	27.5	Av Bay 1	-27.5	406	-27	340
TACAN	2	1	30	Av Bay 2	-30	406	27	340	PL Recorder		1	43	Av Bay 1	-43	406	-27	340
TACAN	3	1	30	Av Bay 3	-30	406	27	340	KUSP		1	41	Av Bay 3B	-41	406	27	340
MLS (RF & DEC)	1	1	23.5	Av Bay 1	-23.5	406	-27	340	KU EA 1		1	45	Av Bay 3	-45	406	27	340
MLS (RF & DEC)	2,3	2	23.5	Av Bay 2	-47	406	27	340	KU EA 2		1	34	Av Bay 3	-34	406	27	340
RA	2	1	4.5	Av Bay 2	-4.5	406	27	340	KU DEA (PLB)		1	83	PLB	-83	576	94	414
BFC	1	1	12.5	Av Bay 1	-12.5	406	-27	340	KU DMA (PLB)		1	89	PLB	-89	576	94	414
BFC	2,3	2	12.5	Av Bay 2	-25	406	27	340	PSP	1,2	2	18	Av Bay 2	-36	406	27	340
MMU	2	1	25	Av Bay 2	-25	406	27	340	COMSEC	2	1	46.5	Av Bay 3	-46.5	406	27	340
NSP	2	1	19	Av Bay 3	-19	406	27	340	FM SIG PROC		1	12	Av Bay 3	-12	406	27	340
AA	4	1	2.3	Av Bay 1	-2.3	406	-27	340	Color TV Monitors		2	40	L12	-80	560	-45	443
AA	2,3	2	2.3	Av Bay 2	-4.6	406	27	340	FM XMTR	1,2	2	6.8	Av Bay 3	-13.6	406	27	340
OPS Recorder	1,2	2	43	Av Bay 2	-86	406	27	340									

Groundrules/Assumptions

1. Reduce to zero fault tolerance for GNC functions & Comm.
2. Retain BFS for PLBD ops, antenna management, and SM insight (no engage capability).
3. Relies on GPS 2 only for nav updates.
4. Data recording capability sacrificed.

ENTRY OPTIONS

Weight Reduction Scenarios - Weight/CG Details

Scenario 1: *Total weight savings = 20,387 lbs*

Weight/cg changes from items A, B, C, D, and E

	<u>Weight</u>	<u>Xcg</u>	<u>Ycg</u>	<u>Zcg</u>	
Entry Interface	214088.6		1098.60	-0.18	370.38
TAEM	213611.1		1097.66	-0.17	370.20
Landing	213529.8		1099.37	-0.16	367.50

Scenario 2: *Total weight savings = 22,924 lbs*

Weight/cg changes from items A, B, C, E, and F

	<u>Weight</u>	<u>Xcg</u>	<u>Ycg</u>	<u>Zcg</u>	
Entry Interface	211551.6		1098.35	-0.26	370.11
TAEM	211074.1		1097.39	-0.25	369.93
Landing	210992.8		1099.12	-0.24	367.19

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ENTRY OPTIONS

Weight Reduction Scenarios - Weight/CG Details

Scenario 3: *Total weight savings = 31,321 lbs*

Weight/cg changes from items A, B, F, and G

	<u>Weight</u>	<u>Xcg</u>	<u>Ycg</u>	<u>Zcg</u>	
Entry Interface	203154.9		1107.83	-0.68	369.52
TAEM	202677.4		1106.85	-0.67	369.33
Landing	202596.1		1108.66	-0.66	366.48

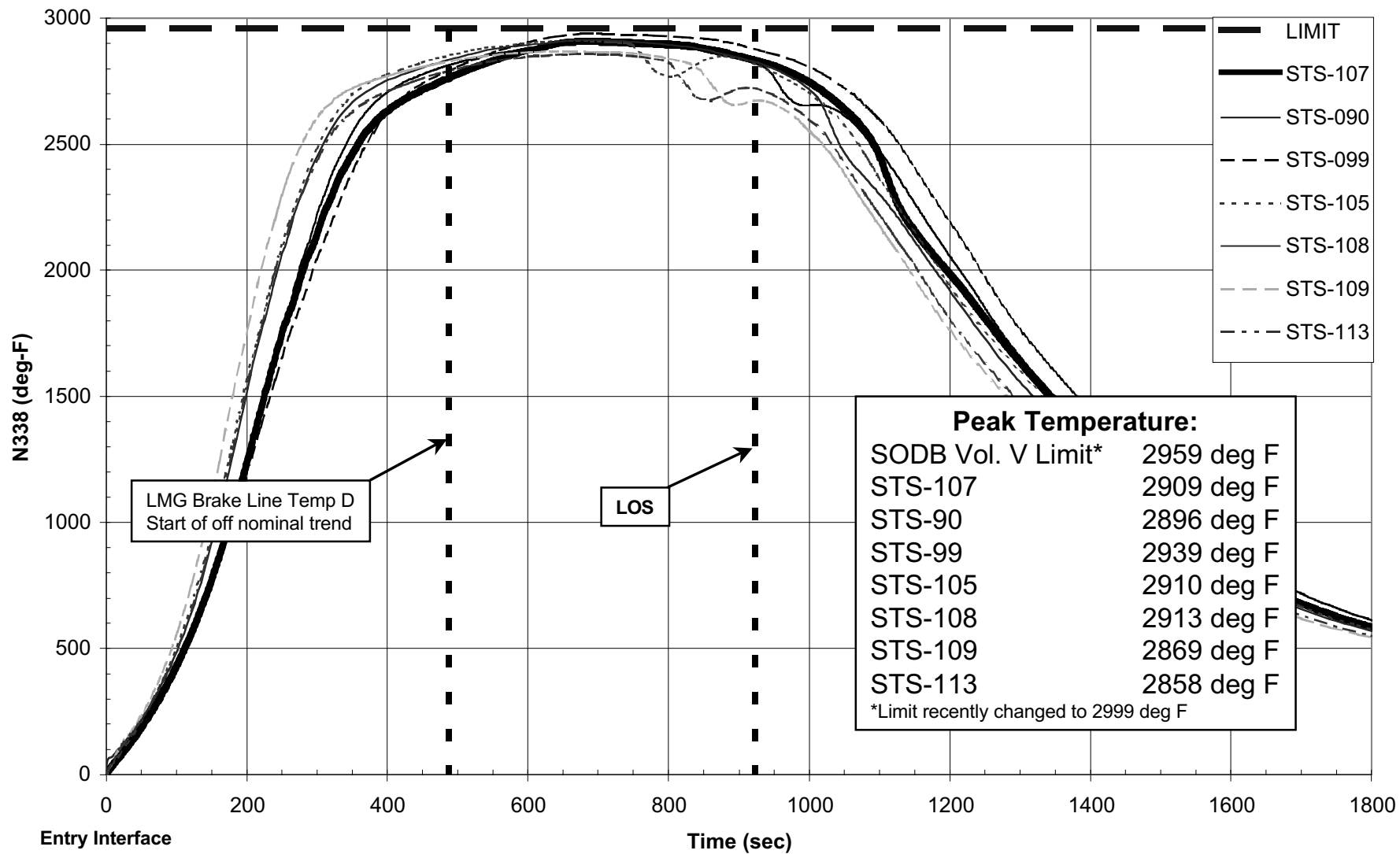
- For a baseline comparison, the following are the predicted end-of-mission mass properties from STS-107.

	<u>Weight</u>	<u>Xcg</u>	<u>Ycg</u>	<u>Zcg</u>	
Entry Interface	234477.0		1078.91	-0.56	371.97
TAEM	233999.5		1078.00	-0.55	371.81
Landing	233918.2		1079.56	-0.54	369.35

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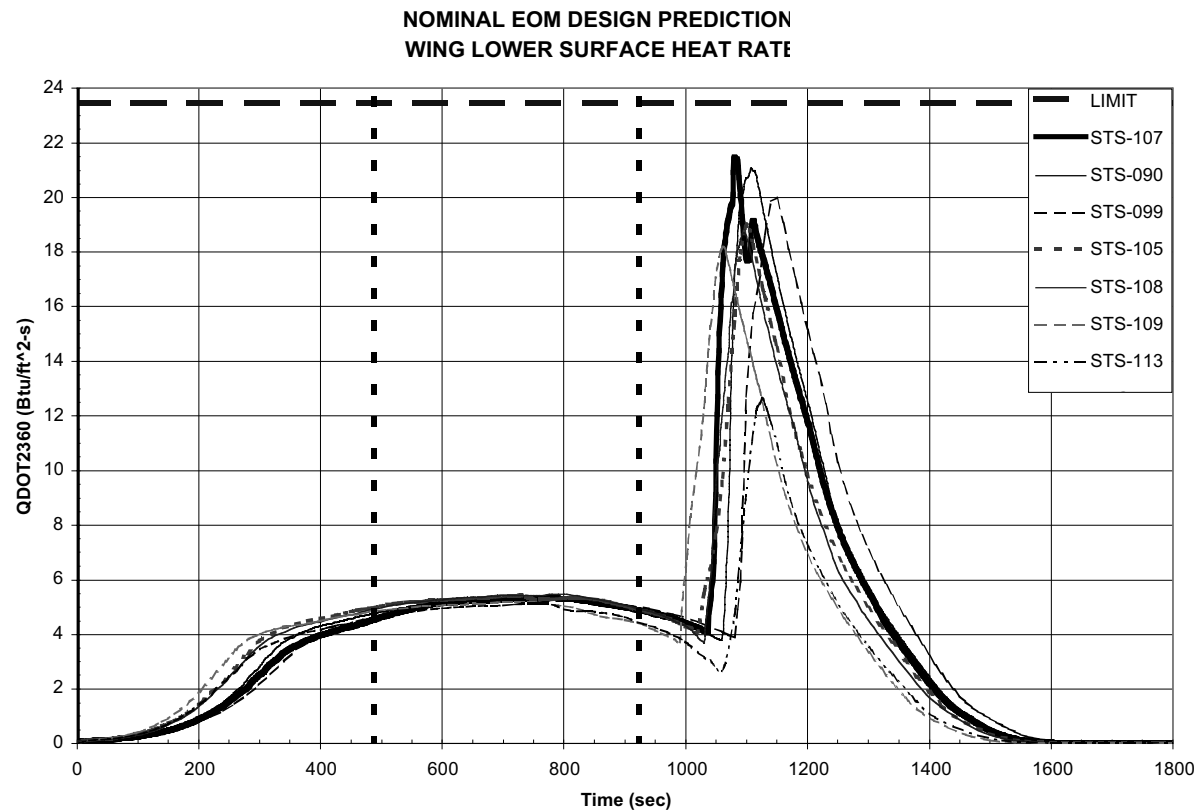
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NOMINAL EOM DESIGN PREDICTION: WING LEADING EDGE STAGNATION TEMPERATURE



ENTRY OPTIONS

Lower Surface Heat Rate – Multiple Flights



ENTRY OPTIONS

Sample Drag Profile

